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2 **Significance of tridymite distribution during cooling and**
3 **vapor-phase alteration of ignimbrites**

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ABSTRACT

53 Thick sequences of silicic ignimbrites contain complex emplacement and cooling histories,
54 often masking contacts between ignimbrite flow packages. Mineralogical and textural
55 variations in these sequences are primarily a function of emplacement temperature and
56 cooling time. Here, we focus on the use of the silica polymorph tridymite to understand the
57 association of vapor-phase crystallization and devitrification within ignimbrite flow
58 packages. As opposed to the common occurrence of cristobalite, the restricted domains in
59 which we observe tridymite may provide more relevant constraints for interpreting post-
60 emplacement devitrification and vapor-phase alteration. This study examines sections
61 through the Whakamaru (New Zealand), Bishop (USA), and Grey's Landing (USA)
62 ignimbrites by combining textural observations with measurements of density, groundmass
63 crystallinity, and the distribution and proportion of tridymite to cristobalite. The rheomorphic
64 Grey's Landing ignimbrite represents a high-temperature endmember scenario, with widely
65 distributed tridymite (up to 20%) resulting from a high magmatic temperature and rapid
66 devitrification in a low porosity deposit. In the welded Whakamaru and Bishop ignimbrites,
67 metastable tridymite (up to 13%) is concentrated along boundaries between flow packages.
68 Here tridymite is interpreted to crystallize in transient permeable zones, forming during
69 vapor-phase alteration prior to compaction, where upper denser-welded flow materials serve
70 as vapor seals. Our results suggest that tridymite may link the initial cooling and welding
71 history of ignimbrites to vapor-phase alteration and devitrification, and may serve as a
72 potential mineralogical fingerprint of depositional contacts, important for consideration of
73 lateral transport of fluids in geothermal reservoirs.

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INTRODUCTION

76 Ignimbrites, the deposits of concentrated pyroclastic flows, show a great range in
77 lithological characteristics linked to their emplacement and cooling histories. These
78 characteristics relate to both the mechanical processes involved in flow emplacement and the
79 consequent thermal characteristics of the resulting deposits (e.g. Smith 1960a,b; Ross and
80 Smith 1961; Streck and Grunder 1995; Grunder and Russell 2005; Quane and Russell 2005;
81 Branney et al. 2008; Wright and Cashman 2014). In particular, ignimbrite welding textures
82 correlate to emplacement temperatures (reflected in the rock density: Wilson and Hildreth
83 2003), varying from non-welded (low temperature; McClelland et al. 2004) to densely-
84 welded with rheomorphic flow (high temperature; Branney et al. 2008).

85 In parallel with the variations in thermal histories seen in density/welding intensity,
86 there is frequently a transformation of the amorphous glass phase by devitrification and
87 vapor-phase alteration (Smith 1960; Streck and Grunder 1995; Keating 2005; Wright et al.
88 2011). Here we adopt simple definitions of devitrification and vapor-phase alteration
89 following prior work on the Whakamaru ignimbrite by Briggs (1976a). Devitrification, the
90 crystallization of the amorphous glass phase, occurs below the glass transition temperature
91 (Lofgren 1971). Vapor-phase alteration in contrast is associated with crystals forming in
92 voids or open spaces (Briggs 1976a). The timing and extent of vapor-phase alteration is
93 dependent on temperature changes, and the source and availability of volatiles (Sheridan
94 1970; Keith 1991). Field investigations have documented the relative timing and relationship
95 between devitrification and vapor-phase alteration, whereby in many cases volatiles released
96 from glass during devitrification promote vapor-phase alteration in the mid- to upper levels of
97 the ignimbrite (Sheridan 1970; Streck and Grunder 1995).

98 This study focuses primarily on the relationship between post-depositional
99 crystallization and emplacement history of the Whakamaru (NZ) and Bishop (USA)
100 ignimbrites. The Grey's Landing ignimbrite (Andrews and Branney, 2011), a high-

101 temperature Snake-River Plain (SRP)-type ignimbrite, provides a textural and mineralogical
102 endmember (Ellis et al. 2015) where crystallization patterns reflect devitrification in a low
103 porosity deposit with little pore space available for vapor-phase crystallization.

104 The mineralogical changes accompanying devitrification and vapor-phase alteration
105 provide insights into post-eruptive processes such as cooling, crystallization, and degassing.
106 These processes in turn are important in understanding fluid flow and reactions in ignimbrites
107 in situations such as geothermal reservoir modelling (Cavazos-Álvarez et al. 2020) and flow
108 of groundwater through underground repositories (Spycher et al. 2003). While the silica
109 polymorph cristobalite has received a great deal of attention because of its widespread
110 occurrence in volcanic deposits and carcinogenic properties (Schipper et al. 2020), we
111 suggest the more restricted domains in which tridymite is observed in ignimbrites may
112 provide a more targeted fingerprint for interpreting ignimbrite emplacement and cooling
113 processes.

114 Tridymite stability has been debated since the early work of Fenner (1913), with
115 experimental observations suggesting important temperature and compositional controls (e.g.
116 Holmquist 1961; Flörke and Langer 1972). Stevens et al. (1997) argued for what is now
117 generally accepted: tridymite stability is dependent on chemical impurities such as water or
118 alkali oxides, with the amount and type of oxide influencing crystallization temperatures (β -
119 tridymite stable starting from 870-1000 °C: Holmquist 1961) and kinetics (Garofalini and
120 Miller 1986). Tridymite is generally considered a metastable phase at lower temperatures
121 (Jones and Segnit 1972), with both metastable cristobalite and tridymite favored by rapid
122 growth rates from amorphous silica. It is suggested that both cristobalite and tridymite
123 initially nucleate, with higher rates of nucleation initially favoring cristobalite, but giving way
124 to tridymite as crystallization progresses (Madden and Van Vlack 1967; Wu et al. 2002). The
125 balance between the proportions of the silica polymorphs formed through devitrification and

126 vapor-phase processes thus may give us information about the post emplacement history of
127 ignimbrites (Payette and Martin 1986; Green and Fitz 1993; Rowe et al. 2012). We therefore
128 investigate the contrasts in silica polymorph development and significance of tridymite
129 occurrences from both devitrification and vapor-phase alteration in the Whakamaru
130 ignimbrite, Bishop Tuff, and Grey's Landing ignimbrite, representing a range of eruption
131 temperatures and emplacement histories.

132

133

GEOLOGIC BACKGROUND

134 This study uses samples from three supereruption-related ignimbrites, Whakamaru
135 (NZ), Bishop (USA), and Grey's Landing (USA; Fig. 1). The 0.35 Ma Whakamaru
136 ignimbrite erupted as part of a sequence of voluminous tuffs ($>1000 \text{ km}^3$; Whakamaru
137 Group) accompanying the formation of the largest caldera in the central Taupo Volcanic
138 Zone of New Zealand (Fig. 1A; Wilson et al. 1986; Brown et al. 1998, Downs et al. 2014).
139 Northwest of the caldera, the Whakamaru ignimbrite forms a thick (locally $>200 \text{ m}$) infill
140 along the paleovalley of the Waikato River (Martin 1965). This infill has since been partially
141 eroded by the river along the line of the pre-ignimbrite valley. Although varying degrees of
142 welding intensity are evident across flow packages, no non-welded parts exposed in this area
143 have survived weathering (Briggs 1976a, b). A chronology for the ignimbrite has not been
144 established: although a widespread co-eruptive fall deposit has been identified beyond the
145 limits of the ignimbrite (Froggatt et al. 1986; Matthews et al. 2012), fall deposits have never
146 been reported underlying, interbedded with or overlying the ignimbrite itself. Estimated
147 magmatic temperatures derived from Fe-Ti oxide pairs indicate several different pumice
148 populations that record temperatures from 740 to 840 °C (Brown et al. 1998), while
149 amphibole compositions yield a similar temperature mode of 770 °C (Matthews et al. 2012).

150 However, Brown et al. (1998) suggest magmatic temperatures from the Whakamaru
151 ignimbrite relevant to this study are at the lower end of that temperature spectrum.

152 Within the Maraetai dam section of the Whakamaru ignimbrite along the Waikato
153 River, early workers defined a region of dominant horizontal fracturing (Fig. 1) as a contact
154 between ignimbrite packages within the deposit (e.g. Ewart 1965; Martin 1965). The upper
155 package, as defined by Martin (1965) has a higher crystal and pumice content, although the
156 contact is described as gradational. In contrast, Briggs (1976b) cast the Whakamaru
157 ignimbrite into six subunits (A-F) based on textural, mineralogical, and magnetic properties.
158 On this basis, and the Maraetai dam section would be composed primarily of subunits D, E,
159 and the lower portion of F as defined by her. Briggs (1976b) argued that the horizontal
160 jointing occurs at the transition from dense to moderate welding, rather than at the lithologic
161 contact between flow packages (Fig. 2, Supplemental Figure 1).

162 The 0.76 Ma Bishop Tuff was erupted accompanying formation of Long Valley
163 caldera in eastern California, representing the culmination of a prolonged history of silicic
164 volcanism in the area (Hildreth 2004; Hildreth and Fierstein 2017). The eruption generated
165 widespread fall deposits and a large, partly welded ignimbrite in a short-lived eruption,
166 estimated to have lasted of the order of a week from consideration of accumulation rates for
167 the fall deposits that are demonstrably coevally emplaced with the ignimbrite (Wilson and
168 Hildreth 1997; Hildreth and Wilson 2007). The fall deposit is subdivided into nine units (F1-
169 F9), in places interbedded with the ignimbrite which itself is divided into early (Ig1) and late
170 (Ig2) flow packages, labelled with an indicator of where the deposit is best developed (Ig2E),
171 and subpackages (a, b, c, d; Wilson and Hildreth 1997). Stratigraphic descriptions of the
172 Bishop Tuff are detailed in Wilson and Hildreth (1997, 2003). Magmatic temperatures are
173 inferred to range from 715 – 820 °C based on Fe-Ti oxides, generally increasing from
174 earlier- to later-erupted material, with the lower ignimbrite (Ig1) less than approximately 765

175 °C (Hildreth and Wilson 2007). Along the Owens Gorge, welding rank varies from non-
176 welded to densely welded. Proximal and distal sections are dominated by non-welded or
177 sintered ignimbrite. Medial sections are dominantly welded to densely welded ignimbrite,
178 with heterogeneous welding patterns associated with the two main ignimbrite flow packages
179 (Ig1 and Ig2; Wilson and Hildreth 2003).

180 Providing contrast to the Whakamaru and Bishop deposits, the ~8 Ma Grey's Landing
181 ignimbrite is part of the 10.6-8 Ma Rogersons Formation in southern Idaho (Fig. 1C; USA),
182 and representative of SRP-type ignimbrites (Fig 1; Branney et al. 2008). Among other
183 features, the Grey's Landing ignimbrite preserves unusually intense welding and
184 rheomorphism associated with a relatively dry magma and high eruption temperature (900-
185 1000 °C: Andrews et al. 2008; Ellis et al. 2010). The Grey's Landing ignimbrite shows
186 variations in thickness from 3 to 75 m, reflecting the underlying paleotopography (Andrews
187 and Branney 2011; Ellis et al. 2015). The 50 m thick Backwaters section of the Grey's
188 Landing ignimbrite has 2-3 m of black, glassy basal vitrophyre, transitioning rapidly into 45
189 m of crystalline ignimbrite with rheomorphic flow banding, and topped with a thin upper
190 vitrophyre. This material is now correlated with deposits in other areas to yield a proposed
191 volume of 2800 km³ (Knott et al. 2020).

192

193

METHODS

194 Samples from the Whakamaru, Bishop, and Grey's Landing ignimbrites are used here.
195 New analytical results are combined with literature data to provide a more comprehensive
196 assessment of the three deposits. A summary of analytical approaches for each sample is
197 detailed in Supplementary Table 1.

198 **Sampling sites and materials**

199 Whakamaru samples used for this study were collected adjacent to Maraetai dam on
200 the Waikato River, New Zealand (Figs. 1A and 2). For stratigraphic and lithologic
201 descriptions of the full Whakamaru section (only accessible with drill core) see Martin
202 (1965). Thirteen samples were collected at semi-regular intervals through the near continuous
203 ~50 m thick section exposed adjacent to the Maraetai power station. Sample numbers 16MD-
204 1 to 16MD-9 were collected along a single road exposure immediately below the dam. An
205 additional four samples (16MD-11 to 16MD-14) were collected through a 14 m section
206 immediately above the dam along a separate road exposure (Sample 16MD-10 is not utilized
207 due to a higher degree of weathering and difficulty in placing it in stratigraphic context).
208 Sampling was intentionally targeted to coincide with changes in fracture patterns,
209 qualitatively described based on their relative predominant orientation and measured spacing
210 (Fig. 2B). Effort was taken to obtain representative bulk samples at each locality, avoiding
211 surfaces with pervasive fracturing which may have experienced more significant vapor phase
212 alteration.

213 Bishop Tuff samples used for this study are from Wilson and Hildreth (2003) (Fig.
214 1B). Samples were collected from measured stratigraphic sections B, G, and H along the
215 walls of Owens Gorge, southeast of the caldera, presented in Wilson and Hildreth (2003)
216 (Fig. 1B; see simplified stratigraphic sections in Supplemental Figure 1). Sections G (132 m)
217 and H (134 m) have a similar stratigraphy, both encompassing roughly equal proportions of
218 ignimbrites Ig1Eb and Ig2Eb. However, section H includes ~5m of ignimbrite Ig2Ea and fall
219 deposits F8 and F9. Section B (162m) includes ~80 m of both Ig1Ea and Ig1Eb with ~ 1m of
220 fall deposit F6 midway through the section (Wilson and Hildreth 2003).

221 X-ray diffraction patterns from the Backwaters section of the Grey's Landing
222 ignimbrite presented in Ellis et al. (2015) are reprocessed here for quantitative mineralogy
223 and combined with backscattered electron (BSE) imaging. Groundmass crystallinity results

224 are from Ellis et al. (2015). Stratigraphy for this section is presented in Andrews and Branney
225 (2011) and Ellis et al. (2015). Samples through the Backwaters section were collected
226 generally every 4m through the crystalline core with increasing sampling density near
227 transitions to the upper and lower vitrophyre (Ellis et al. 2015).

228

229 **Imaging**

230 BSE images were collected from representative Whakamaru and Bishop (section G)
231 thin sections and polished 25 mm diameter epoxy rounds, respectively. Images were utilized
232 to identify groundmass textures and mineral phases (alkali feldspar and silica phases). For
233 image analysis the thin sections were either carbon-coated or gold-coated and analyzed with a
234 JEOL Neoscope JCM-6000plus Benchtop Scanning Electron Microscope (SEM) with an
235 energy dispersive spectrometer (EDS) at GNS Science, Wairakei Research Centre. Grey's
236 Landing ignimbrite BSE images were collected from carbon-coated polished 25 mm diameter
237 epoxy rounds, on a JEOL 8500F field emission -electron microprobe (FE-EMPA) at
238 Washington State University.

239

240 **Mineralogy**

241 Crystallinity measurements were made on a PANalytical Empyrean powder X-ray
242 diffractometer with a Cu X-ray tube ($\text{Cu K}\alpha_1$ 1.5406Å) at the University of Auckland.
243 Samples were analyzed from 5° to 50° 2 θ , with an integrated dwell time of 144 sec/step
244 (0.026° 2 θ step size) on a PIXcel 1D detector (strip detector) with attached graphite
245 monochromator (following the methodology of Zorn et al. 2015). Handpicked, phenocryst-
246 free groundmass, bulk ignimbrite, and sieved fines from Whakamaru ignimbrite samples
247 were analyzed following XRD preparation methodologies described by Rowe et al. (2012).
248 For Bishop ignimbrite samples, only phenocryst-free groundmass was analyzed following the

249 same methodology. Crystallinity from XRD patterns is determined using the statistical
250 freeware AMORPH (Rowe and Brewer 2008). Measured crystallinities are calibrated based
251 on a mixture of granite and glass, varying in 10% proportions (Fig. 3). A third-order
252 polynomial best fit is used for the calibration curve, accounting for the decrease in signal-
253 noise at low crystallinities (<10%), and apparent peak broadening resulting from overlapping
254 diffraction peaks at high crystallinities (>90%). Crystallinity methods for the Grey's Landing
255 ignimbrite samples are reported in Ellis et al (2015) and Supplementary Table 1, following
256 the procedure of Rowe et al (2012). Ellis et al. (2015) utilized the same basic methodology
257 employed in this study, except that background fitting was conducted manually using the
258 Jade software package, rather than with the AMORPH program.

