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1 **Anisotropic Thermoelastic Properties of Fe₇C₃ at High Pressures by Single-Crystal**
2 **X-Ray Diffraction**

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26 **ABSTRACT**

27 Carbon has been suggested as one of the light elements existing in Earth's core. Under
28 core conditions, iron carbide Fe_7C_3 is likely the first phase to solidify from an Fe-C melt
29 and has thus been considered a potential component of the inner core. The crystal
30 structure of Fe_7C_3 , however, is still under debate, and its thermoelastic properties are not
31 well constrained at high pressures. In this study, we performed synchrotron-based single-
32 crystal X-ray diffraction experiment using an externally-heated diamond anvil cell to
33 determine the crystal structure and thermoelastic properties of Fe_7C_3 up to 80 GPa and
34 800K. Our diffraction data indicate that Fe_7C_3 adopts an orthorhombic structure under
35 experimentally investigated conditions. The pressure-volume-temperature data for Fe_7C_3
36 were fitted by the high-temperature Birch-Murnaghan equation of state, yielding
37 ambient-pressure unit cell volume $V_0 = 745.2(2) \text{ \AA}^3$, bulk modulus $K_0 = 167(4) \text{ GPa}$, its
38 first pressure derivative $K_0' = 5.0(2)$, $dK/dT = -0.02(1) \text{ GPa/K}$, and thermal expansion
39 relation $\alpha_T = 4.7(9) \times 10^{-5} + 3(5) \times 10^{-8} \times (T-300) \text{ K}^{-1}$. We also observed an anisotropic elastic
40 response to changes in pressure and temperature along the different crystallographic
41 directions. Fe_7C_3 has strong anisotropic compressibilities with the linear moduli $M_a > M_c$
42 $> M_b$ from zero pressure to core pressures at 300K, rendering the b axis the most
43 compressible upon compression. The thermal expansion of c^3 is approximately four times
44 larger than that of a^3 and b^3 at 600K and 700K, implying that the high temperature may
45 significantly influence the elastic anisotropy of Fe_7C_3 . Therefore the effect of high
46 temperature needs to be considered when using Fe_7C_3 to explain the anisotropy of Earth's
47 inner core.

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48 *Key words* : iron carbide, thermal equation of state, anisotropy, inner core, temperature
49 effect

50

51 **INTRODCUTION**

52 Earth's inner core is considered to consist primarily of iron alloyed with nickel
53 and one or more light elements e.g. sulfur, silicon, oxygen, hydrogen and carbon, as
54 informed by numerous geophysical and geochemical constraints (recently reviewed by
55 Hirose et al., 2013; Li and Fei, 2014; Litasov and Shatskiy, 2016). The Fe-C system has
56 been proposed as a candidate composition for Earth's core largely due to the high
57 cosmochemical abundance of carbon, the frequent occurrence of iron carbide phases in
58 meteorites, and the high solubility of carbon in Fe-Ni liquids under the core-mantle
59 differentiation conditions (Wood, 1993). If the liquid core contained carbon, the iron
60 carbide phase, Fe₇C₃, may be the first phase to crystallize from the iron-carbon melt
61 under core conditions rather than other iron carbide phases such as Fe₃C, as suggested by
62 previously published Fe-C phase diagrams (Fei and Brosh, 2014; Lord et al., 2009;
63 Nakajima et al., 2009). The extrapolated density and sound velocity of Fe₇C₃ may
64 account for the density deficit and low S-wave velocity (v_s) of the inner core (Chen et al.,
65 2012; Chen et al., 2014; Liu et al., 2016a; Nakajima et al., 2011). In addition, its high
66 Poisson's ratio at inner core conditions was suggested to be comparable to that of the
67 inner core (Prescher et al., 2015). Moreover, the melting experiments by Liu et al.
68 (2016b) suggested that Fe₇C₃ may be a constituent of the innermost inner core for carbon-
69 bearing core composition due to its high melting temperature.

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70 The crystal structure of Fe_7C_3 has remained controversial over the last few
71 decades. Previous experimental studies reported its structure as either hexagonal ($P6_3mc$)
72 (Herbstein and Snyman, 1964) or orthorhombic ($Pnma$, $Pmn2_1$, $Pmc2_1$, $Pmcn$ or $Pbca$)
73 (Barinov et al., 2010; Bouchard, 1967; Fruchart et al., 1965; Prescher et al., 2015).
74 Theoretical calculations also compared the stability of hexagonal and orthorhombic
75 phases. Fang et al. (2009) determined that the orthorhombic phase ($Pnma$) is more stable
76 than the hexagonal phase ($P6_3mc$), whereas Raza et al. (2015) calculated that the
77 orthorhombic phase (space group $Pbca$) is the stable phase below 100 GPa and the
78 hexagonal phase becomes more stable above 100 GPa.

79 The elastic constants of Fe_7C_3 were also calculated at 0K for the two crystal
80 structures with space groups of $P6_3mc$ and $Pbca$ (Mookherjee et al., 2011; Raza et al.,
81 2015). There has been, however, only one study that calculated the thermoelasticity of
82 Fe_7C_3 with the space group of $P6_3mc$ (Li et al., 2016). Most of the high-pressure
83 experimental studies of the density of Fe_7C_3 were performed at room temperature. The
84 thermal equation of state (EoS) parameters have only been determined below 30 GPa
85 (Litasov et al., 2015; Nakajima et al., 2011), which leads to a large uncertainty when
86 extrapolating the experimental data to the pressure and temperature (P - T) conditions of
87 the inner core. Accurate knowledge on the crystal structure and thermoelastic properties of
88 Fe_7C_3 under core conditions is needed to construct a comprehensive and seismologically
89 consistent Fe-C inner core compositional model.