259 Using the same diffraction patterns as for the crystallinity measurements, mineral
260 phases were identified from HighScore Plus software utilizing the Crystallography Open
261 Database (COD; e.g. Grazulis et al. 2009). Silica polymorphs were identified using reference
262 pattern number 96-900-8111 for cristobalite (Dollase 1965), pattern number 96-901-3394 for
263 tridymite (Konnert and Appleman 1978), and pattern number 96-101-1098 for quartz. In
264 sections identified as tridymite-bearing (Whakamaru and Bishop-G), phase proportions were
265 also calculated using an automated Rietveld refinement through HighScore Plus on samples
266 with a crystallinity greater than approximately 75%. Rietveld refinement is utilized to provide
267 a quantification of the variation in tridymite and cristobalite proportions (T/C) throughout the
268 stratigraphic sections. Ellis et al. (2015) identified the tridymite/cristobalite ratio from the
269 Grey's Landing ignimbrite as a qualitative value based on variation in peak height from X-
270 ray diffraction patterns, but we reprocessed their diffraction patterns using the Rietveld
271 refinement to provide a better comparison for this study. The Rietveld refinement does not
272 take into account the amorphous componentry so mineral proportions are recalculated using

273 AMORPH results (for Whakamaru and Bishop sections) and reported crystallinity values
274 from Ellis et al. (2015) for Grey's Landing.

275

276 **XRF analyses**

277 Major element compositions were determined from X-ray fluorescence (XRF) at the
278 University of Auckland on a PANalytical Axios 1-kW wavelength dispersive X-ray
279 fluorescence spectrometer (WDXRF) following procedures described in Zorn et al. (2018).
280 Powders for XRF analysis were also used for calculating loss on ignition (LOI) from heating
281 3.5g of powder for ~ 1 hour at 1000 °C.

282

283 **Density analyses**

284 As defined by Wilson and Hildreth (2003), density provides an analog to welding
285 rank. Densities of coherent (sintered to densely welded) ignimbrite from Whakamaru samples
286 were measured at GNS Science, Wairakei Research Centre, New Zealand. Dry, saturated
287 (wet), and particle densities, as well as apparent porosity, of each sample were measured
288 following the methodology of Hatherton and Leopard (1964). Weighing errors are reported at
289 ± 0.005 g. Two samples were run in duplicate and triplicate with calculated with standard
290 deviation of 0.005 and 0.025 g/cm³, respectively. Methods used for the Bishop Tuff density
291 samples, are reported in Wilson and Hildreth (2003) and in Supplementary Table 1. No
292 density data are available for the Grey's Landing ignimbrite samples.

293

294 **RESULTS**

295 **Field Observations**

296 Detailed field descriptions for the Bishop are in Wilson and Hildreth (1997), and
297 Andrews and Branney (2011) for the Grey's Landing ignimbrite. Lithologic and stratigraphic

298 descriptions for the Maraetai dam section of the Whakamaru ignimbrite are provided in
299 Martin (1965). Here we describe new exposure characteristics in support of mineralogical
300 observations, with an emphasis on fracture patterns in the Whakamaru ignimbrite. There are
301 distinctive broad differences in fracture patterns throughout the section which are stylistically
302 illustrated in Fig. 2. The lower section (below the dam, corresponding to the Maraetai
303 Ignimbrite of Martin 1965) has visible variations in the dominant orientation of fractures
304 through the section (Fig. 2). The lowest part shows large, columnar, continuous massive units
305 of densely welded ignimbrite (0 to 11 m stratigraphic height). A minor horizontal component
306 is present but poorly defined. The dominant fracture spacing at the base of this section is on
307 the order of 1.5 m, with regular smaller scale vertical fractures at an average spacing of 40
308 cm. Up-section, the fracture pattern becomes poorly defined, with neither horizontal nor
309 vertical components dominating. Sampling locations 16MD-2 and -3 show a transitional
310 phase, with irregular sub-vertical and sub-horizontal fractures. From approximately 11 to
311 16 m stratigraphic height the dominant fracture pattern follows a well-defined horizontal
312 trend. (Fig. 2B). Spacing between horizontal fractures is between 0.5 -1 m. At sample site
313 16MD-5 semi regular sub-vertical fractures reappear. Horizontal fracturing still dominates at
314 16MD-5 but is progressively lost between 16MD-5 and 16MD-8, with an increasing sub-
315 horizontal to sub-vertical fracture pattern. Sites 16MD-8 to -9 represent the uppermost
316 section of samples from below the dam and correspond to the Maraetai upper flow unit as
317 defined by Martin (1965) (Fig. 2A; Supplemental Figure 1). Large, massive blocks are
318 separated by thin vertical fractures with a minimum of 2 m spacing, suggestive of columnar
319 jointing (Fig. 2C).

320 In the upper section (above the Maraetai dam), the Whakamaru ignimbrite structures
321 are poorly defined and no horizontal jointing component is observed. Massive units are
322 separated by thin fractures spaced 5 to 5.5 m apart. Here, the rock is coherent but non-welded

323 and decreases in compaction upwards, as evidenced by the shapes of the pumice cavities
324 (increasingly elliptical to circular pumice upwards, compared to unobservable pumice in the
325 lower section). The ignimbrite colour of the upper section (pink) is also distinct from the
326 lower section (grey).

327

328 **SEM imaging**

329 Representative BSE images from the Whakamaru ignimbrite and Bishop section G
330 are provided in Figs. 4 and 5, respectively. Groundmass textures show evidence of both
331 devitrification (within glass) and vapor phase alteration (within voids) (Fig. 4, 5). The
332 granophyric textures within the glass are most highly developed in sample 16MD-5, with a
333 finer grain size (less mature texture) in samples 16MD-2 and 16MD-9 (Fig. 4). Alkali
334 feldspar has a characteristic axiolitic texture in shards as well as displaying a feathery texture
335 where growing into void space (Fig. 4B,D,H). In the interior of relict glass shards, alkali
336 feldspar and a silica phase (cristobalite or tridymite) are intergrown in a graphic texture (e.g.
337 Fig. 4F). Note, we refer to a silica phase here rather than specifically to cristobalite or
338 tridymite as these are not distinguishable from our BSE images or EDS. Samples 16MD-9
339 and 16MD-12 have a greater proportion of vapor phase alteration, coincident with the lower
340 apparent compaction compared to samples 16MD-5 and 16MD-2 (Fig. 4). Grain forms in the
341 devitrified texture are predominantly nondescript, with blocky morphologies for silica phases,
342 interspersed with alkali feldspar.

343 Distinct variations are evident through the Bishop section G samples (Fig. 5). In the
344 lowest part of the section (BR-089), the ignimbrite is densely welded. Although porous,
345 individual glass shards are not easily identifiable. Devitrification of the glassy matrix has
346 resulted in a fine granophyric texture, with streamers of the silica phase interspersed through
347 larger regions of alkali feldspar (Fig. 5F). Although less welded, there is an apparent greater

348 separation of silica phases and alkali feldspar in sample BR-086, with silica phases elongated,
349 parallel to the length of the glass shards, and surrounded by alkali feldspar (Fig. 5D). A
350 similar but less well developed texture is evident in sample BR-083. Both BR-086 and -083
351 show evidence for increased vapor-phase alteration: however, like the upper section of the
352 Whakamaru, this is coincident with a decreased density in these samples.

353 In the Grey's Landing ignimbrite BSE images, all images correspond to the
354 crystalline interior of the ignimbrite, ranging in stratigraphic height from 4 to 48 m (Fig. 6).
355 There is a systematic coarsening of the devitrification texture (alkali feldspar and silica
356 phase), with the development of elongate silica phase minerals, toward the interior of the
357 ignimbrite (Fig. 6B-D). Foliation is also evident in the uppermost ignimbrite samples (e.g. 48
358 m) with an apparent alignment of iron-oxides (Fig. 6F). Given the lack of porosity and
359 identifiable relict pyroclastic textures, there is no visual evidence of vapor-phase alteration.
360 The Grey's Landing BSE images display a distinctly different texture when compared to both
361 the Bishop and Whakamaru ignimbrite samples (Figs. 4-6). Although a micro-vesicularity is
362 unevenly present through the samples, overall the ignimbrite displays a higher degree of
363 compaction and welding when compared to the Bishop and Whakamaru deposits.

364

365 **Silica polymorphs**

366 Silica polymorphs (cristobalite, tridymite, quartz), are identified based on X-ray
367 diffraction patterns of ignimbrite samples. Overall, cristobalite and tridymite account for
368 between 25-33% of crystalline phases in all sampled units (Tables 1 and 2; Supplementary
369 Table 2). The proportions of cristobalite and tridymite are negatively correlated, however: as
370 tridymite abundances increase, cristobalite decreases consistently in all three sections where
371 tridymite is observed (Fig. 7). Cristobalite is a significant groundmass component (evidenced
372 by prominent peaks at 21.947° and $36.056^\circ 2\theta$; Fig. 8A) in all Whakamaru ignimbrite

373 samples, averaging 24 ± 5 %. Tridymite, most easily identified by its XRD peak at $20.6^\circ 2\theta$,
374 is most abundant within <11 m thickness of the stratigraphic section, primarily in samples
375 16MD-3b (15 m section height) to 16MD-5b (21 m section height) varying from 1.5 to 15 %,
376 with lesser proportions of 1.2 % in 16MD-7 (31 m section height) and $<1\%$ above 16MD-8
377 (41 m section height). Low abundances of tridymite (less than $\sim 1\%$) are unresolvable based
378 on appearance of distinct diffraction peaks and are only identified from Rietveld refinement.
379 The tridymite/cristobalite (T/C) ratio varies significantly over this stratigraphic range, with a
380 maximum relative T/C ratio of 1.3 at 18 m height (Fig. 9).

381 Bishop Tuff sections B, G, and H (Fig. 1) each have substantial differences in their
382 silica polymorphs. Quartz, which occurs in all the Bishop samples as a major phenocryst
383 component, is commonly observed in varying proportions in the diffraction patterns, likely
384 representing microphenocrysts in the groundmass (Hildreth, 1979). Quantified during
385 Rietveld refinement, in section G quartz concentrations vary from 0.3-1.5%. In section B, all
386 samples with $<20\%$ groundmass crystallinity lack XRD evidence of either cristobalite or
387 tridymite (Fig. 8D). The 100%I ($21.947^\circ 2\theta$) cristobalite peak overlaps with phenocryst
388 phase Na-rich plagioclase feldspar (e.g. oligoclase; Hildreth, 1979) and the cristobalite 14%I
389 peak at $36.056^\circ 2\theta$ is notably missing in these cases (Fig. 8D, samples BR159-B and BR145-
390 B). Thus, the diffraction peak at $21.7^\circ 2\theta$ is most likely associated with Na-rich plagioclase
391 feldspar.

392 Excluding the upper vitrophyre, all analysed samples from section H contain
393 significant amounts of cristobalite, and tridymite is notably absent. In section G, cristobalite
394 is present in all samples, however unlike in section H, tridymite is also evident in samples
395 BR-085 to -087, from 74 to 77 m in the section (Fig. 9; Wilson and Hildreth 2003).
396 Cristobalite concentrations in section G are relatively constant ($30 \pm 2\%$) in samples where
397 tridymite is absent, but decrease to $\sim 15\%$ as tridymite proportions increase (Fig. 8). The T/C

398 ratio reaches a maximum of 1.0 from 74 to 76 m stratigraphic height then decreases rapidly
399 up section. A large gap in available samples in the stratigraphic section from 56 to 74 m
400 precludes an assessment of the symmetry of the T/C ratio in this section, especially given the
401 relatively narrow range over which the ratio decreases up section (Fig. 9).

402 Cristobalite is ubiquitous in Grey's Landing samples (excluding upper and lower
403 vitrophyre), with concentrations varying from ~10-30%. Tridymite is observed through most
404 of the stratigraphic sequence, from 8-36 m stratigraphic height and varies from 0 to 20%,
405 resulting in a T/C ratio of 0 to 1.9 (Fig. 9). Tridymite is more widespread and its proportions
406 greater than observed in either the Whakamaru or Bishop section G.

407

408 **Crystallinity**

409 Crystallinity measurements from the Whakamaru (Maraetai dam section) ignimbrite
410 predominantly record highly crystalline conditions. Both whole rock and separated fines have
411 crystallinities almost exclusively >90% (Supplemental Table 3). Whole rock crystallinities
412 remain above 95% except in the uppermost ~10 m of samples (16MD-WR-11 to 16MD-WR-
413 14), consistent with less welding and compaction from field observations in those samples
414 (Fig. 4, 9). Groundmass crystallinity is up to 15% lower than whole rock crystallinity,
415 ranging from 71 to 94% and generally decreasing up section. Full crystallinity results
416 processed through AMORPH are available in Supplemental Table 3 and summarized for
417 groundmass analyses in Table 1.

418 Only groundmass crystallinity was measured from the Bishop sections (G, H, B; Figs.
419 9, 10). Section B is primarily glassy, with crystallinities varying from 3-44%, with only 30%
420 of the analyzed samples having groundmass crystallinities >20%. Sections G and H have
421 crystallinities more similar to the Whakamaru section. Section H ranges from 59-94%,

422 excluding an upper vitrophyre with 3% groundmass crystallinity, while Section G
423 groundmass crystallinity varies from 75 to 93% (Tables 1 and 2).

424 Whole rock and groundmass crystallinity of the Grey's Landing ignimbrite samples
425 are reported in Ellis et al. (2015). Within the crystalline core of the ignimbrite, groundmass
426 crystallinities vary from 76 to 93%, while glassy vitrophyre ranges only from 4 to 16%,
427 creating a bimodal crystallinity distribution (Table 1). There is no systematic variation in
428 groundmass crystallinity through the crystalline core of the ignimbrite, and transitions
429 between the core and the vitrophyre are sharp.

430

431 **Major element composition**

432 Major element compositions for the Whakamaru ignimbrite show no systematic
433 variation along its stratigraphy (Table 3). LOI values are generally <1 wt% (excluding an
434 outlier value of 2.1 wt% in sample 16MD-6) between samples 16MD-1 and 16MD-8.
435 Upwards, in samples 16MD-9 to 16MD-14, LOI values increase to a maximum of 3.4 wt%.

436

437 **Density and Porosity**

438 Density measurements of the Whakamaru ignimbrite samples vary from 2.16 to 1.53
439 g/cm³ (Table 1; Supplemental Table 4). Similar bulk densities for samples 16MD-1 to
440 16MD-7 yield an average of 2.11 ± 0.03 g/cm³. Stratigraphically above sample 16MD-7
441 densities decrease to the break in section with 16MD-9 at 1.80 g/cm³. In the upper
442 Whakamaru section, densities vary from 1.53 to 1.66 g/cm³. Apparent porosities are
443 negatively and linearly correlated to density, ranging from 17 to 39.3% (Supplemental Table
444 4). Porosities are constant from 15 to 20% in the lowermost samples (16MD-1 to 16MD-7),
445 increasing to 30% to the top of the lower section (below the dam), and then consistently

446 range from 35-39% in the upper section (above the dam). Henceforth, we utilize only density
447 values from the Whakamaru ignimbrite to provide a direct correlation to the Bishop samples.

448 Densities for Bishop samples are variable through the sections with a total range from
449 1.22 to 2.34 g/cm³ (Tables 1 and 2; Wilson and Hildreth 2003), where sections G and H have
450 similar density profiles, with densities >2 g/cm³ near the base of the section then density
451 minima above the contact between ignimbrite Ig1Eb and Ig2Eb, and at the top of Ig2Eb
452 (Figs. 9 and 10)10. Clast densities for section B are initially low (<1.8 g/cm³), increase across
453 the contact between Ig1Ea and Ig1Eb (and inter-bedded fall deposit), reach a maximum of
454 2.07 g/cm³ and then decrease to the top of the section (Fig. 10).

455

456

DISCUSSION

457 **Tridymite and cristobalite in ignimbrites**

458 Both tridymite and cristobalite are present in all three ignimbrite sections: however,
459 the relative distribution is different between the Whakamaru, Bishop, and Grey's Landing
460 ignimbrite. In welded materials, cristobalite is the dominant silica polymorph, ubiquitous in
461 the Whakamaru and Grey's Landing ignimbrite samples and common in sections G and H of
462 the Bishop, while tridymite is relatively rare. It is the scarcity of tridymite in these cases that
463 provides an opportunity to refine models of deposition, cooling, and crystallization. In the
464 following discussion, endmember examples of the distribution of tridymite relative to other
465 ignimbrite properties are detailed using the Bishop and Grey's Landing ignimbrite sections.
466 This is followed by discussion of the distribution of tridymite in the less-constrained
467 stratigraphic context of the Whakamaru ignimbrite.

468 The occurrence of tridymite in the Bishop ignimbrite (section G) is over a very
469 narrow region (~3 m) and corresponds to the contact between ignimbrites Ig1Eb and Ig2Eb
470 (Fig. 9; Wilson and Hildreth 2003). However, the rock density decreases consistently over

471 this lithologic contact and the actual density minimum is located above/outside of the
472 tridymite zone (Fig. 9). Notably in Bishop section G, a decrease of ~10 vol% groundmass
473 crystallinity corresponds to the lithologic contact between ignimbrite packages (uncorrelated
474 to sample density: Fig. 9). Despite the change in groundmass crystallinity over the tridymite
475 zone, there is no correlation between the T/C ratio, or tridymite abundance, to the
476 groundmass crystallinity or density. This suggests that the important variable here in
477 regulating the appearance and proportion of tridymite is not the groundmass crystallinity or
478 density, but the presence of lithologic contacts between ignimbrite emplacement packages.

479 The other Bishop sections (B, H) portray a range of different features which allow us
480 to evaluate the occurrence of tridymite in section (G). Bishop section H has almost an
481 identical density and groundmass crystallinity profile to Bishop section G (Figs. 9 and 10). In
482 addition, field evidence indicates a wide zone of vapor-phase alteration in Ig2Eb above the
483 fall horizon in section H (Wilson and Hildreth 2003). However, importantly, there is no
484 tridymite observed in section H, despite the field evidence for vapor-phase alteration. The
485 only significant variation in these two sections is structural; section H contains ~5 m of
486 ignimbrite Ig2Ea and parts of fall units F8 and F9 sandwiched between the more massive
487 Ig1Eb and Ig2Eb ignimbrite packages (Fig. 10). This would suggest that the presence of the
488 fall units (and minor ignimbrite) reflects an altered cooling and degassing history, inhibiting
489 the formation of tridymite at the lithologic contact in this section.

490 Bishop section B has markedly different density and crystallinity profiles to sections
491 G and H. Densities (<2 g/cm³) and groundmass crystallinities (<40 vol %) are generally
492 lower. However, these parameters are positively correlated, largely driven by differences in
493 density and crystallinity between the two ignimbrite packages (Ig1Ea and Ig1Eb), with higher
494 densities and groundmass crystallinities observed in Ig1Eb compared to the glassy Ig1Ea
495 unit. Because of the overall low crystallinity in both units, it is impossible to accurately

496 distinguish the cristobalite and feldspar peaks from the XRD results. However, no lower
497 intensity cristobalite peaks are evident at higher 2θ in the X-ray patterns. Similarly, no
498 tridymite is identified in any of the section B samples. These results support limited vapor-
499 phase alteration or devitrification, and only in higher density samples in Ig1Eb.

500 The single, densely welded rheomorphic Grey's Landing ignimbrite provides a
501 distinctive contrast to the multiple flow packages and fall deposits of the Bishop Tuff. In
502 contrast to the Bishop sections, tridymite is present in ~60% of the 45 m thick crystalline core
503 of the ignimbrite. The abundances of tridymite (and T/C ratios) are not symmetrical through
504 the ignimbrite but rather are skewed toward the lower half of the deposit (Fig. 9). While this
505 matches numerical models of cooling profiles (Ellis et al. 2015), it clearly does not take into
506 account the relative movement of these phase transitions as a result of compaction in the
507 rheomorphic ignimbrite. Interestingly, the coarsest groundmass textures (Fig. 6) do not
508 correlate to the highest proportion of tridymite in the groundmass (Fig. 9), suggesting that the
509 proportion of tridymite is not simply a function of cooling rate.

510 In the Whakamaru ignimbrite, tridymite is observed roughly two-thirds of the way up
511 section (from the base; Fig. 11; Supplemental Figure 1). The two competing possible
512 interpretations of flow packages and welding in this section affect the consideration of
513 tridymite growth in relation to ignimbrite emplacement (Martin 1965; Briggs 1976b). XRF
514 analyses are inconclusive in differentiating potential flow packages, and LOI measurements,
515 with one exception, are all low (less than 1 wt%; Table 3) through the lower ~57 m of the
516 section, gradually increasing upwards into the upper Whakamaru ignimbrite. As the tridymite
517 zone corresponds to the horizontal jointing, this therefore implies that the tridymite zone may
518 occur at a contact between flow packages (Martin 1965) or approximately midway through
519 subunit D (Briggs 1976b; Brown et al. 1998), the former paralleling the distribution in the
520 Bishop Tuff and the latter more consistent with the distribution in the Grey's Landing

521 ignimbrite. However, as Whakamaru subunits A-E (Briggs 1976b) have been proposed to
522 represent a single cooling unit, the distribution of tridymite within the cooling unit as a whole
523 is inconsistent with the Grey's Landing ignimbrite crystallization pattern. Regardless of the
524 structural model, however, we note the key observation is the correlation between the
525 horizontal/sub-horizontal fracture patterns and the emergence of the tridymite zone (Figs. 9
526 and 11).

527 The change in fracture pattern also corresponds to irregular variations in groundmass
528 crystallinity, varying from 90% to 100%. Tridymite occurrences up-section are
529 predominantly in samples from the sub-horizontal to horizontal fracture pattern zones
530 (16MD-3b) but extend up through the transition zone until fractures return to a sub-vertical
531 predominant pattern (16MD-7; Fig. 2). Although the maximum T/C ratio is observed within
532 the zone dominated by pervasive horizontal fractures, these ratios slowly decrease up through
533 overlying ignimbrite (Fig. 9). Density values show no obvious correlation to the appearance
534 of tridymite and are constant ($\sim 2.1 \text{ g/cm}^3$) through the tridymite-bearing zone. Similarly,
535 despite the variations in groundmass crystallinity over this critical zone ($\sim 10 \text{ vol}\%$), there is
536 no clear correlation to the proportion or occurrence of tridymite (Fig. 9). However, despite
537 textural complexities evident in BSE imaging, we do note that the tridymite zone corresponds
538 to a coarser-grained devitrification texture (Figs. 4E-F and 5C-D). Field observations,
539 textures, crystallinity and density measurements all indicate that localized processes, such as
540 gas pressure or permeability, control the distribution of tridymite in the ignimbrites.

541

542 **Mechanisms of tridymite formation**

543 The stability or metastability of tridymite is largely a function of temperature and the
544 availability of alkali oxides and water (e.g. Fenner 1913; Garofalini and Miller 1986; Stevens
545 et al. 1997). In the following discussion we first examine the potential formation of higher-

546 temperature stable tridymite in the Grey's Landing section, and then examine lower-
547 temperature metastable tridymite formation in both the Bishop and Whakamaru sections.

548 Assuming availability of alkalis, at magma temperatures suggested by Fe-Ti oxides
549 for the studied ignimbrites (Brown et al. 1998; Hildreth and Wilson 2007; Andrews et al.
550 2008; Matthews et al. 2012), only the Grey's Landing ignimbrite (>900 °C) has the potential
551 to form stable β -tridymite (e.g. Fenner 1913). Ellis et al. (2015) suggest that tridymite
552 occurrences in the rheomorphic Grey's Landing ignimbrite correlate to cooling rates of the
553 ignimbrite. However, this depends on the mechanism of tridymite formation. As discussed
554 above, the densely welded texture with minimal micro-porosity of the Grey's Landing
555 ignimbrite (Fig. 4) favors the formation of silica polymorphs through devitrification as
556 opposed to pervasive vapor-phase alteration. If stable β -tridymite is forming during
557 devitrification, this must occur rapidly after emplacement, before temperatures drop below
558 ~870 °C. Andrews and Branney (2011) suggest textures indicate cooling through the solidus
559 before reaching a calculated glass transition temperature of ~725 to 525 °C (from dry to 1
560 wt% H₂O, respectively). A maximum cooling time (slowest cooling rate) from numerical
561 modelling suggests the Grey's Landing ignimbrite interior would reach temperatures below
562 ~870 °C after approximately 2.5 years (Ellis et al. 2015), after which quartz would constitute
563 the stable silica polymorph. However, thermal heterogeneities, vertical fracturing, and any
564 influx of meteoric or surface water all will decrease this cooling time (e.g. Keating 2005;
565 Randolph-Flagg et al. 2017). The presence of cristobalite, and lack of tridymite, at the top
566 and bottom of the Grey's Landing ignimbrite section is explained by results from
567 crystallization experiments, which demonstrate cristobalite is formed as a metastable phase in
568 the cooling-related phase transitions from amorphous volcanic glass (silica-rich) to tridymite
569 (Wu et al. 2002).

570 Similar observations of “magmatic” or primary tridymite were suggested for high-
571 temperature rheomorphic ignimbrites and rhyolitic lavas from the Keweenawan Midcontinent
572 Rift (USA: Green and Fitz 1993) and the Harvey volcanics (New Brunswick, Canada: Payette
573 and Martin 1986). Rowe et al. (2012) also recognized high proportions of tridymite
574 throughout the Tuff of Knob, another high-temperature SR-type ignimbrite. They suggested
575 however that, based on the presence of quartz as well, the tridymite was metastable. The
576 limited presence of quartz may also be explained by the slow kinetics associated with
577 structural changes from tridymite to quartz (e.g. Gibbs 1926).

578 Alternatively, if devitrification is a slower process, occurring after significant cooling,
579 then tridymite would likely form as a metastable phase (<870 °C). At this point, the transition
580 from metastable cristobalite to tridymite would reflect the longer duration of cooling.
581 Although both metastable phases will nucleate together, their relative proportion will change
582 from cristobalite-dominant to tridymite-dominant, resulting from the faster initial
583 crystallization rate of cristobalite, followed by its transformation to tridymite (Madden and
584 Van Vlack 1967; Garofilini and Miller 1986; Wu et al. 2002).

585 Tridymite is commonly associated with vapor phase alteration (Caporuscio et al.
586 2012) or extending cooling times beneath the glass transition temperature (Ellis et al. 2015).
587 BSE images from both the Bishop section G and Whakamaru ignimbrite samples suggest a
588 combination of devitrification and vapor-phase alteration accompanied tridymite growth
589 (Figs. 4 and 5). As discussed above, regardless of the mechanism of formation, due to the
590 lower temperatures of the Bishop Tuff and Whakamaru ignimbrite tridymite will be
591 metastable.

592 In the Bishop Tuff section G, there is no significant change in crystallinity in the
593 tridymite zone compared to the ignimbrite above or below it (Fig. 4), indicating that the
594 appearance of tridymite does not appreciably increase the overall groundmass crystallinity.

595 Importantly, as the proportion of tridymite increases, we see a corresponding linear decrease
596 (with a slope of -1) in the proportion of cristobalite (Fig. 7). This change in relative
597 proportions of silica polymorphs, without a corresponding change in groundmass
598 crystallinity, suggests a phase transition from cristobalite to tridymite. We see a similar
599 correlation in the Whakamaru section, where samples 16MD-2 and 16MD-3 both have
600 groundmass crystallinities greater than 90%, greater than or comparable to the groundmass
601 crystallinity in the tridymite zone (Fig. 9). Despite this, we see the same negative correlation
602 between tridymite and cristobalite correlation suggesting the tridymite formation comes at the
603 expense of cristobalite (Fig. 7B).

604 Within the Bishop, the localization of tridymite to the direct contact between Ig1Eb
605 and Ig2Eb implies a structural characteristic of the ignimbrite or its emplacement history
606 around this contact is what regulates the presence of tridymite. A model describing thermal
607 and gas pressure fluctuations for two 50 m thick ignimbrites (emplaced 20 days apart in this
608 model) suggest that for at least the first two months, the maximum gas pressure will coincide
609 with the lithologic contact, but that the pressure rapidly decreases after emplacement (Riehle
610 2015). In contrast, results of the thermal model suggests that the maximum temperature after
611 up to 4 years is at the lithologic contact between ignimbrites (Riehle 2015). However, neither
612 of these two models is appropriate for the Bishop Tuff because of the evidence for rapid
613 emplacement of the flow packages together with their coeval fall deposits (Wilson and
614 Hildreth 2003). As discussed above, the primary difference in sections G and H is the
615 presence of fall deposits and ignimbrite making an approximate 5 m-thick high porosity
616 transition between denser welded ignimbrite packages. We propose that the upper denser-
617 welded tuff (Ig2Eb) served as a sealant for gas escape from the lower ignimbrite but that the
618 interbedded fall deposits in section H served as a permeable, laterally continuous bed to keep
619 vapor pressure reduced. Thus in contrast, high gas pressure near the Bishop flow package

620 contact in section G facilitated tridymite precipitation while high temperatures promote
621 increased devitrification (Keating 2005). Despite the origin of the horizontal fractures in the
622 Whakamaru, corresponding to either a change in welding (Briggs 1976a,b) or a flow package
623 contact (Martin 1965) we propose that this change in jointing with overlying thick ignimbrite
624 served to restrict gas escape in a similar fashion as observed in the Bishop G section (Fig.
625 11).

626 An alternative model to explain tridymite crystallization along the flow package
627 boundaries is through post-depositional hydrothermal circulation, where geothermal fluids
628 utilize laterally continuous zones of higher permeability (Bignall et al. 2010). However,
629 vapor-phase mineral growth and devitrification are the only textures evident related to
630 secondary mineralization (Figs. 4 and 5). There is no evidence for more widespread
631 silicification, a change in major element composition, or a change in density/porosity
632 associated with tridymite deposition compared to cristobalite-only samples (Fig. 9).
633 Similarly, since tridymite appears to form directly at the expense of cristobalite, our
634 observations are unlikely to relate to a separate hydrothermal alteration event (Fig. 7B).
635 Lastly, there is no evidence of low temperature hydrolysis reactions in the form of secondary
636 hydrous phases such as clays (Fig. 8). All of these factors point to tridymite formation
637 associated with initial cooling and degassing of the ignimbrites. Thus, we predict that
638 tridymite, formed predominantly through vapor-phase alteration, serves as a potential
639 fingerprint for horizontal structures or lithologic contacts with initial higher porosities,
640 capable of localizing prolonged crystallization prior to compaction to the modern state.

641

642

IMPLICATIONS

643

644 The occurrence and distribution of tridymite in the Grey's Landing, Bishop, and
Whakamaru large silicic ignimbrites are highly variable. Unlike the widespread distribution

645 of cristobalite in volcanic rocks, our results imply that tridymite crystallization is dependent
646 on emplacement temperature and localized conditions promoting trapping of gas phases and
647 slow cooling.

648 At one extreme, high temperature ignimbrites (>870 °C) such as Grey's Landing have
649 the potential to preserve stable tridymite, crystallizing rapidly under high temperature
650 conditions shortly after emplacement. In these instances, tridymite abundances and T/C
651 ratios, in conjunction with geothermometry and groundmass textures, may preserve an
652 ignimbrite thermal history, with the variations in T/C ratios recording a cooling profile.
653 Coupled with numerical thermal models or chronometers (Ellis et al. 2015, 2018), T/C
654 variations have the potential to inform maximum timescales of devitrification.

655 Under lower temperature conditions (<870 °C) tridymite exists as a metastable phase.
656 The occurrence of tridymite in the welded Whakamaru and Bishop (section G) ignimbrites, is
657 limited to interpreted lithologic boundaries, in particular, contacts between flow packages.
658 We propose that: 1), upper denser-welded material serve as seals, trapping degassing volatiles
659 from lower flow packages, and 2) contacts initially serve as short-lived permeable zones,
660 preserving conditions for tridymite vapor-phase crystallization, whereas the lower
661 permeability of the upper material must inhibit vapor-phase tridymite formation. In
662 ignimbrites either lacking a seal (Bishop section B), or in the case of Bishop section H,
663 containing an interbedded and highly permeable fall deposit, gas pressures are not maintained
664 to promote tridymite formation. These results imply a new methodology for assessing syn-
665 and post-emplacement petrogenetic processes in an important but relatively minor
666 mineralogical component.

667 One outgrowth of this study arises from the observation that welded ignimbrites are
668 the dominant rock type in numerous geothermal reservoirs associated with silicic volcanic
669 systems (e.g. Taupo Volcanic Zone, New Zealand; Coso Hot Springs, U.S.A.; Kyushu

670 Japan). Beyond volcanological implications, one of the initial drivers of this research was to
671 understand if there exists a relationship between changing fracture patterns and groundmass
672 mineralogy that could improve understanding of fluid flow in the Whakamaru ignimbrite
673 where it forms a geothermal reservoir rock (e.g. Milicich et al. 2018). Laterally continuous
674 permeable zones both within and between ignimbrite formations are recognized as important
675 controls of fluid flow (Bignall et al. 2010). However, Milicich et al. (2018) highlight the
676 challenge of identifying stratigraphic sequences from drill cuttings in geothermal wells. Our
677 results from moderate-temperature welded ignimbrites (Bishop and Whakamaru) suggest that
678 tridymite is localized to contacts between pyroclastic flow packages. At least in the case of
679 the Whakamaru section at Maraetai, we see that this contact coincides with a distinctive
680 reorientation of dominant fracture patterns to horizontal, and thus the potential for localized
681 changes to permeability and fluid flow regimes in a reservoir host stratigraphy (Fig. 2). While
682 further testing on geothermal well cuttings is required, tridymite may prove to be a useful
683 mineralogical tracer of depositional contacts in silicic geothermal reservoirs.

684

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855

856 FIGURE CAPTIONS

857 Figure 1: Location maps of (A) Maraetai Dam locality of the Whakamaru ignimbrite, New
858 Zealand; (B) Owens Gorge sections B, G, and H of the Bishop ignimbrite from Wilson and
859 Hildreth (2003); and (C) the Backwaters section of the Grey's Landing ignimbrite, central
860 Snake River Plain, USA modified from Ellis et al. (2015). Ignimbrites indicated in gray.