90 For the inner core, seismic waves travel faster along the rotational axis than in the
91 equatorial plane; one possible explanation for this anisotropy is the presence of
92 preferentially-orientated iron with strong single-crystal elastic anisotropy in Earth's inner

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93 core (Deuss, 2014; Hirose et al., 2013). The alloying of light elements with iron often
94 leads to different crystal structure and elasticity (Litasov and Shatskiy, 2016). Thus,
95 quantification of the elastic anisotropy of iron alloys is essential for us to understand the
96 inner-core anisotropy. For *hcp* metals and isostructural iron alloys such as Fe-Ni-Si
97 system, the elastic anisotropy is related to the *c/a* ratio, that is, the compressibilities and
98 thermal expansion of the *a* and *c* unit cell parameters under high pressure and high
99 temperature (Fischer and Campbell, 2015; Steinle-Neumann et al., 2001; Wenk et al.,
100 1988). For orthorhombic Fe₇C₃, the elastic anisotropy is also correlated with the different
101 compressional response to applied pressure of each primary crystallographic axis as
102 reported in a calculation by Raza et al. (2015). Therefore, it is crucial to constrain how
103 the compressibility and thermal expansion along individual crystallographic axes respond
104 to pressure and temperature, so as to understand the potential for this material to
105 contribute to the seismic anisotropy observed in the inner core (Deuss, 2014). In this
106 study, we determined the thermal EoS and the thermoelastic properties of Fe₇C₃ along
107 different crystallographic axes up to 80 GPa and 800K by employing an externally-heated
108 diamond anvil cell (DAC) with synchrotron-based single-crystal X-ray diffraction
109 (XRD).

110

111 **METHODS**

112 The Fe₇C₃ single crystal sample was synthesized at 18 GPa and 1773 K in a multi-
113 anvil press (Prescher et al., 2015). Single-crystal XRD characterizations of the sample at
114 ambient conditions were conducted at beamline 13-BMC, the Advanced Photon Source
115 (APS), Argonne National Lab and at the University of Hawai'i at Mānoa (UHM) using a
116 Bruker D8 Venture single-crystal diffractometer ($\lambda = 0.5609 \text{ \AA}$). The sample was

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117 mounted on a MiTeGen micromesh that was attached to a goniometer head. At beamline
118 13-BMC, the sample was rotated from -60° to $+60^\circ$. 120° wide-angle exposure and 1° step
119 exposures were collected. For the ambient characterization of the sample at UHM, a
120 preliminary matrix run was first completed with 1° steps through orthogonal slices of
121 reciprocal space. Indexing of diffraction peaks from the matrix run was used by Bruker
122 APEX 3 software to determine an optimal data collection strategy that ensured 100%
123 completeness to a resolution limit of 0.65 \AA . This strategy was then used to collect a full
124 dataset.

125 A BX90 DAC with a pair of $250 \mu\text{m}$ -culet diamond anvils was used for the high-
126 pressure XRD experiments (Kantor et al., 2012). A cubic boron nitride seat on the
127 upstream side and a large-opening tungsten carbide seat on the downstream side were
128 used to maximize access to reciprocal space for the single-crystal XRD measurements. A
129 pyrophyllite ring-heater base was fabricated using a milling machine and sintered in a
130 furnace at 1373 K for 20 hours. Three Pt-10wt.%Rh (0.01") wires were wound around the
131 heater base and covered by high-temperature cement. Two K-type thermocouples
132 (Chromega-Alomega 0.005" and Chromega-Alomega 0.010") were mounted near the
133 diamond culet and in touch with the downstream diamond to measure the temperature.
134 The rhenium gasket was preindented to a thickness of $\sim 35 \mu\text{m}$ and a sample chamber of
135 $150 \mu\text{m}$ in diameter was drilled by an electrical discharge machine (EDM). A $10 \mu\text{m}$ thick
136 Fe_7C_3 single-crystal grain and two pressure calibrants, a small ruby sphere (Mao et al.,
137 1986) for the neon gas loading and a piece of gold foil near the sample as the primary
138 pressure scale in experiments (Fei et al., 2007), were loaded in the sample chamber. Neon
139 gas, which was used as a pressure-transmitting medium, was loaded in the sample

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140 chamber using the gas loading machine at GeoSoilEnviroCARS of the APS. The pressure
141 uncertainties were estimated by the pressure difference of gold and neon (Fei et al.,
142 2007).

143 The high-pressure and high-temperature synchrotron-based single-crystal XRD
144 experiments were conducted at beamline 13-BMC, APS, Argonne National Lab. The
145 typical size of the focused monochromatic X-ray beam ($\lambda = 0.4340 \text{ \AA}$) was $16 \times 11 \text{ \mu m}^2$. A
146 MAR165 charged coupled device (CCD) detector was used to collect the diffraction
147 patterns. The X-ray accessible opening angle of the DAC was $\pm 20^\circ$. The rotation axis for
148 the single-crystal diffraction experiment was placed horizontally, perpendicular to the
149 incident X-ray beam. A series of 10° wide-angle exposures and 1° step exposures from
150 -20° and 20° were collected at four different detector positions for each pressure and
151 temperature point. The investigated range of pressure was 1 bar to 79.2 GPa and range of
152 the temperature was 300K to 800K (Fig. S1).

153 To analyze the synchrotron-based single crystal XRD data, we utilized the
154 ATREX software package for peak fitting and intensity corrections (Dera et al., 2013).
155 The unit cell and orientation matrix were determined by the CELL_NOW software
156 (Bruker AXS Inc.). Lattice parameters were refined by least-squares fitting in the RSV
157 software (Dera et al., 2013). The structure refinement was performed using SHELXL
158 (Sheldrick, 2008). The ambient pressure data collected at UHM were analyzed using the
159 Bruker APEX 3 software package to solve the complexity in the crystal structure. The P -
160 V - T data and P - x (i.e. $a/b/c$ axes) were fitted by the EosFit7-GUI program (Gonzalez-
161 Platas et al., 2016).

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163 RESULTS AND DISCUSSION

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164 **The crystal structure of Fe₇C₃ at room pressure and temperature**

165 The indexing of single-crystal XRD patterns of Fe₇C₃ at ambient conditions
166 indicates an orthorhombic lattice with space group *Pbca* ($Z = 8$), and with unit-cell
167 parameters of $a = 11.979(1) \text{ \AA}$, $b = 4.5191(8) \text{ \AA}$ and $c = 13.767(2) \text{ \AA}$. However, the
168 ambient data indicate some structural complexity beyond the simple ideal structure
169 described previously (Prescher et al., 2015), and consistently present in all of the several
170 single crystal specimens that we have examined. This non-ideality involves the presence
171 of twin micro-domains, but seems to also include structural modulation.

172 The presence of peaks that could not be indexed using a single orientation matrix
173 to the initially indexed domain indicates a likely twinned crystal structure (Fig. S2). The
174 second domain is significantly weaker than the first. A total of 1651 peaks from the
175 dominant domain were utilized to refine the crystal structure (Fig. 1 and CIF in the
176 deposit materials), which is generally consistent with that reported by Prescher *et al.*
177 (2015). In the *Pbca* structure, three distorted CFe₆ trigonal prisms form triads by sharing
178 corners. The triads are stacked parallel to the b axis to form a column. Each stack is
179 rotated $\sim 60^\circ$ relative to its neighbors. Columns are oriented inversely along the b axis
180 compared to their neighbor columns. Columns with the same direction are edge sharing
181 and columns with the opposite direction are corner sharing (Fig. 1).

182 The quality of structural refinement was high ($R_{\text{int}} = 7.26\%$ and $R_1 = 4.97\%$),
183 however, we noted some artifacts that may be related to the twinning and/or the
184 additional disorder within the structure. Three noticeably large peaks appeared in the
185 difference Fourier map with heights above 2.5 e/\AA^3 , located about 0.8 \AA from carbon
186 atoms, and 1.6 \AA from closest Fe atoms. We attempted to reduce the symmetry to

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187 allowed orthorhombic and monoclinic subgroups of *Pbca* but could not find an
188 alternative space group that would better account for this difference electron density. We
189 also noted that the residual electron density reported by Prescher et al. (2015) was also
190 quite high (2.022 e/Å³), which may indicate similar structural complexity in their
191 samples. Proper refinement of such complexity in the structure may require a description
192 using a 4-dimensional space group and the introduction of an extra basis vector or
193 modulation vector. Additional ambient pressure experiments at varied temperatures are
194 needed to confirm the likelihood of the modulation and whether the modulation is
195 commensurate or incommensurate. Detailed crystallographic studies will be required to
196 determine the exact origin of this difference electron density, but this is out of the scope
197 for the present study which is primarily focused on the thermoelastic behaviors.

198

199 **Thermal equation of state of Fe₇C₃**

200 The unit cell volumes of Fe₇C₃ along various isotherms from 300K to 800K were
201 determined by synchrotron-based single-crystal XRD measurements up to 79.2 GPa (Fig.
202 S3 and Table S1). No discontinuous crystal-structure change was observed over the entire
203 pressure and temperature range. The room temperature *P-V* data were fitted by the third-
204 order Birch-Murnaghan Equation of State (B-M):

$$205 \quad P = \frac{3}{2}K_{T_0} \left[\left(\frac{V_{T_0}}{V} \right)^{\frac{7}{3}} - \left(\frac{V_{T_0}}{V} \right)^{\frac{5}{3}} \right] * \left\{ 1 + \frac{3}{2}(K_{T_0}' - 4) \left[\left(\frac{V_{T_0}}{V} \right)^{\frac{2}{3}} - 1 \right] \right\} \quad (1)$$

206 where K_{T_0} , K_{T_0}' and V_{T_0} are the isothermal bulk modulus, its first pressure derivative
207 and the unit cell volume at ambient pressure and given temperature T , respectively. The
208 10 *P-V* data were weighted by the uncertainties in both pressure and volume and fitted
by the

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209 third-order B-M EoS with $K_0 = 165(4)$ GPa, $K_0' = 5.1(2)$ and $V_0 = 745.3(2)$ Å³ (K_0 , K_0'
210 and V_0 are for $T = 300$ K). Normalized stress (F_E) as a function of the Eulerian finite strain
211 (f_E) is also plotted as an inset of Fig. 2, where $f_E = [(V/V_0)^{-2/3} - 1]/2$ and $F_E = P/[3f_E(1+2f_E)^{5/2}]$
212 and the EoS can be simplified as $F_E = K_0 + 3K_0'/2(K_0' - 4)f_E$, neglecting the high order terms
213 (Angel, 2000). The f - F plot can be used to verify which order of the B-M EoS is
214 sufficient to satisfactorily represent the compression behavior of the sample (Angel,
215 2000). The quasi-linear f - F relationship suggests the adequacy of using the third-order B-
216 M EoS and its positive slope indicates $K_0' > 4$ (Fig. 2 inset). Previous studies reported
217 that the slope of the f - F plot changed abruptly as a result of the magnetic transitions of
218 hexagonal Fe₇C₃ (Chen et al., 2012; Liu et al., 2016a), but we did not observe this,
219 potentially due to the sparsity of our data at 300K (Fig. 2 inset).

220 Due to the similarity between the orthorhombic structure with the *Pbca* space
221 group and the hexagonal structure with *P6₃mc* space group, the compressibility of Fe₇C₃
222 was compared with the compressibility of both orthorhombic and hexagonal Fe₇C₃ in the
223 previous studies (Table 1 and Fig. 2). Our bulk modulus is consistent with the
224 orthorhombic Fe₇C₃ phase from Prescher et al. (2015), but its pressure derivative, K' , is
225 smaller (5.1(2) in this study while 6.1(1) in Prescher et al. (2015)). The discrepancy may
226 be caused by two reasons. First, we used a gold pressure standard whereas Prescher et al.
227 (2015) used ruby as their pressure standard. Second, our experiment involved external
228 heating while the experiments in Prescher et al. (2015) were conducted at room
229 temperature. The larger K' in their study may indicate less hydrostatic sample chamber
230 with increasing pressure (this is seen in other materials, e.g. Finkelstein et al. (2017)).
231 High temperatures could help to relax the deviatoric stress present in the sample chamber.

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232 Comparing with the hexagonal Fe₇C₃ shown in Fig. 2 and Table 1, our density as a
233 function of pressure and compressibility is similar to the values reported by Liu et al.
234 (2016a), who argued that the pressure calibration in his study might be more accurate
235 because the Au pressure standard was placed on the top of the sample.

236 In our study, Equation (1) was used along various high-temperature isotherms at
237 300K, 400K, 500K, 600K, 700K, and 800K (Table S1 and Fig. 3). Assuming that dK/dT
238 is constant through the temperature ranges, K_{T0} and K_{T0}' can be described as:

$$239 \quad K_{T0} = K_0 + dK/dT \times (T-300) \quad (2)$$

$$240 \quad K_{T0}' = K_0' \quad (3)$$

241 and the temperature dependence of volume can be expressed by the empirical polynomial
242 equation (Berman, 1988) as:

$$243 \quad V_{T0} = V_0(1 + \alpha_0(T-300) + \frac{1}{2}\alpha_1(T-300)^2) \quad (4)$$

244 Taking the first derivative of the Equation (4) gives the thermal expansion coefficient α_T
245 $= \alpha_0 + \alpha_1(T-300)$ by approximation. The fit to the P - V - T data (Table S1) using Equations
246 (1-4) results in $K_0 = 167(4)$ GPa, $K_0' = 5.0(2)$ and $V_0 = 745.2(2)$ Å³, $dK/dT = -0.02(1)$
247 GPa/K and thermal expansion $\alpha_T = 4.7(9) \times 10^{-5} + 3(5) \times 10^{-8} \times (T-300)$ K⁻¹. K_0 , K_0' and V_0
248 obtained by the high-temperature Birch-Murnaghan EoS are consistent with the values by
249 only fitting the 300K data within the uncertainties.