861 Figure 2: (A) Illustrative section of fracture patterns with field observations and
862 corresponding sampling sites. Field photos of Whakamaru welded ignimbrite at Maraetai
863 Dam illustrating (B) horizontal fracturing at sampling site 16MD-4 and (C) vertical fracturing
864 at sampling site 16MD-8 (examples of fracture patterns highlighted by white arrows).

865 Figure 3: AMORPH calibration curve for crystallinity measurements. Actual crystallinity (y-
866 axis) from weighed components of amorphous glass and mineral powders. Error bars on data
867 points represent one standard deviation of repeated cycles of AMORPH pattern
868 deconvolution and resultant crystallinity determination (Rowe and Brewer 2018). The third-
869 order polynomial best fit line accounts for peak overlap at high crystallinity and increased
870 difficulty distinguishing signal from noise at low crystallinity.

871 Figure 4: Low and high magnification SEM BSE images of Whakamaru groundmass textures
872 from samples 16MD-12 (55 m; A-B), 16MD-9 (49 m; C-D), 16MD-5 (20 m; E-F), and
873 16MD-2 (5 m; G-H). White arrows in (B) and (H) denote vapor-phase crystallization within
874 void spaces, while arrows in (F) denote examples of devitrification.

875 Figure 5: Low and high magnification SEM BSE images of Bishop section G groundmass
876 textures from samples BR083 (86 m; A-B), BR086 (76 m; C-D), and BR089 (56 m; E-F).
877 Arrows in (A) denote vapor-phase crystallization along pumice clast margins, while (D)

878 exemplifies devitrification. White arrows in (E) point out examples of “silica streamers” as
879 discussed in the text.

880 Figure 6: BSE images through the Grey’s Landing section demonstrating the coarsening of
881 texture towards the interior of the flow. Images were collected at 4 m (A), 8 m (B), 16 m (C),
882 24 m (D), 36 m (E), and 48 m (F). Relatively coarse alkali feldspar and silica phases are
883 annotated in (D) while alignment (foliation) of oxide phases is annotated in (F). The scale bar
884 in all images is 10 μm .

885 Figure 7: (A) Enlargement of key peaks associated with tridymite from X-ray diffraction
886 patterns for Whakamaru samples ($20\text{--}22.5^\circ 2\Theta$) illustrating changing peak heights of
887 tridymite and cristobalite diffraction peaks as proportions change. (B) Rietveld refinement
888 results for silica polymorphs cristobalite and tridymite demonstrating the decrease in
889 cristobalite with increasing tridymite in 1:1 proportions for all three tridymite-bearing
890 sections.

891 Figure 8: Representative X-ray diffraction patterns from (A) the Whakamaru ignimbrite and
892 (B-D) Bishop sections G, H, and B. Diffraction patterns in red are from the contact between
893 major flow packages, or in the case of the Whakamaru ignimbrite, horizontal fracturing.
894 Diffraction patterns in black are stratigraphically below flow package contacts, and in grey
895 are above the contacts. Diffraction patterns are arbitrarily offset for viewing but have the
896 same scale. Dashed lines indicate the key tridymite diffraction peak used to identification at
897 $20.6^\circ 2\Theta$. Dotted lines in (A) and (D) refer to cristobalite 100% intensity (100%I) and 14%
898 intensity (14%I) peaks at 21.947° and $36.056^\circ 2\Theta$, respectively.

899 Figure 9: Density, groundmass crystallinity (C_{gm}), and relative proportions of tridymite and
900 cristobalite (T/C) with stratigraphic height for the Bishop Tuff section G (A-C), and
901 Whakamaru ignimbrite (D-F). Only groundmass crystallinity and T/C are presented for the

902 Grey's Landing ignimbrite (G-H) as corresponding density measurements are not available.
903 Tridymite zones are indicated in blue. Red stars indicate samples with corresponding BSE
904 images in Figs. 7-9. Long-dashed lines in A-C and D-F represent inferred lithologic contacts,
905 while the short-dashed line (D-F) represents the region of horizontal fracturing (see text for
906 more details). Ignimbrite emplacement units defined in Wilson and Hildreth (2003) and
907 Martin (1965) and summarized in supplemental figure 1. Density measurements from Bishop
908 section G from Wilson and Hildreth (2003).

909 Figure 10: Corresponding density and groundmass crystallinity (C_{gm}) measurements versus
910 stratigraphic height for the Bishop sections H (A-B), and B (C-D). Long-dashed lines
911 represent inferred lithologic contacts with ignimbrite and fall deposit nomenclature from
912 Wilson and Hildreth (2003) and summarized in supplemental figure 1. Density measurements
913 for Bishop sections from Wilson and Hildreth (2003).

914 Figure 11: Illustrative stratigraphic models of the Grey's Landing (A), Whakamaru (B), and
915 Bishop (C) ignimbrites, with major deformation or structural features indicated with
916 corresponding zones of tridymite crystallisation (blue). The Grey's Landing ignimbrite
917 schematic column is modified from Andrews and Branney (2011), while the Whakamaru
918 column is modified from Martin (1965) and Brown et al. (1998). The dashed line in (B)
919 represents the break in stratigraphy between before the upper Whakamaru flow package.
920 Estimated magmatic temperatures from Fe-Ti oxides (see text for details and references).

921

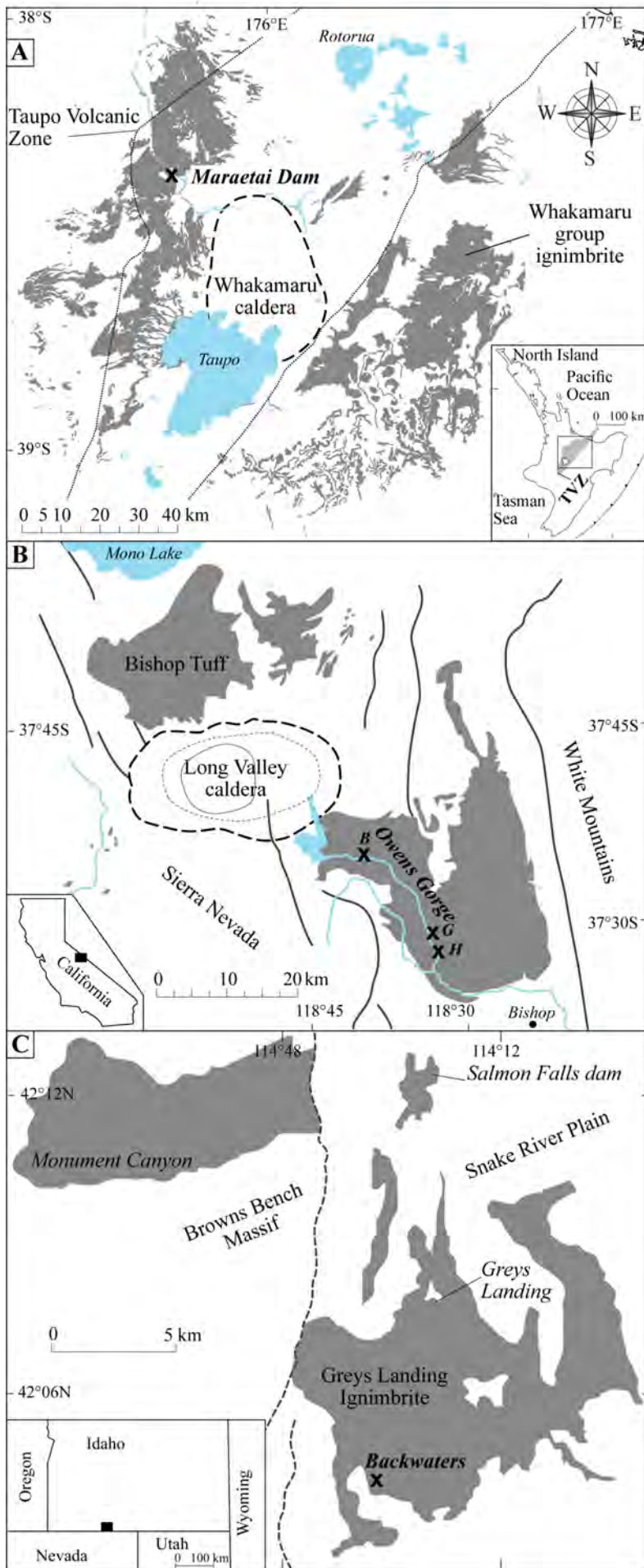
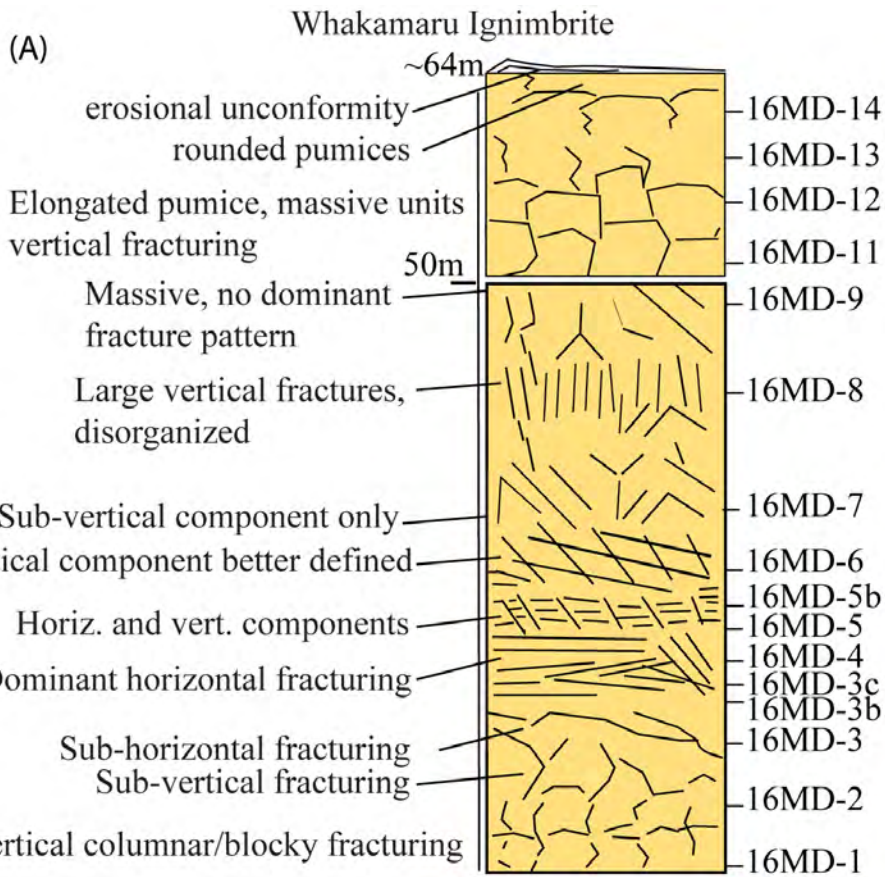
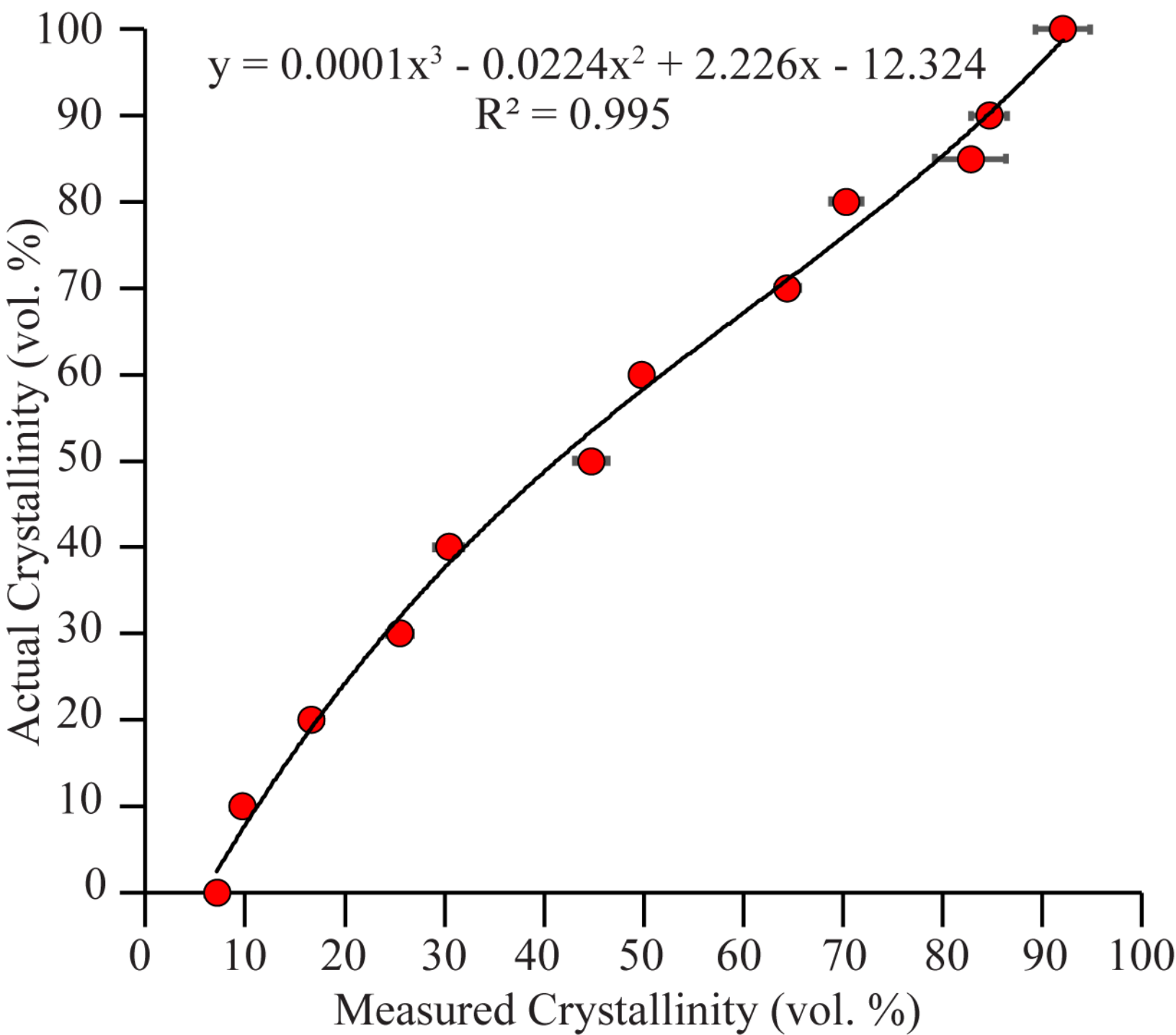
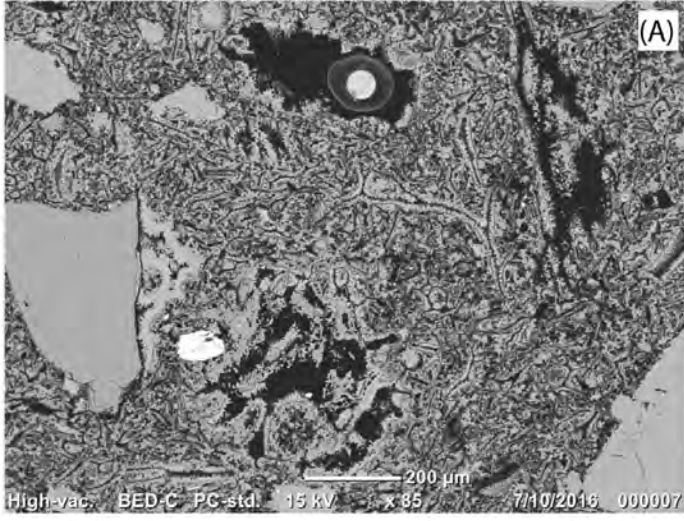


Figure 1

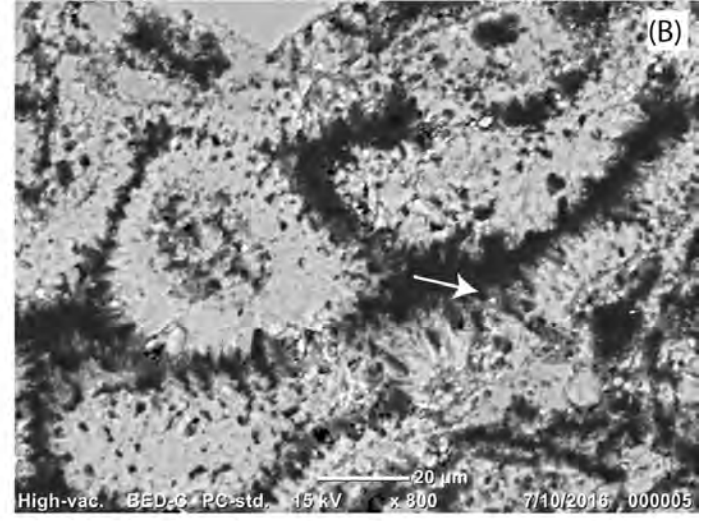




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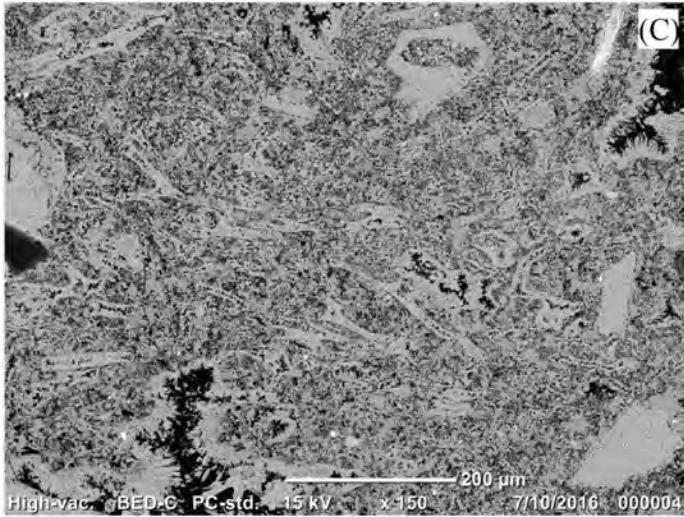


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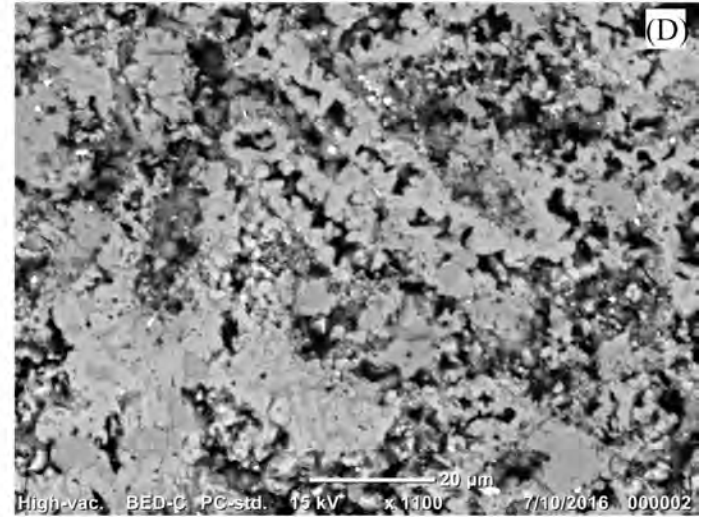


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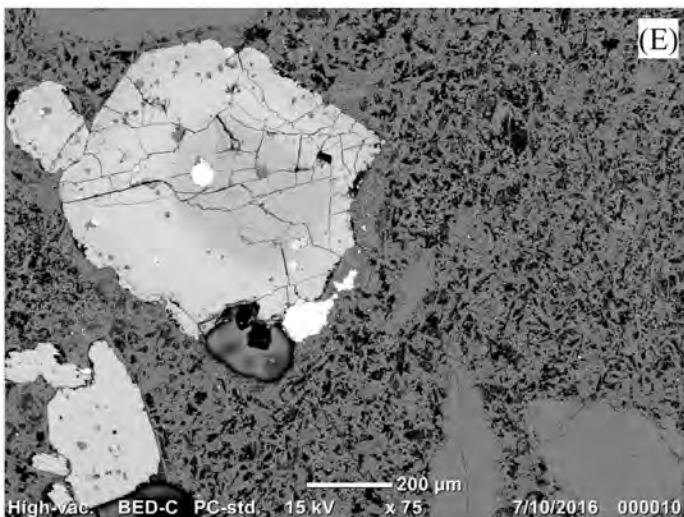


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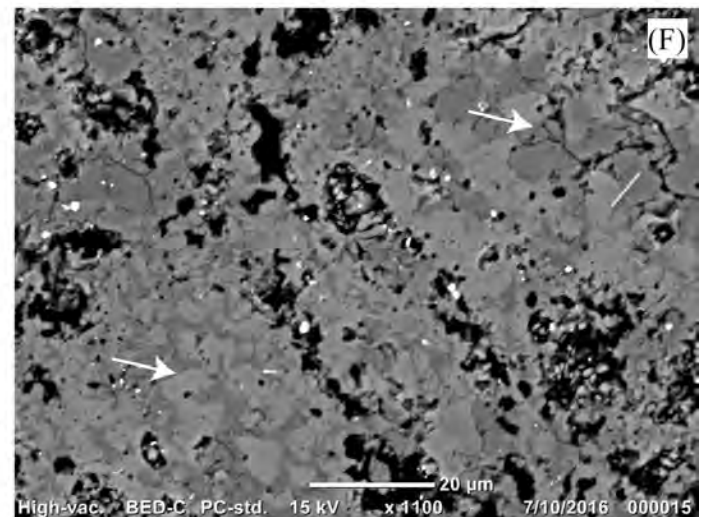


(D)

16MD-5

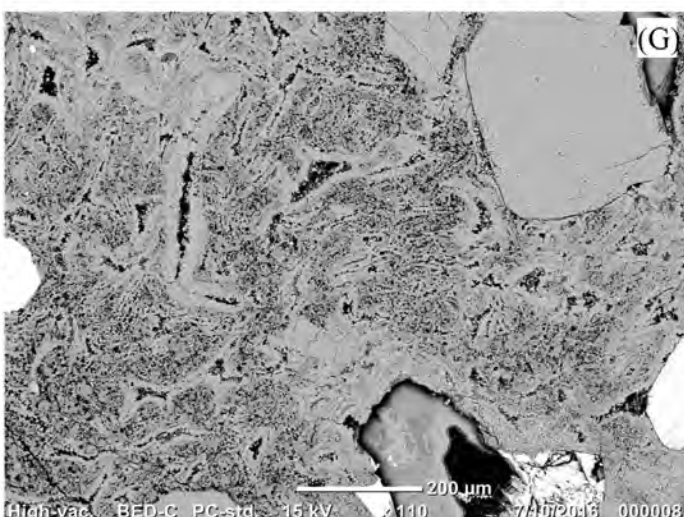


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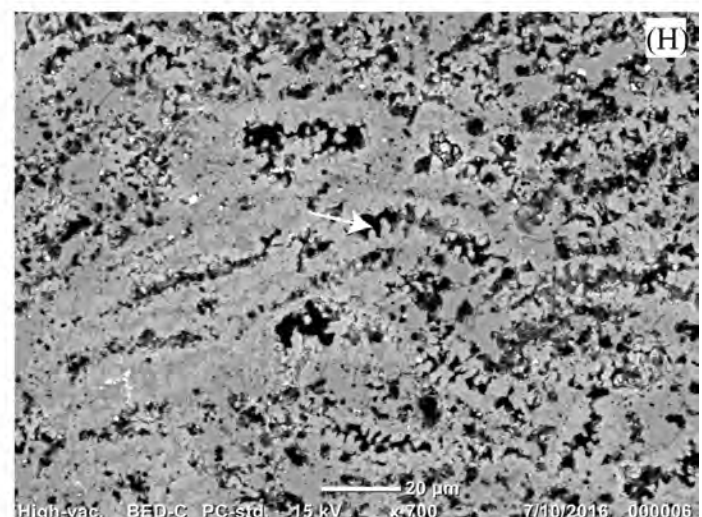


(F)

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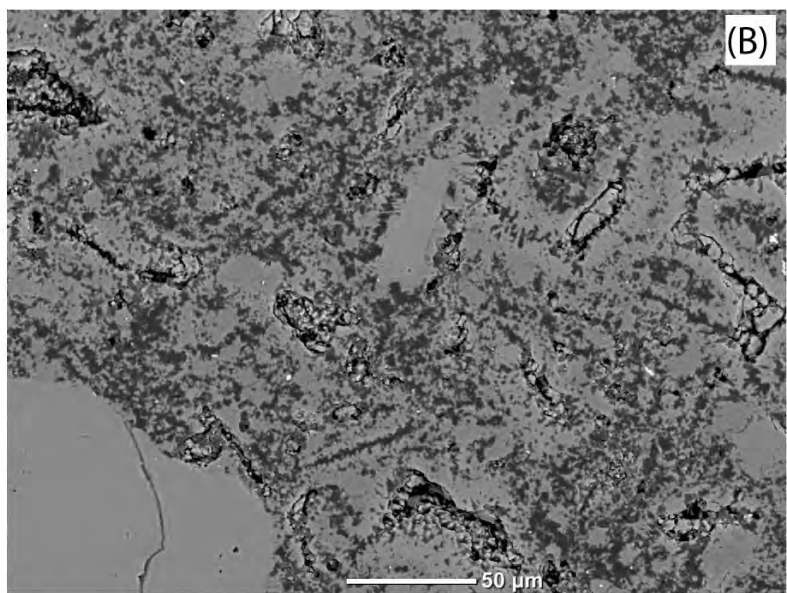
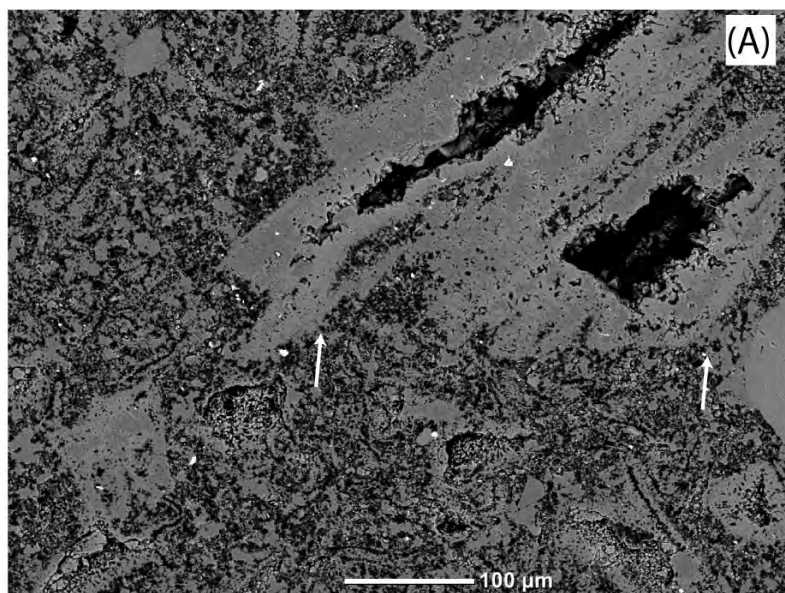


(G)

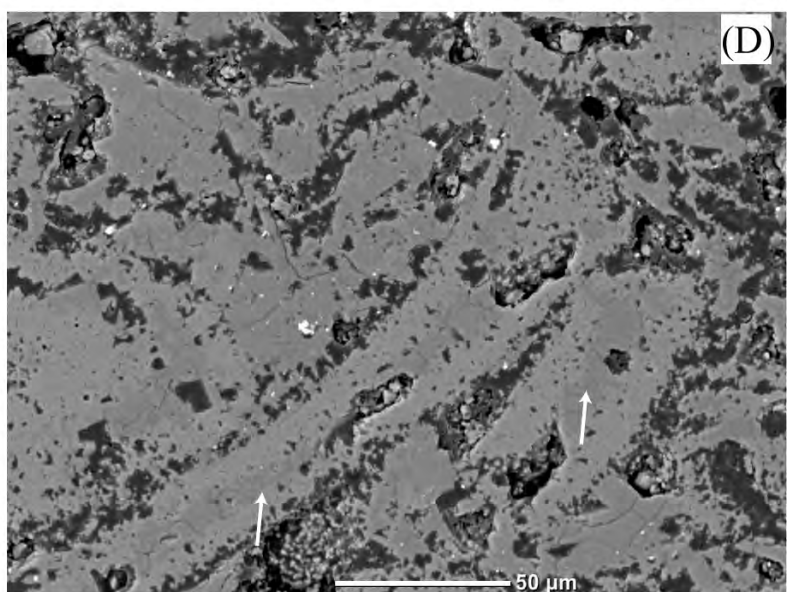
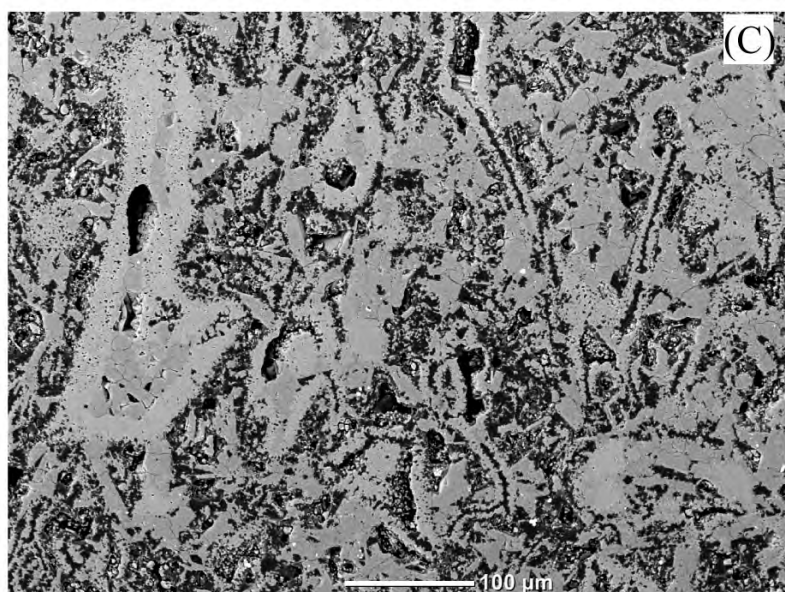