250

251 **Compressibilities and thermal expansions of the a , b and c axes**

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252 The compression data of the a , b and c axes at 300 K were fitted by the EosFit7-
253 GUI program (Gonzalez-Platas et al., 2016). The program fits the cube of the lattice
254 parameters to obtain the linear moduli and its pressure derivative, typically denoted as M
255 and M' , respectively (Angel et al., 2014). M is the inverse of the linear compressibility β
256 ($\beta_i = x_i^{-1}(\partial x_i / \partial P)_T$) and three times that of the volume-like K value (Angel, 2000). The
257 fitting yields $M_a = 577(14)$ GPa, $M_a' = 18.6(9)$, $M_b = 438(9)$ GPa, $M_b' = 12.7(4)$, $M_c =$
258 $490(32)$ GPa and $M_c' = 16(2)$. $M_a > M_c > M_b$ indicates that the axial compressibilities of
259 Fe_7C_3 are anisotropic (Fig. 4). Considering the trade-off between M and M' ,
260 compressibilities of the a , b and c axes are distinguishable from each other (Fig. 4a inset).
261 Given that $M_a' > M_c' > M_b'$ and considering their magnitudes, the b axis would stay the
262 most compressible, $\sim 17.4\%$ smaller than the c axis and $\sim 26.5\%$ smaller than the a axis in
263 linear modulus at 330-364 GPa (Fig. 4b). The reason that the a and c axes are less
264 compressible than the b axis is that Fe ions are distributed more densely in the same a - c
265 plane than in the b direction, which makes the Fe-Fe bonds shorter and stronger in a and c
266 directions (Fig. 1). Similar to our results, theoretical calculations by Raza et al. (2015)
267 also indicated that the axial compressibilities of the orthorhombic Fe_7C_3 are discernably
268 anisotropic, and the compressibility of the b axis is most obviously different from those of
269 the other axes. The calculated sound velocity (v_p) of Fe_7C_3 in b direction is the slowest,
270 while the sound velocities in the a and c directions are relatively similar at 360 GPa (Raza
271 et al., 2015), which is consistent with our linear incompressibility results.

272 Thermal expansion of a^3 , b^3 and c^3 are also calculated using the Equation (5) (Fig.
273 5):

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$$\alpha = \frac{x_{T(P)}^3 - x_{0(P)}^3}{x_{0(P)}^3 (T - T_0)} \quad (5)$$

274

275 We found that the thermal expansions of c^3 (about $8 \times 10^{-5} \text{ K}^{-1}$) from 300K to 600K or
276 700K were larger than that of a^3 and b^3 by a factor of approximately 4, indicating that
277 there are anisotropic responses of lattice expansion to high temperature along different
278 crystallographic directions (Fig. 6). The anisotropic response was also reflected by an
279 increase in the c/a ratio upon heating (Fig. 7). The b/a ratio was nearly unchanged with
280 temperature and the b/c ratio decreased with temperature (Fig. 7). This means that the
281 significant change of the c/a ratio with temperature can be mainly attributed to the large
282 expansion of the c axis upon heating.

283 The distinct anisotropic responses could influence the compressibility and sound
284 velocities of Fe_7C_3 . For *hcp* iron, the c/a ratio also increases upon heating and the elastic
285 anisotropy changes, showing that the corresponding longitudinal modulus of c axis, C_{33}
286 decreases and becomes smaller than C_{11} (Steinle-Neumann, 2001). This suggests that an
287 expanded c axis may result in elastic softening along this crystallography direction. One
288 consequence might be a large sound velocity reduction along the c axis than the other
289 axes at high temperatures. Although the crystal structure of *hcp* iron is different from that
290 of Fe_7C_3 , the change of the c/a ratios upon heating in Fe_7C_3 , resulted from the
291 compressibilities change of the crystallographic axis, may still indicate the change of the
292 elastic anisotropy.

293 Along the isotherms, the c/a ratio gradually decreases up to ~ 40 GPa and then
294 increases abruptly (Fig. 7), probably due to the high-spin to low-spin transition of Fe_7C_3
295 (Chen et al., 2012; Chen et al., 2014). For higher temperature data, the change occurs at

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296 higher pressures: this is consistent with that high temperature would promote low-spin to
297 high-spin transition in 3d metal compounds (Gütlich et al., 1994) and probably indicates
298 a positive slope for the spin transition (Liu et al., 2016a). The spin transition may
299 have lead to the kink in the c/a ratio at ~ 40 GPa at 300K (Fig. 7). After the spin
300 transition, it appears that the c/a ratio decreases at a similar slope as before the spin
301 transition. The effect of the spin transition on the compressibilities of
302 crystallographic axes is not obvious in this study. We found it was reasonable to use
303 one linear equation of state to describe the compressibilities of crystallographic axes
304 (Fig. 4). Further studies with denser data coverage and to higher pressure are required
305 to further confirm that.

306 Temperature may significantly influence the elastic properties of Fe_7C_3 at high
307 pressures. When only pressure is taken into account, the a and c axes of Fe_7C_3 have
308 relatively similar compressibility but the b axis is more compressible. According
309 to theoretical calculations, the b axis is also the direction along which acoustic waves
310 travel the slowest (Raza et al., 2015). When temperature is considered, the c axis expands
311 more significantly than the other axes and thus becomes elastically softer at high
312 temperatures, which suggests that the acoustic wave traveling along the c axis may also
313 slow down and influence the elastic anisotropy. At high pressure and temperature
314 conditions like in the inner core, the a axis of Fe_7C_3 will stay the most incompressible
315 and thus has the highest sound velocity along a axis. Our data implies that
316 temperature is an important factor when considering the anisotropy of Fe_7C_3 at core
317 conditions and caution needs to be exercised for extrapolating to the inner-core
318 conditions.