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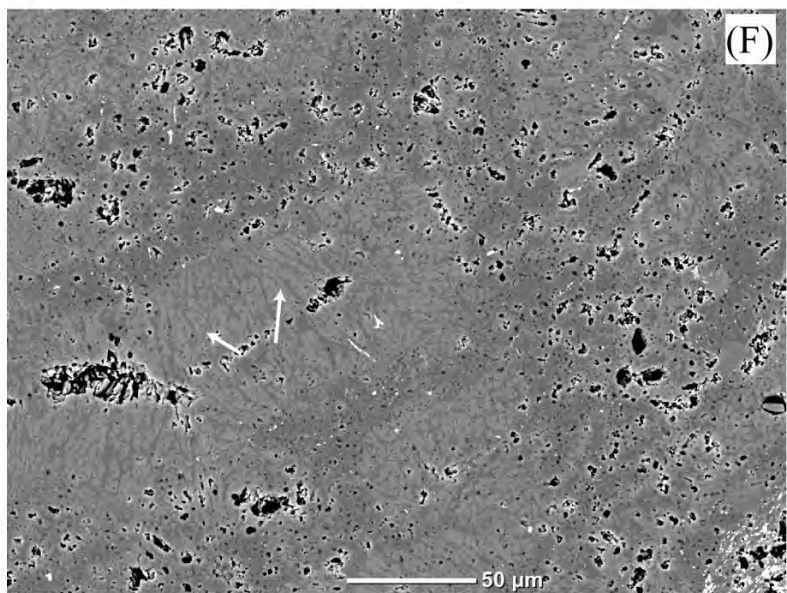
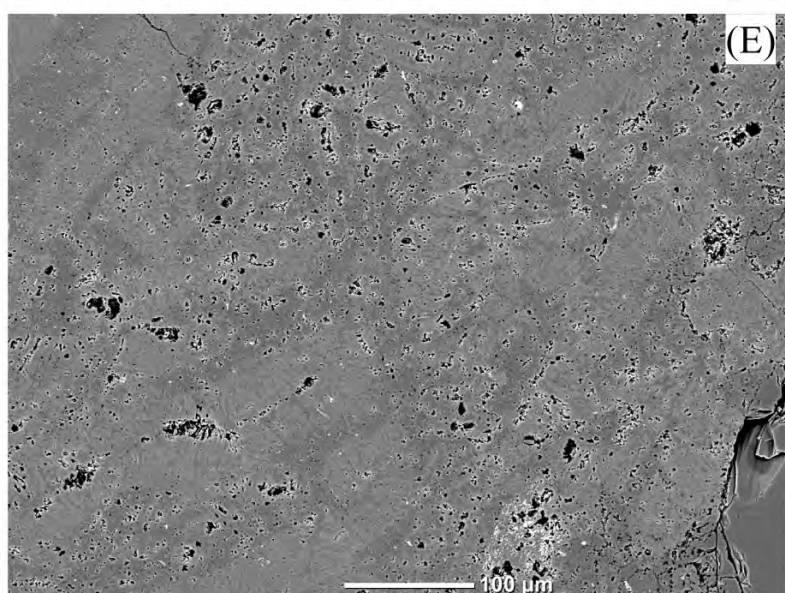
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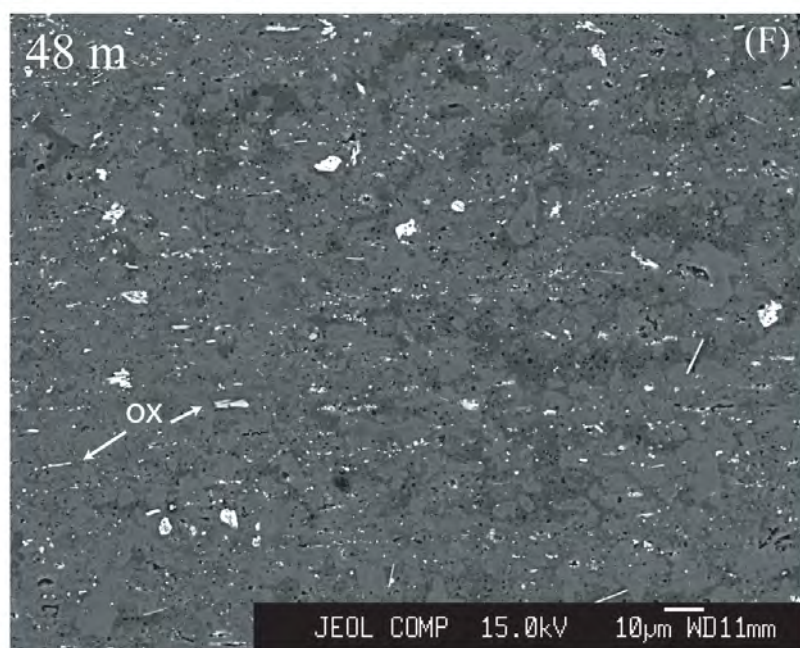
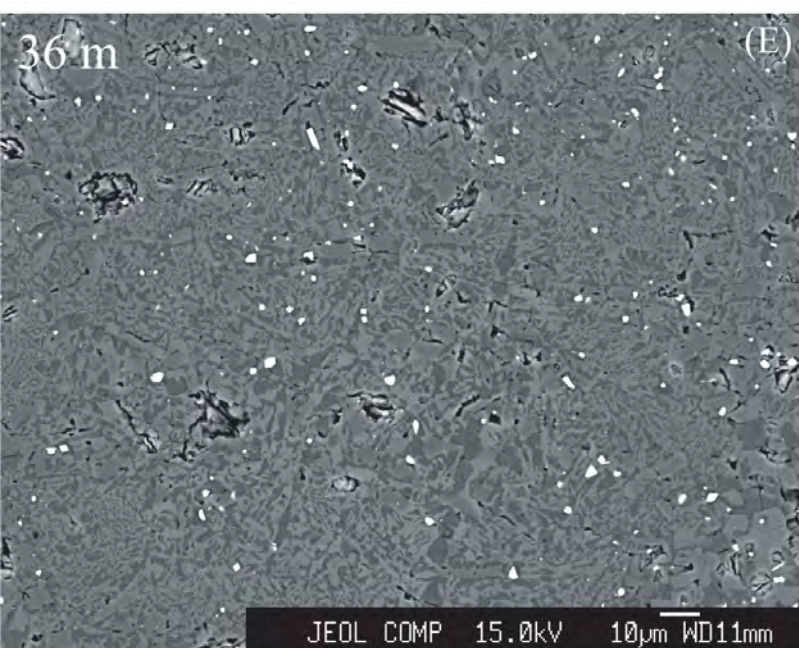
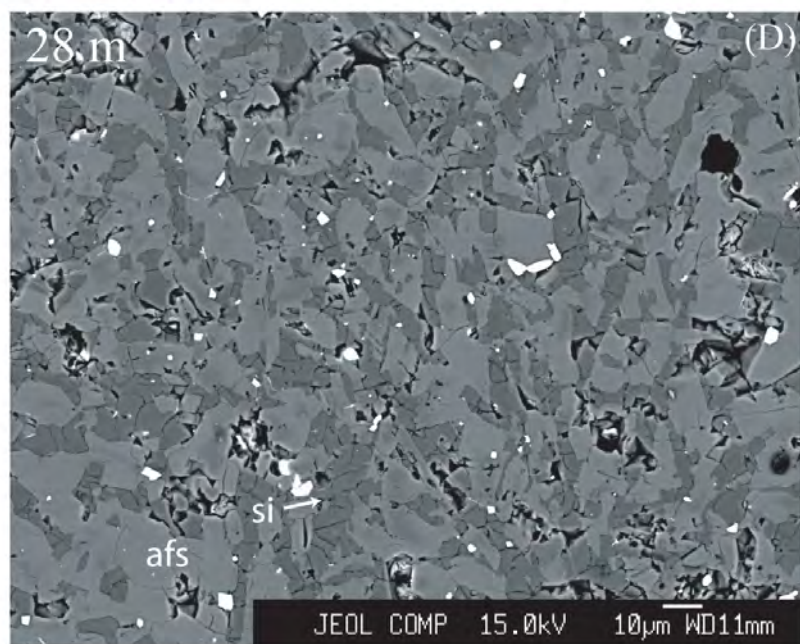
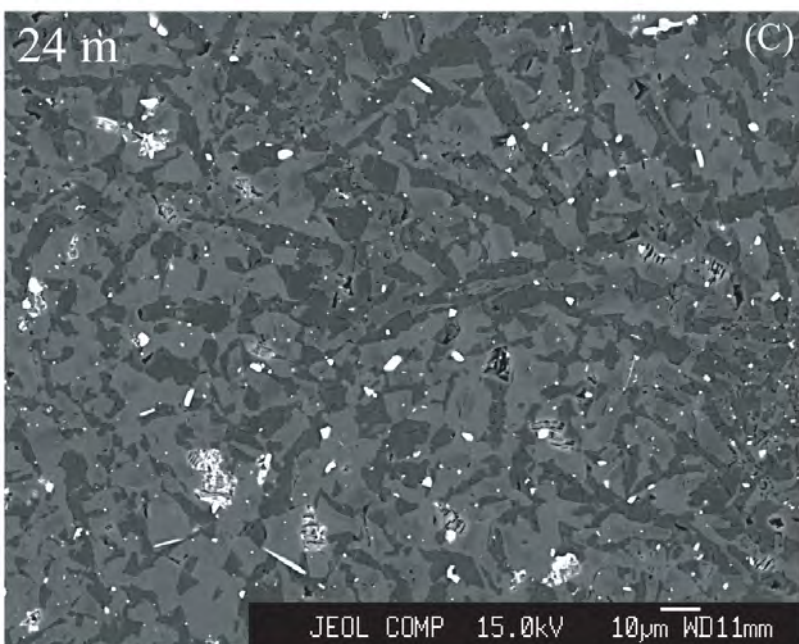
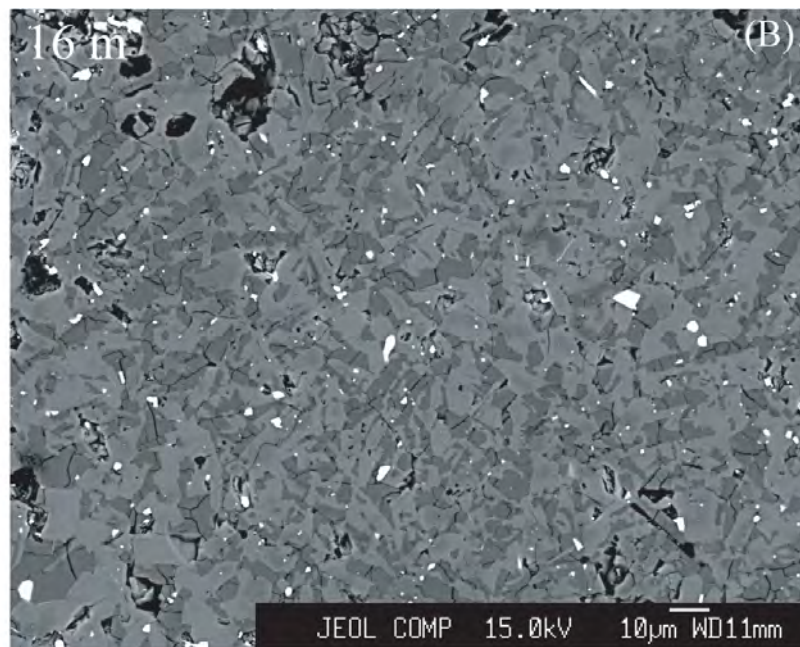
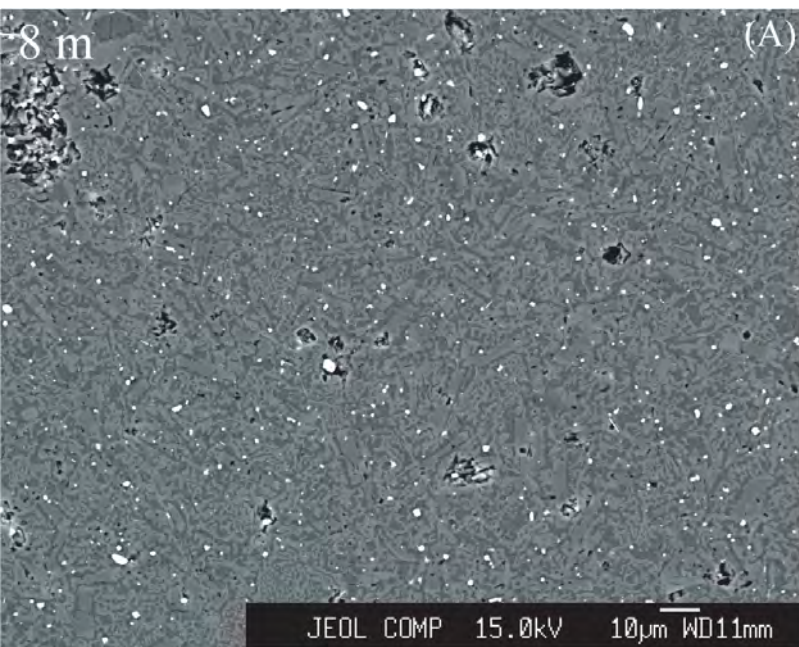


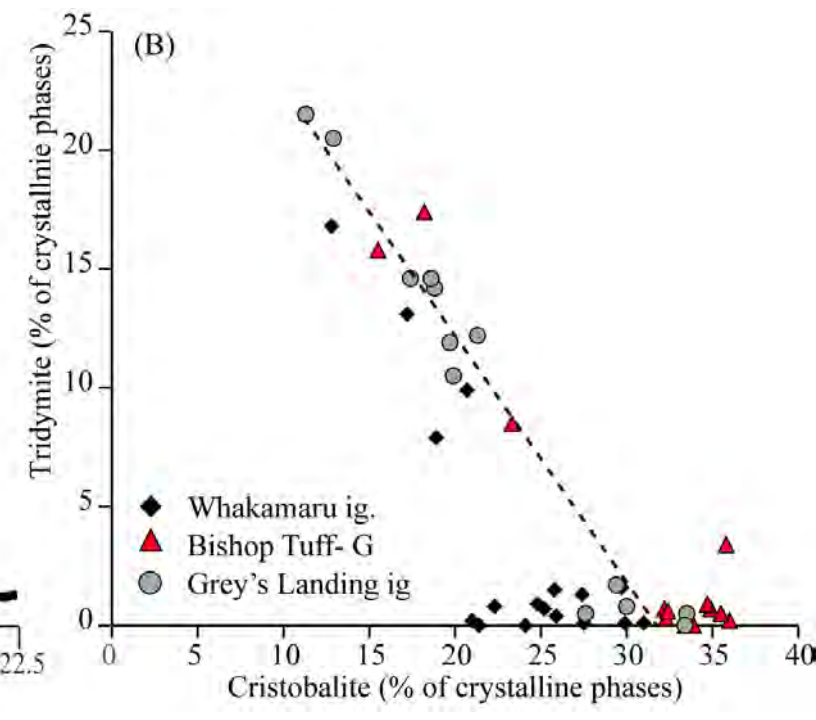
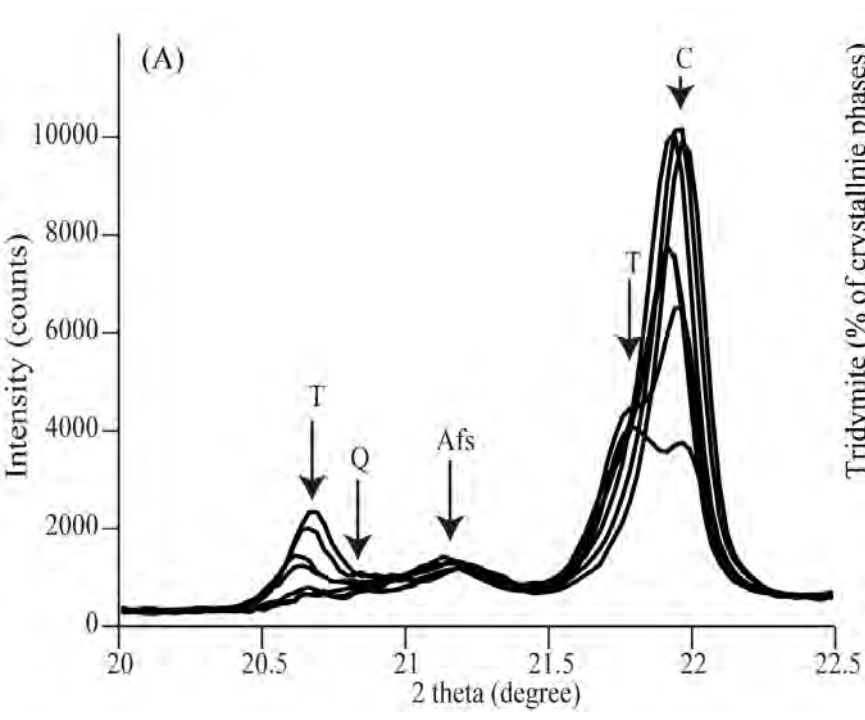
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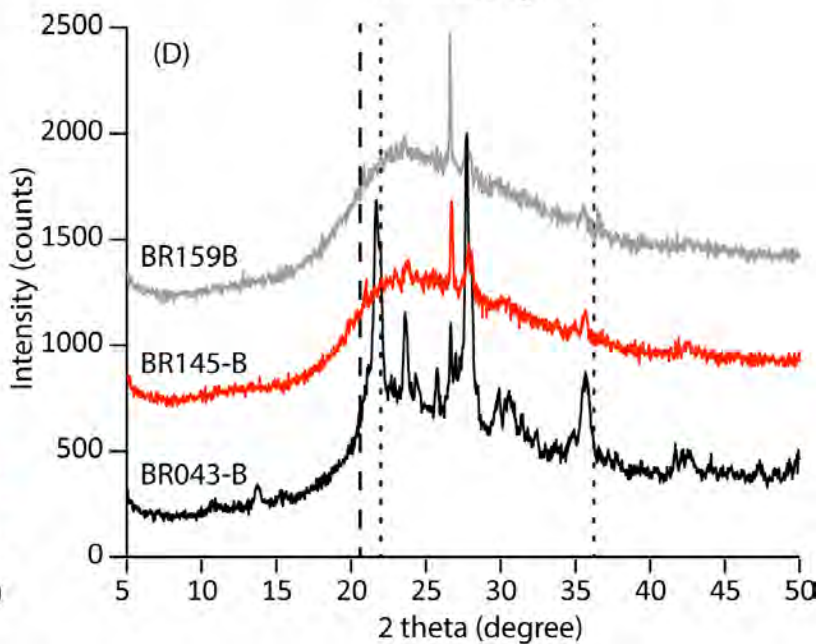
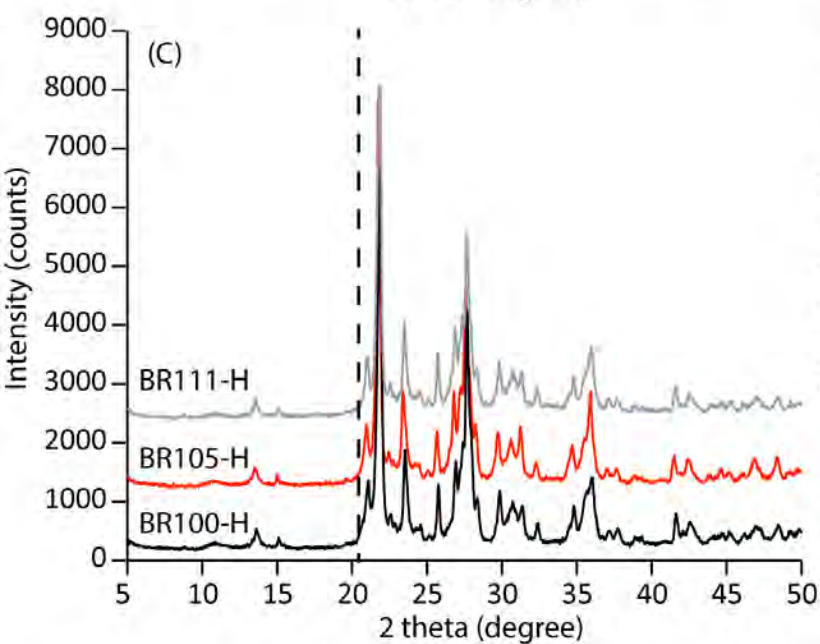
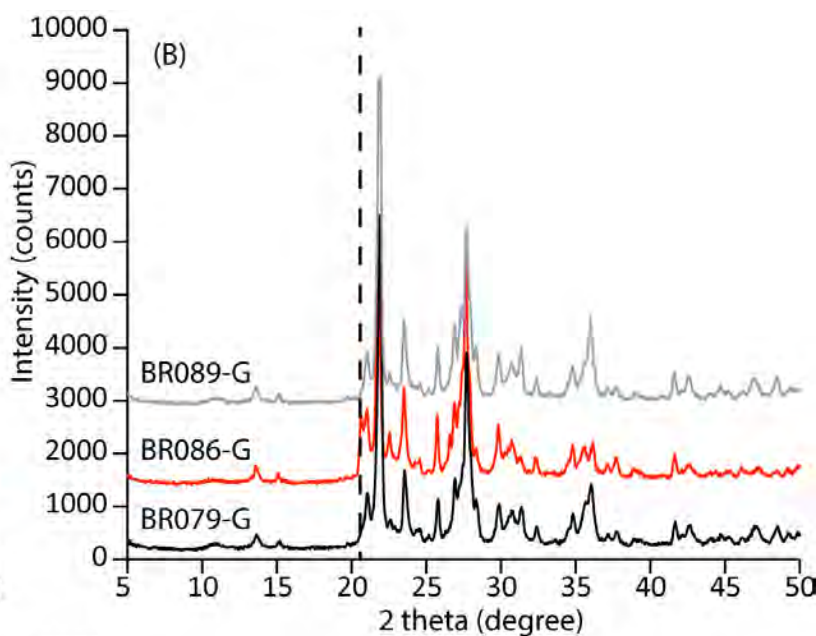
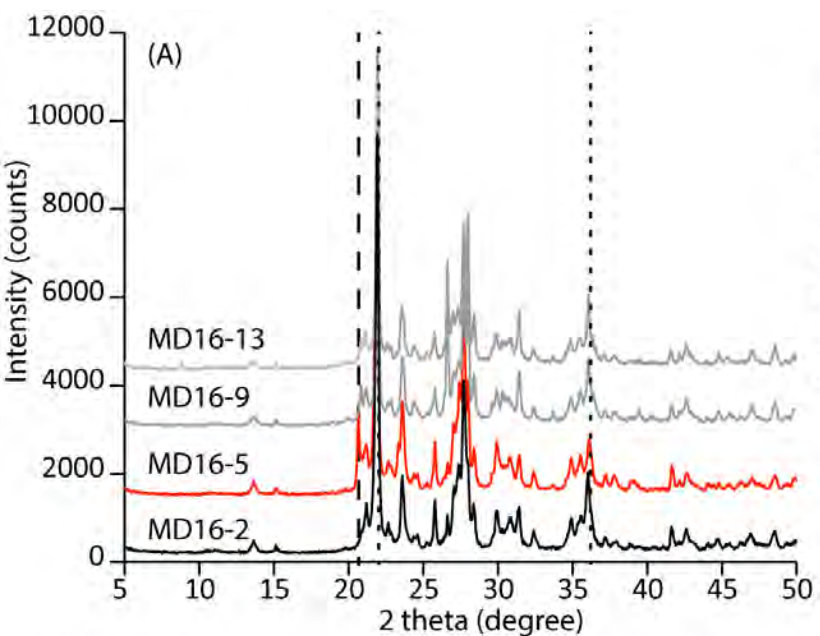