GEOPHYSICAL IMPLICATIONS FOR EARTH'S INNER CORE

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319 Seismological data suggest that Earth's inner core exhibits strong elastic
320 anisotropy, an anomalously high Poisson's ratio and low shear-wave velocity (v_s) (Deuss
321 (2014) and the papers cited within). These seismic features are possibly linked to the
322 crystallographic anisotropy of the inner-core crystals. According to the theoretically
323 calculated Fe-C phase diagram at 330 GPa, if an Fe-C liquid has >2wt.% carbon, Fe_7C_3
324 would crystallize first to form an iron carbide inner core (Fei and Brosh, 2014); the
325 innermost inner core has been further suggested to be Fe_7C_3 based on the melting
326 experiments of the Fe-C system to core pressures (Liu et al., 2016b). With decreasing
327 core temperature and the depletion of carbon in the outer core by the growth of Fe_7C_3 in
328 the inner core, the Fe-C melt will approach the eutectic composition. C-doped Fe and
329 Fe_7C_3 would crystallize from the eutectic composition and form the outer part of the inner
330 core which surrounds the innermost inner core. Our results on the anisotropic
331 compressibility and thermal expansion of the different crystallographic axes of Fe_7C_3
332 may provide an explanation for the seismic observations of the inner core, particularly the
333 observed inner core anisotropy. The effect of temperature on the elastic properties and
334 anisotropy of Fe alloys such as Fe_7C_3 are crucial for us to construct a seismologically
335 consistent core compositional model and thus inform better understanding of the
336 composition and structure of the inner core. The thermal expansions of iron carbides at
337 high pressures are crucial for modeling the Fe-C phase relations at extreme conditions
338 (Fei and Brosh, 2014), which may inform our understanding of the mineralogy of the
339 inner core and the role of carbon during inner core crystallization.

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- 463

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464 **FIGURE CAPTIONS**

465

466 Figure 1. The crystal structure of Fe_7C_3 projected along the b axis (**left**), the a axis
467 (**upper right**) and the c axis (**lower right**) at ambient conditions (space group $Pbca$, $Z =$
468 8). Blue balls represent Fe. One carbon (pink) is located in the center of each CFe_6
469 triangular prism colored in pink.

470

471 Figure 2. Density of the orthorhombic Fe_7C_3 at 300K in this study compared with other
472 studies. The fitted density using the third-order Birch-Murnaghan EoS is also displayed
473 as the solid line. The solid circles represent the density of orthorhombic Fe_7C_3 in this
474 study. The pressure and density uncertainties are mostly within the symbols. The open
475 symbols are from other studies for comparison (Chen et al., 2012; Liu et al., 2016a;
476 Nakajima et al., 2011; Prescher et al., 2015). Inset is the F - f plot of data in this study.

477

478 Figure 3. The P - V - T data of Fe_7C_3 fitted by the high-temperature Birch-Murnaghan EoS.
479 The pressure and volume uncertainties are within the symbols. Solid curves are the fitting
480 results.

481

482 Figure 4. The compressibilities of the a , b and c axes of Fe_7C_3 as a function of pressure.
483 **(a)** The variation of a/a_0 , b/b_0 and c/c_0 as a function of pressure were fitted by the linear
484 EoS. The uncertainties are mostly within the symbols. Inset: the confidence ellipses for

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485 the a , b and c axes, illustrating the trade-off between M_0 and M' . **(b)** The calculated and
486 extrapolated linear moduli of the a , b and c axes as a function of pressure.

487

488 Figure 5. The high-temperature **(a)** a/a_0 , **(b)** b/b_0 and **(c)** c/c_0 of Fe_7C_3 versus pressure.

489 The room-temperature data were fitted by the linear EoS.

490

491 Figure 6. Thermal expansion of a^3 , b^3 and c^3 axes of Fe_7C_3 at 600K and 700K. Open
492 symbols represent the calculated thermal expansion for different axes. Dashed lines are
493 guide lines showing the thermal expansion of c^3 is approximately 4 times larger than a^3
494 and b^3 .

495

496 Figure 7. The **(a)** c/a ratio, **(b)** b/c ratio and **(c)** b/a ratio of Fe_7C_3 up to 800K as a
497 function of pressure.

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500 Table 1 The thermoelastic properties of Fe₇C₃ compared with previous studies.

<i>P</i> range (GPa)	<i>T</i> range (K)	<i>K</i> ₀ (GPa)	<i>K</i> ₀ [*]	Normalized <i>V</i> ₀ (Å ³) ^a	Thermoelastic properties	Method	Reference	
Orthorhombic (<i>Pbca</i>)								
0-79.2	300	165(4)	5.1(2)	93.2(3)	— d <i>K</i> /d <i>T</i> = -0.02(1) GPa/K	SCXRD+DAC	This study	
0-79.2	300-800	167(4)	5.0(2)	93.2(3)	<i>a</i> ₀ = 4.7(9)*10 ⁻⁵ K ⁻¹ <i>a</i> ₁ = 3(5)*10 ⁻⁸ K ⁻² ^b —	SCXRD+DAC	This study	
4-158	300	168(4)	6.1(1)	93.1 (1) Hexagonal (<i>P6₃mc</i>)	—	SCXRD+DAC	Prescher et al. (2015)	
ferromagnetic	0-18	300	201 (2)	4 (fixed)	93.2(1)	— γ(5)2.57= 0	PXRD+DAC+multianvil press	Nakajima et al. (2011)
paramagnetic	18-71.5	300-1973 [†]	253 (7)	3.6(2)	92.1 (3)	θ= 920 (140) K q = 2.2(5)	PXRD+DAC+multianvil press	Nakajima et al. (2011)
ferromagnetic			231	4.4	91			
nonmagnetic			291	4.5	88			
paramagnetic	7-53	300	201 (12)	8.0 (1.4)	92.4 (2)	—	SCXRD+DAC	Chen et al. (2012)
nonmagnetic	53-167	300	307 (6)	3.2 (1)	91.5 (4)	—	SCXRD+DAC	Chen et al. (2012)
	0	297-911	—	—		<i>a</i> ₀ = 3.1(6)*10 ⁻⁵ K ⁻¹ <i>a</i> ₁ = 1.2(6)*10 ⁻⁸ K ⁻² ^c	PXRD	Litasov et al. (2015)
ferromagnetic	0-7	300	186(5)	6.9(2.2)	93.1 (1)	—	PXRD+DAC	Liu et al. (2016a)
noncollinear	7-20	300	166(13)	4.9 (1.1)	93.5(4)	—	PXRD +DAC	Liu et al. (2016a)
paramagnetic	20-66	300	196(9)	4.9 (2)	92.3 (5)	—	PXRD +DAC	Liu et al. (2016a)

501 Notes: SCXRD and PXRD are acronyms of single-crystal XRD and powder XRD,

502 respectively.

503 ^a Normalized *V*₀ represents volume per Fe₇C₃ formula.

504 ^b The coefficient of thermal expansion was calculated as $\alpha = \alpha_0 + \alpha_1 \times (T-300)$.

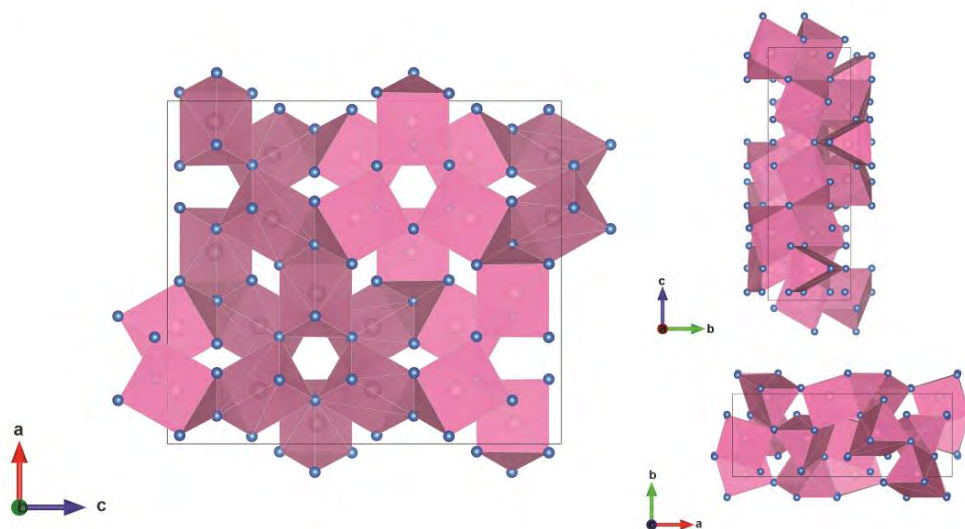
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505 ^cThe coefficient of thermal expansion was calculated as $\alpha = \alpha_0 + \alpha_1 \times T$.

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Figure 1



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508 Figure 1

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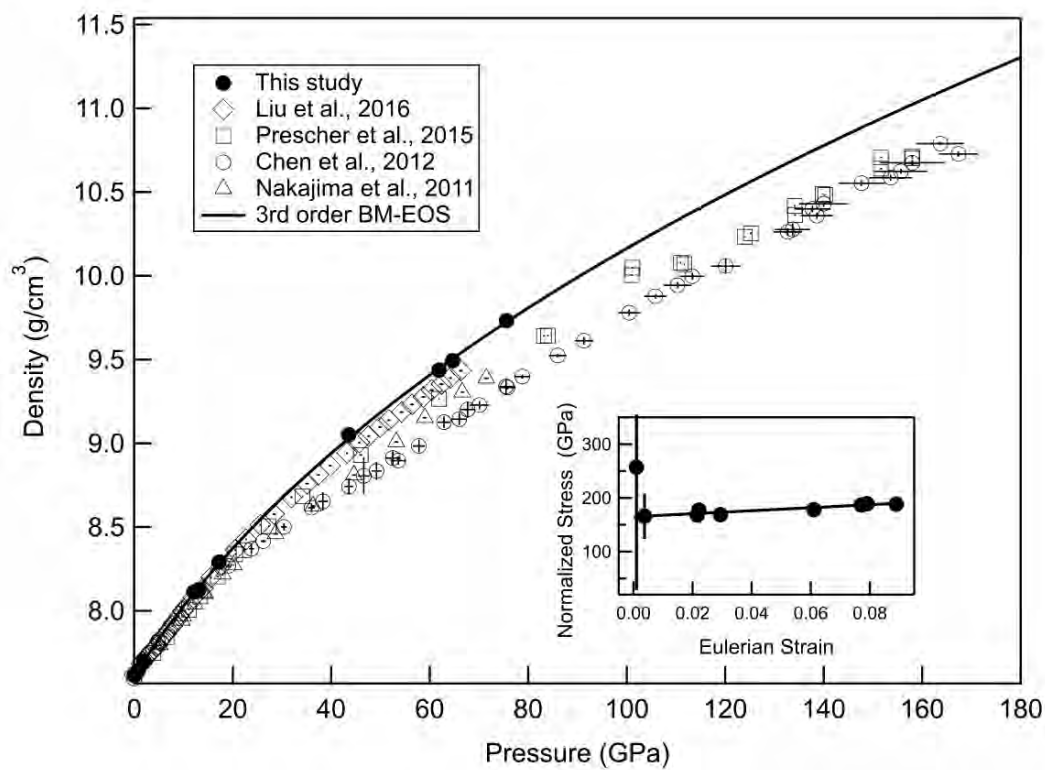
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Figure 2



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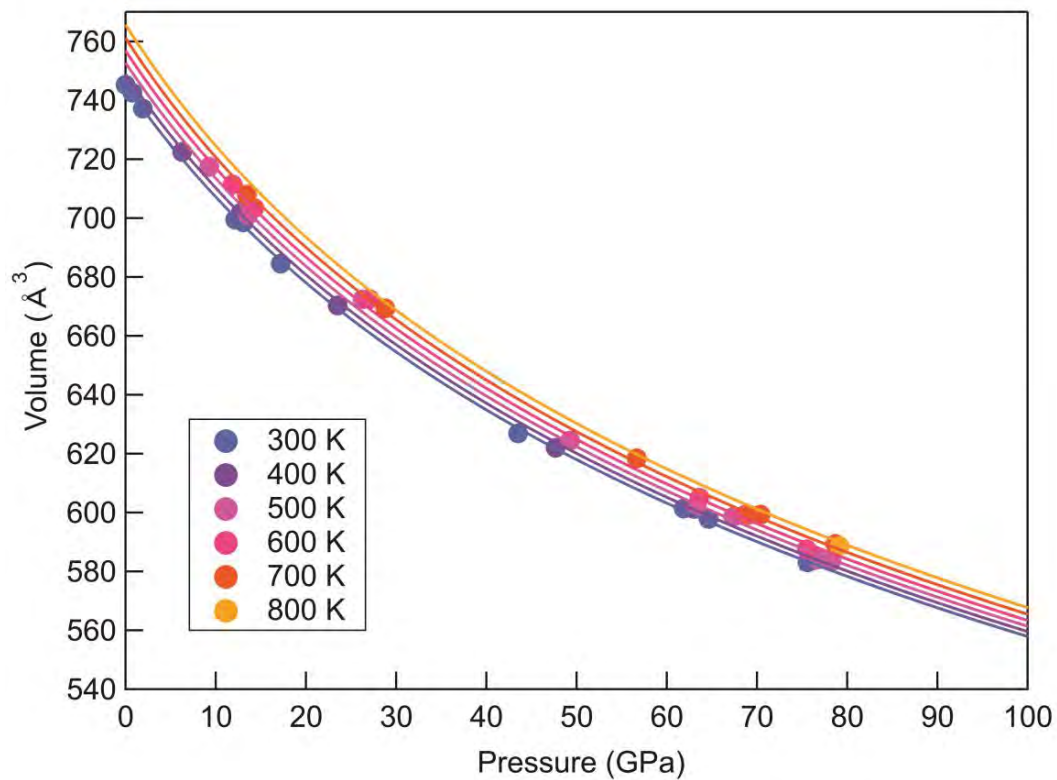
515 Figure 2