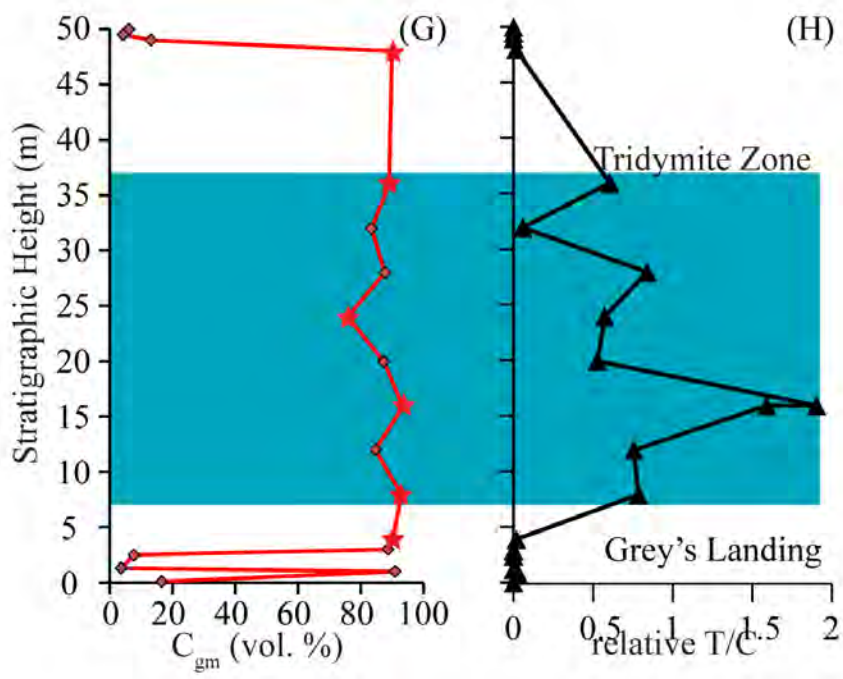
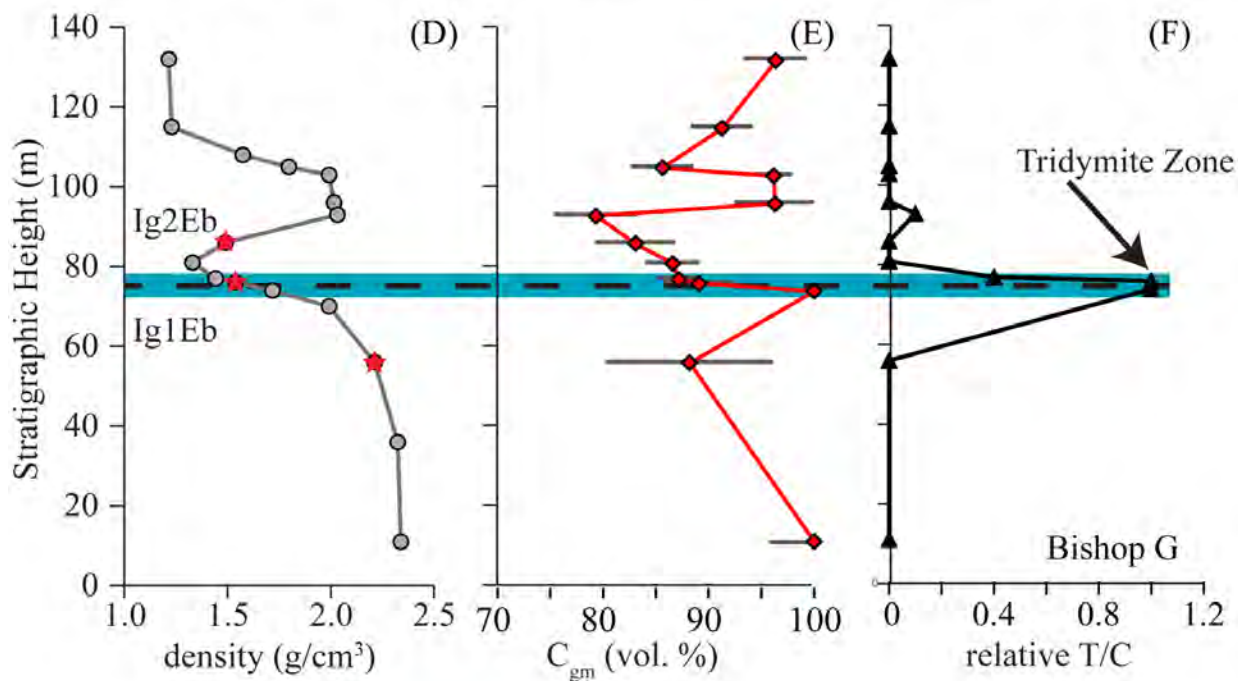
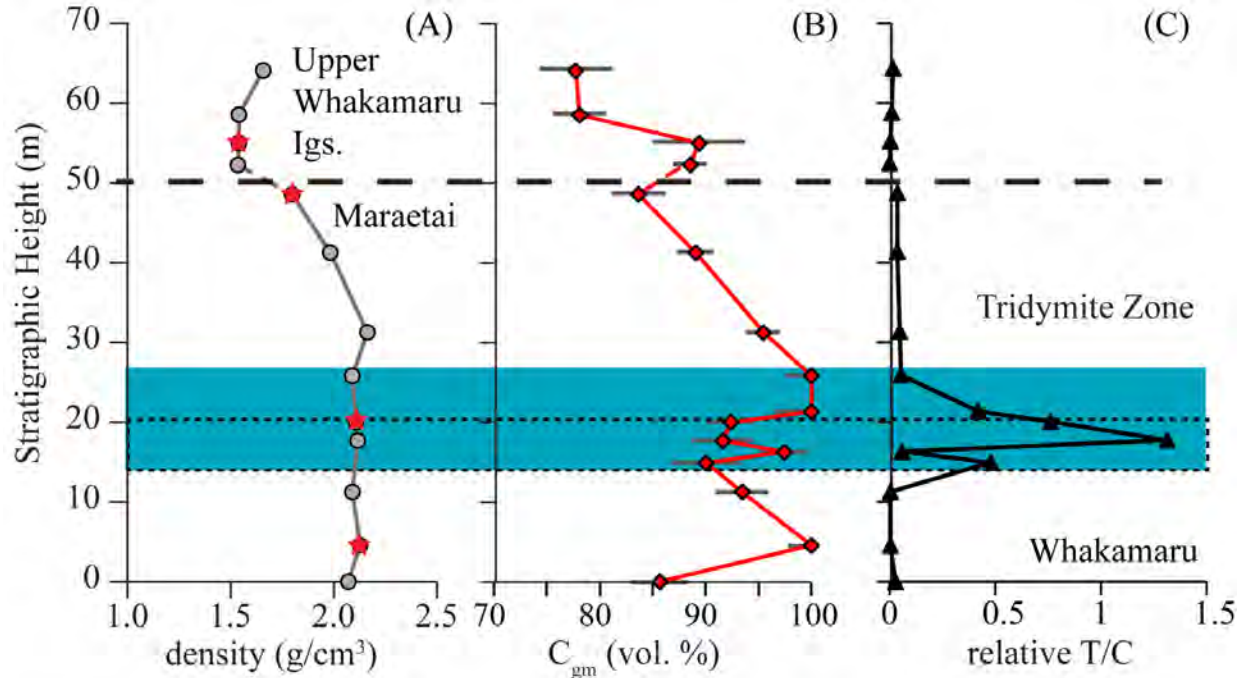
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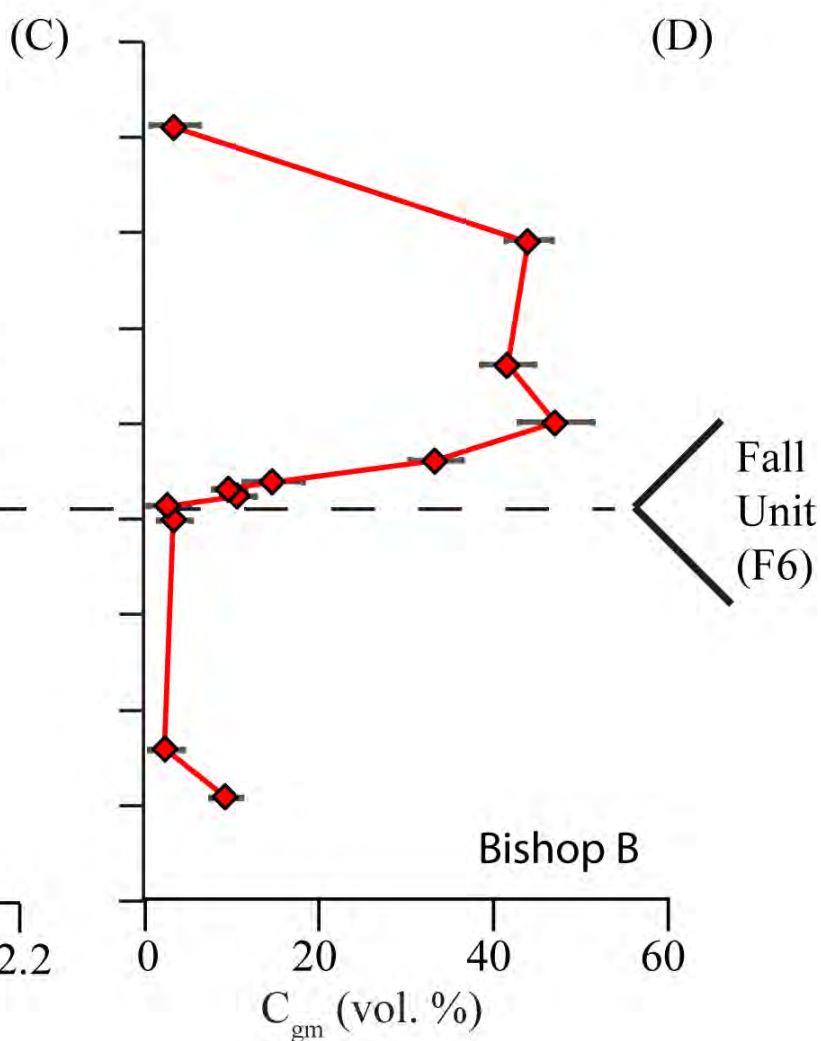
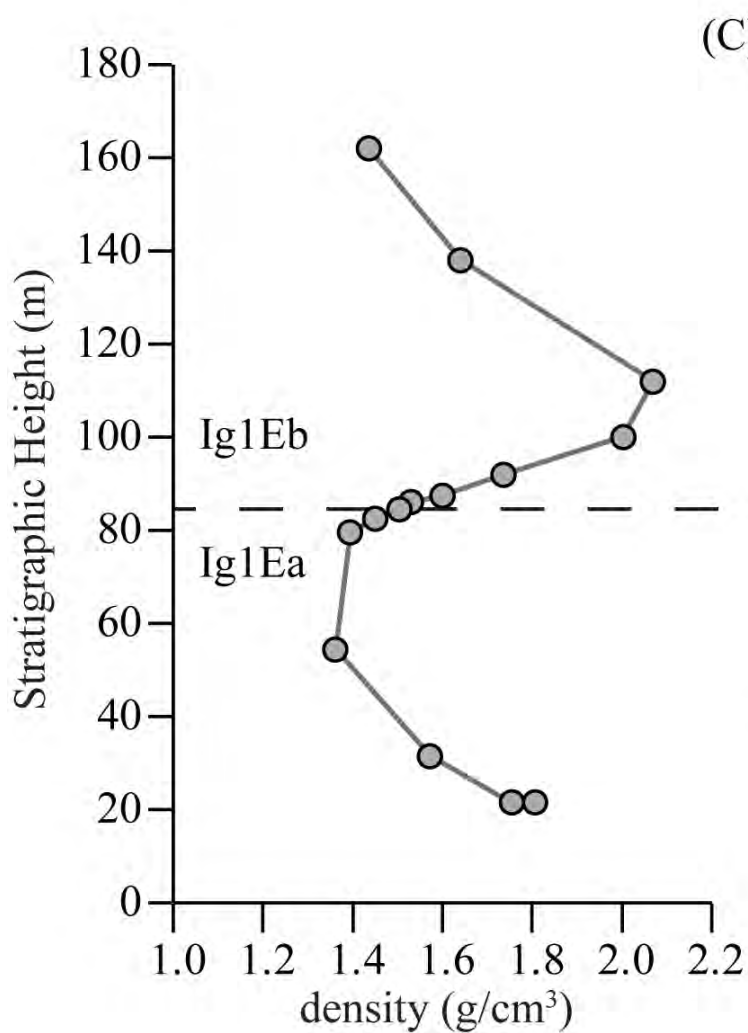
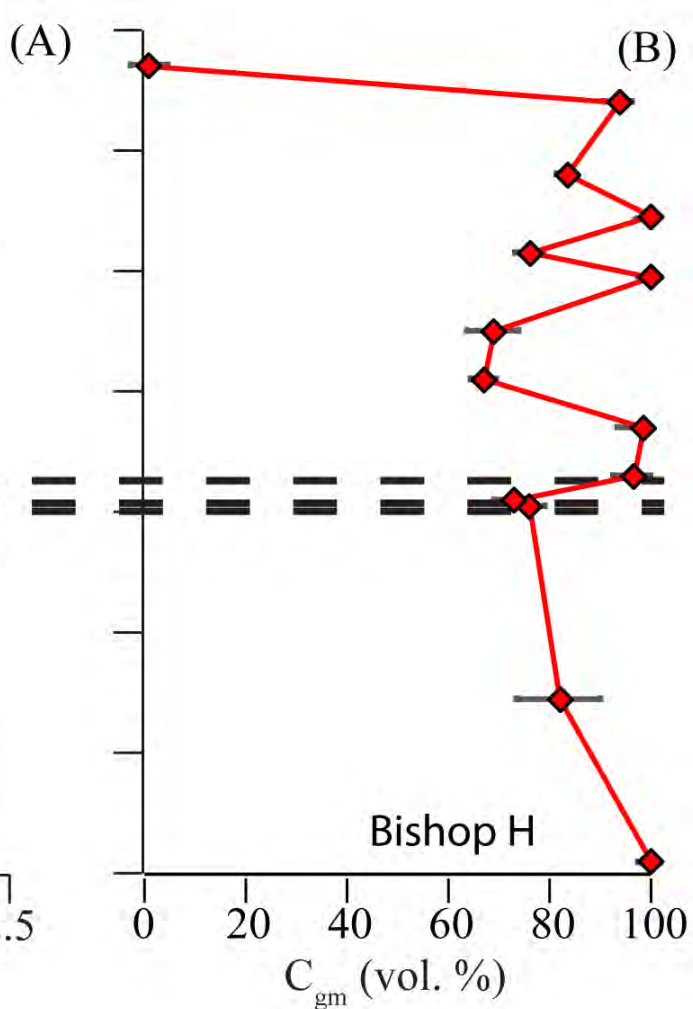
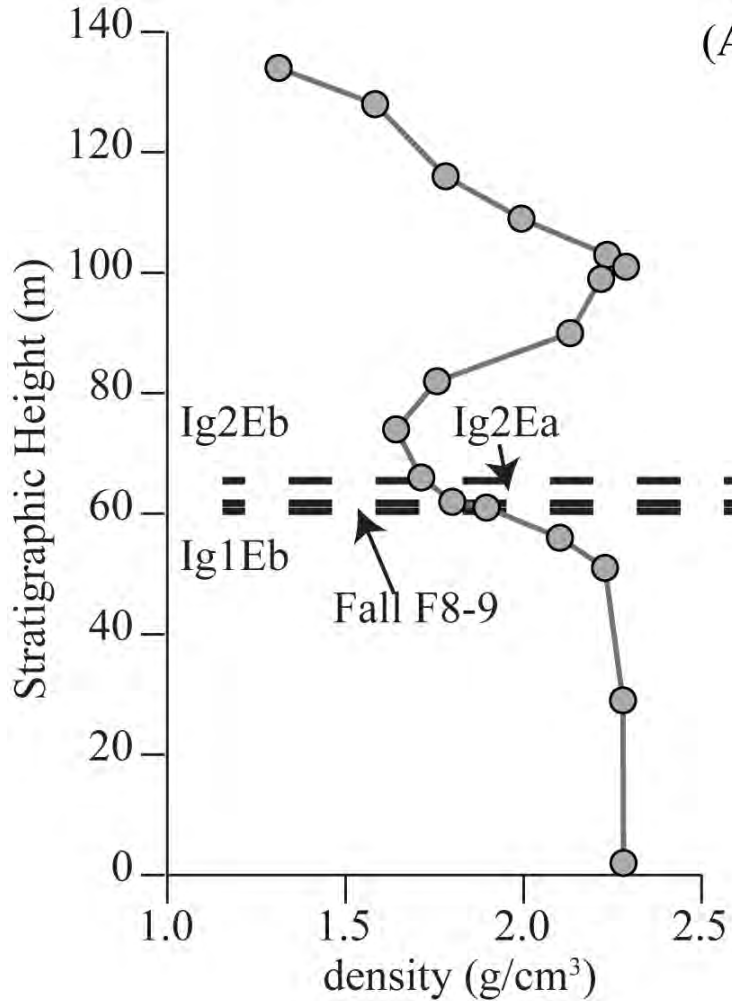




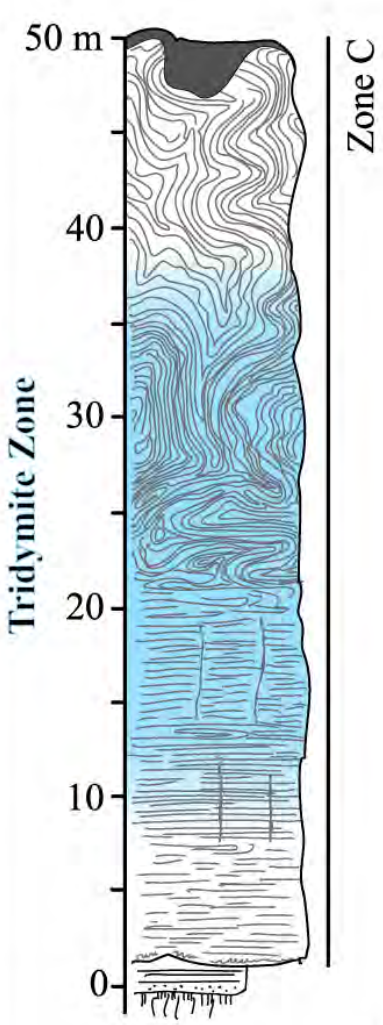






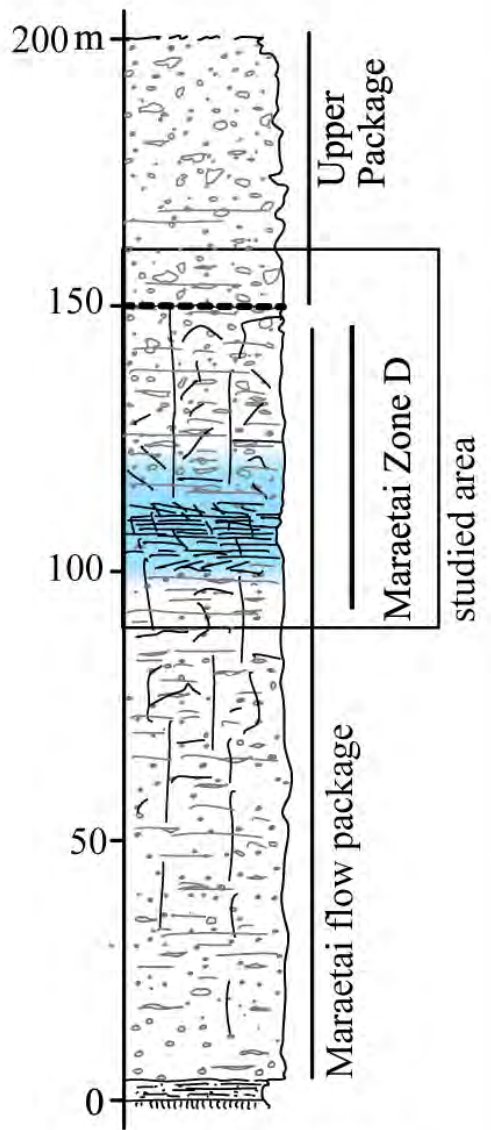


A 1 apparent flow
Highly welded
T°C >900 emplacement



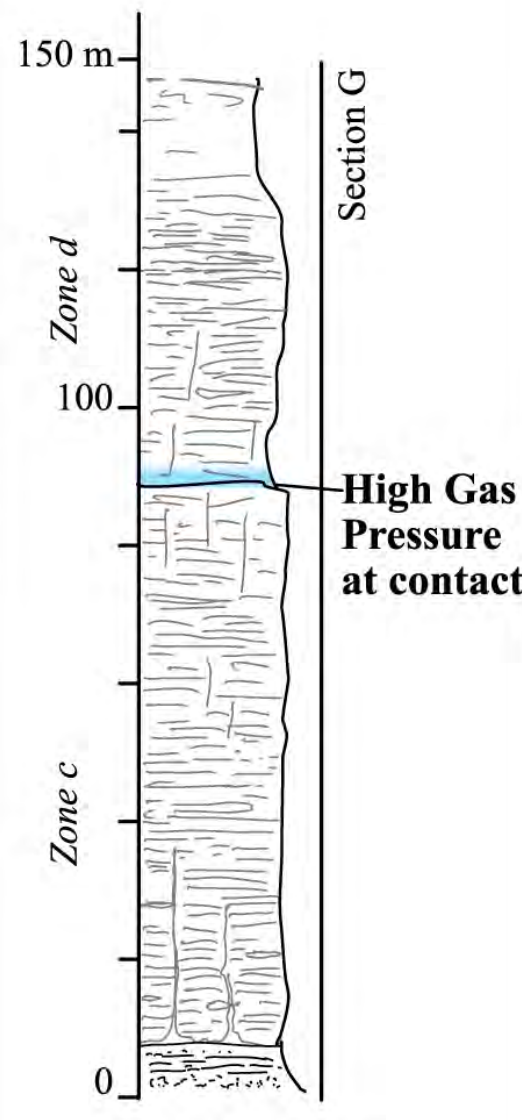
Grey's Landing Type

B multiple flow packages
Welded
T°C ~ 770 emplacement



Whakamaru Type

C multiple flow packages
Welded
T°C ~ 714 emplacement



Bishop "G" Type

Table 1: Summary of density and XRD results for the Whakamaru ignimbrite, Bishop Tuff section (G), and Grey's L

strat. m	density g/cm ³	C _{gm}	C _{gm} SD	Crs %	Trd %	T/C	
<i>Whakamaru ignimbrite</i>							
16MD-14	64	1.66	0.78	0.03	21.1	0.3	0.0
16MD-13	59	1.54	0.78	0.02	17.1	0.2	0.0
16MD-12	55	1.54	0.89	0.04	24.4	0.1	0.0
16MD-11	52	1.53	0.89	0.01	18.8	0.0	0.0
16MD-10		1.33	1	0.02	23.8	0.0	0.0
16MD-9	49	1.80	0.84	0.02	21.1	0.8	0.0
16MD-8	41	1.98	0.89	0.02	19.7	0.7	0.0
16MD-7	31	2.16	0.95	0.01	25.2	1.2	0.0
16MD-6	26	2.09	1	0.02	29.0	1.6	0.1
16MD 5b	21 --		1	0.03	17.9	7.5	0.4
16MD-5	20	2.11	0.92	0.02	15.5	11.8	0.8
16MD-4	18	2.12	0.92	0.03	11.5	15.1	1.3
16MD 3c	16 --		0.97	0.02	24.0	1.4	0.1
16MD 3b	15 --		0.90	0.03	18.4	8.8	0.5
16MD-3	11	2.09	0.93	0.02	27.2	0.1	0.0
16MD-2	5	2.13	1	0.02	29.4	0.1	0.0
16MD-1	0	2.07	0.86	0.03	21.8	0.6	0.0
<i>Bishop Tuff Section G¹</i>							
BR076 G	132	1.22	0.96	0.03	32.2	0.6	0.0
BR077 G	115	1.23	0.91	0.03	28.9	0.3	0.0
BR079 G	105	1.80	0.86	0.03	31.1	0.2	0.0
BR080 G	103	1.99	0.96	0.02	32.0	0.8	0.0
BR081 G	96	2.02	0.96	0.04	32.8	0.5	0.0
BR082 G	93	2.03	0.79	0.04	29.5	2.8	0.1
BR083 G	86	1.49	0.83	0.04	27.3	0.6	0.0
BR084 G	81	1.33	0.87	0.02	28.2	0.5	0.0
BR085 G	77	1.44	0.87	0.02	20.3	7.4	0.4
BR086 G	76	1.54	0.89	0.03	16.1	15.4	1.0
BR087 G	74	1.72	1	0.03	15.3	15.6	1.0
BR089 G	56	2.21	0.88	0.08	29.4	0.0	0.0
BR091G	11	2.34	1	0.04	32.2	0.0	0.0
<i>Grey's Landing Ignimbrite²</i>							
11-031	50		0.06	--	--	--	
11-032	49.5		0.04	--	--	--	
11-033	49		0.13	--	--	--	
11-034	48		0.90		30.1	0.4	0.0
11-051	36		0.89		17.5	10.6	0.6
11-050	32		0.83		24.5	1.4	0.1
11-049	28		0.88		15.3	12.8	0.8
11-048	24		0.76		16.2	9.3	0.6
11-047	20		0.87		17.4	9.2	0.5
11-046	16		0.93		10.5	20.1	1.9

11-046ii	16	0.94		12.1	19.2	1.6
11-045	12	0.85		15.9	12.0	0.8
11-044	8	0.93		17.3	13.6	0.8
11-041	4	0.90		24.9	0.5	0.0
11-040	3	0.89		29.6	0.0	0.0
11-039	2.5	0.08	--	--	--	
11-038	1.3	0.04	--	--	--	
11-037	1	0.91		27.3	0.7	0.0
11-036	0.1	0.16	--	--	--	

Note: C_{gm} (groudmass crystallinity) and C_{gm} standard deviation (SD) in volume fractions. Cristobalite (Crs) and tridymite (Trd) proportions from rietveld refinement (scaled based on calculated crystallinity). T/C is the tridymite to cristobalite ratio. ¹Density from Wilson and Hildreth (2003). ²Crystallinity from Ellis et al (2015).

anding ignimbrite.

Table 2: Summary of density and XRD results for Bishop Tuff (B and H).

strat. m	density ¹ g/cm ³	C _{gm}	C _{gm} SD
<i>Bishop Tuff Section H</i>			
BR099 H	2	2.28	1 0.02
BR100 H	29	2.28	0.82 0.08
BR103 H	61	1.90	0.76 0.03
BR104 H	62	1.80	0.73 0.04
BR105 H	66	1.71	0.97 0.04
BR106 H	74	1.64	0.99 0.05
BR107 H	82	1.76	0.67 0.03
BR108 H	90	2.13	0.69 0.05
BR109 H	99	2.22	1 0.02
BR111 H	103	2.24	0.76 0.03
BR112 H	109	1.99	1 0.03
BR113 H	116	1.78	0.84 0.02
BR114 H	128	1.58	0.94 0.03
BR115 H	134	1.31	0.01 0.04
<i>Bishop Tuff Section B</i>			
BR144	21.5	1.806	0.09 0.02
BR149	31.5	1.57	0.02 0.02
BR145	79.5	1.39	0.03 0.02
BR146	82.5	1.45	0.03 0.02
BR147	84.5	1.50	0.11 0.02
BR040	86	1.53	0.10 0.02
BR148	87.5	1.60	0.15 0.03
BR041	92	1.74	0.33 0.03
BR042	100	2.00	0.47 0.04
BR043	112	2.07	0.42 0.03
BR044	138	1.64	0.44 0.03
BR045	162	1.44	0.03 0.03

Note: C_{gm} (groudmass crystallinity) and C_{gm} standard deviation (SD) in volume fractions. ¹Densities from Wilson and Hildreth (2003).

Table 3: XRF and LOI measurements from the Whakamaru transect at Maraetai dam.

Sample	SiO ₂	TiO ₂	Al ₂ O ₃	Fe ₂ O ₃	MgO	MnO	CaO	K ₂ O
<i>Whakamaru samples</i>								
16MD-1	71.68	0.34	14.89	2.67	0.49	0.062	2.55	2.88
16MD-2	72.29	0.33	14.79	2.56	0.43	0.059	2.43	2.93
16MD-3	72.89	0.32	14.68	2.53	0.44	0.058	2.32	3.01
16MD-4	72.63	0.32	14.44	2.53	0.45	0.055	2.30	3.03
16MD-5	72.06	0.33	14.76	2.55	0.45	0.054	2.40	2.99
16MD-6	72.48	0.35	15.16	2.68	0.43	0.057	2.02	3.22
16MD-7	72.78	0.32	14.53	2.45	0.45	0.053	2.36	3.02
16MD-8	72.48	0.33	14.78	2.61	0.46	0.066	2.48	2.80
16MD-9	72.89	0.30	14.90	2.47	0.31	0.065	2.05	3.15
16MD-11	72.35	0.32	14.66	2.59	0.38	0.063	2.31	3.02
16MD-12	72.55	0.32	14.61	2.57	0.51	0.064	2.26	3.46
16MD-13	73.28	0.31	14.95	2.51	0.37	0.064	2.11	3.17
16MD-14	72.94	0.33	15.15	2.63	0.42	0.065	2.14	3.15
<i>standards</i>								
OU-1	58.21	0.427	14.99	8.83	4.554	0.123	6.4	0.21
SY-2	59.81	0.13	11.97	6.18	2.558	0.303	7.9	4.46
SY-2	59.67	0.132	11.9	6.19	2.567	0.304	7.89	4.44

Na2O	P2O5	LOI	Total
4.18	0.072	0.89	99.80
4.14	0.063	0.67	100.03
4.09	0.062	0.75	100.40
4.10	0.065	0.69	99.92
4.16	0.061	0.45	99.81
3.76	0.024	2.16	100.18
4.16	0.063	0.64	100.19
4.06	0.064	0.95	100.13
3.70	0.032	1.67	99.86
4.37	0.059	1.47	100.11
4.80	0.062	3.39	101.21
3.76	0.024	2.11	100.54
3.70	0.053	2.35	100.58
2.43	0.044	3.28	99.56
4.22	0.43	1.054	99.35
4.23	0.429	1.054	99.13