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Figure 3



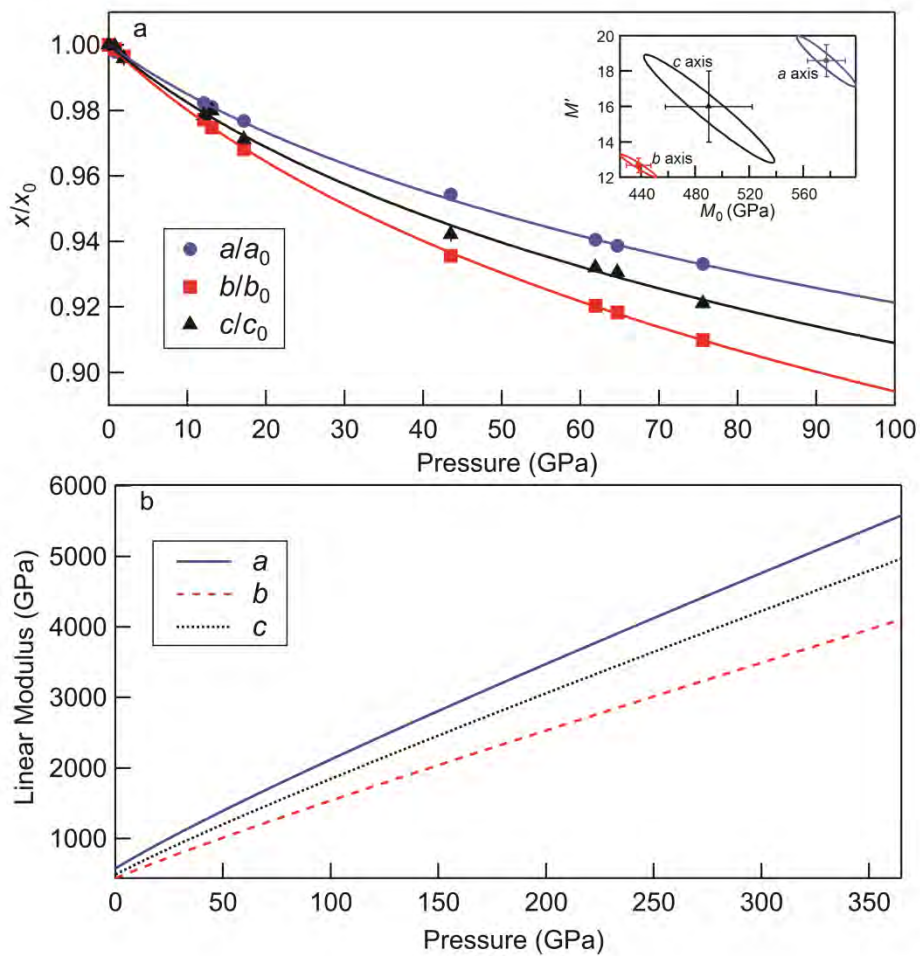
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519 Figure 3

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Figure 4

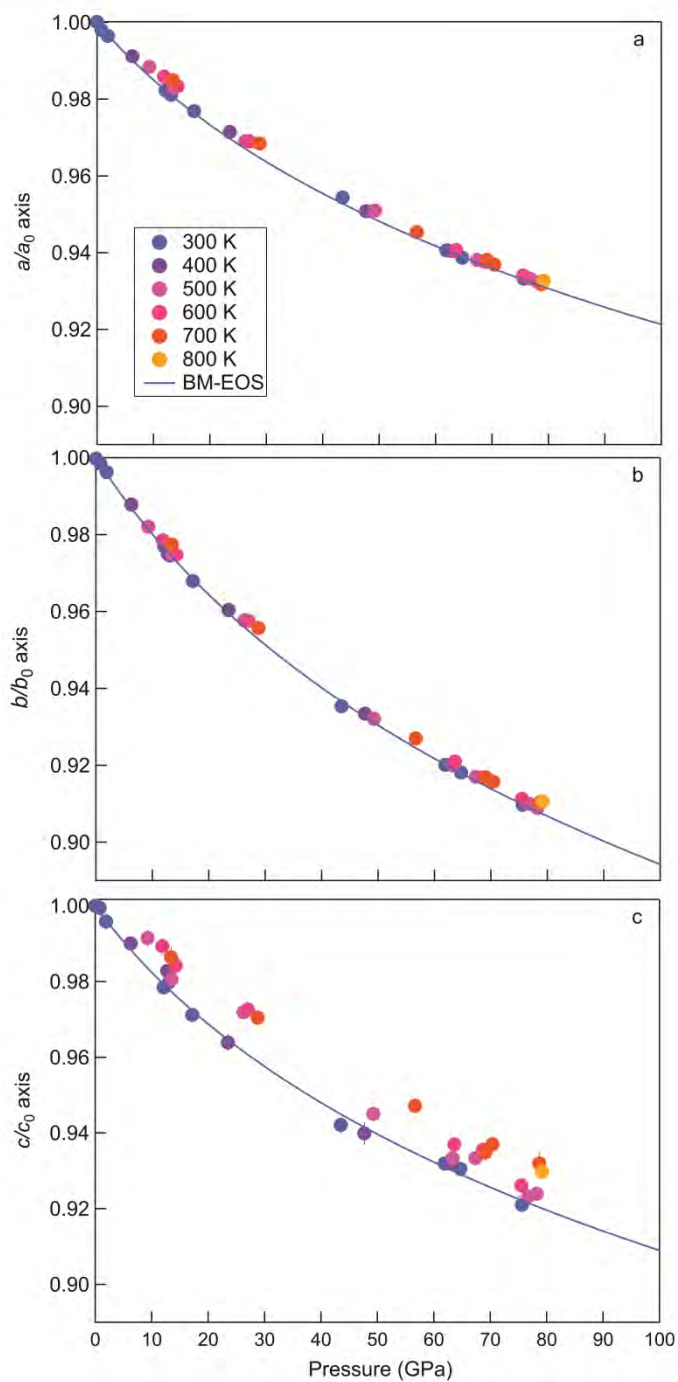


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522 Figure 4

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Figure 5

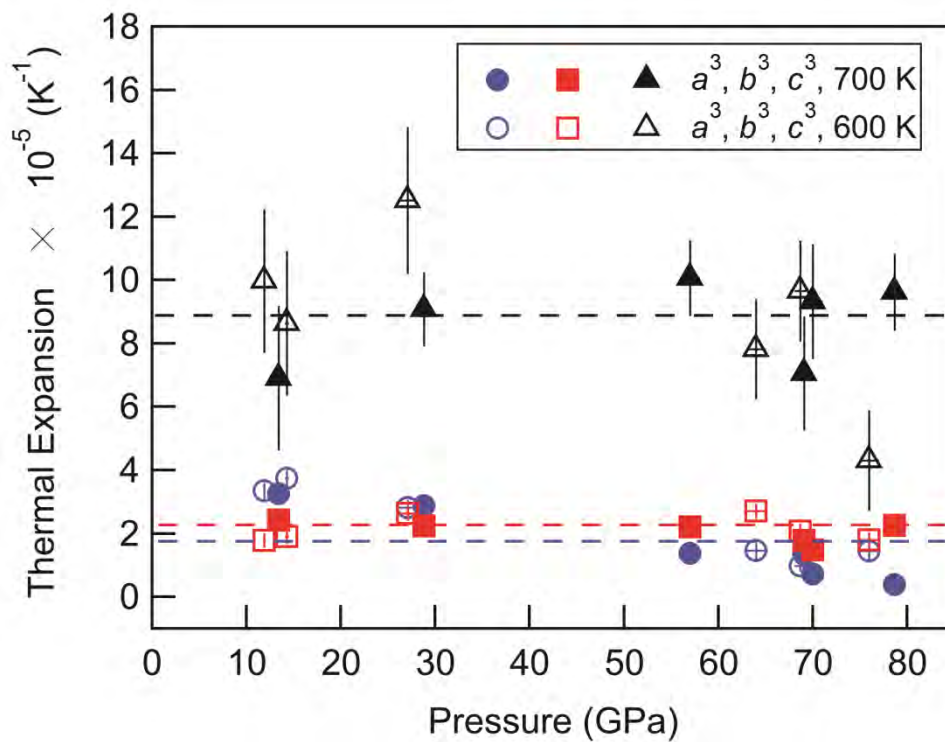


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524 Figure 5

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Figure 6

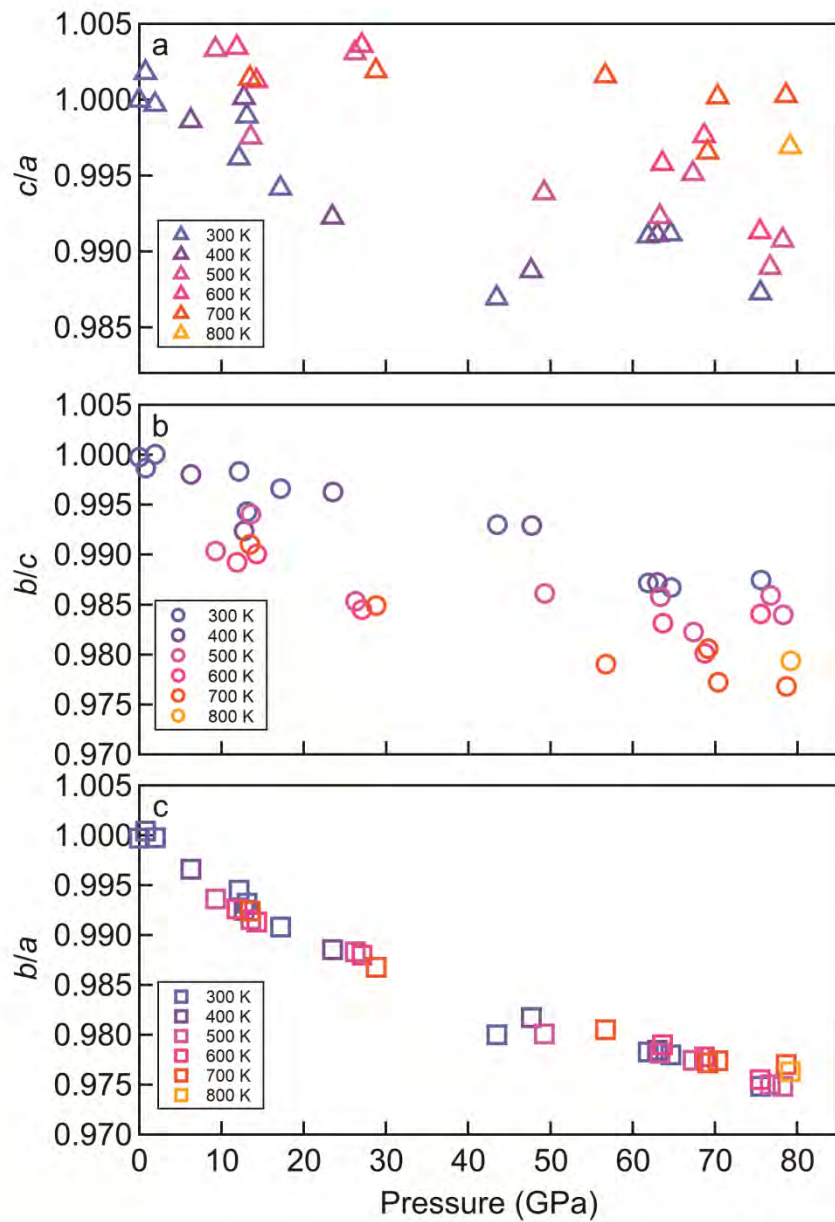


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526 Figure 6

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Figure 7



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528 Figure 7

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