1	Revision 1
2	Melting temperature depression due to electronic spin transition of iron
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Abstract

11 The electronic spin transition of iron has been shown to strongly affect many 12 physical properties of the host mineral. However, the response of melting temperatures to 13 the spin transition remains largely unexplored. Here, we study the melting of lower mantle 14 minerals, ferropericlase and bridgmanite, using Lindemann's Law. This empirical law 15 predicts a negligible melting temperature depression for Earth-relevant bridgmanite but a 16 substantial depression for Earth-relevant ferropericlase across the spin transition of iron, 17 consistent with extant experimental results. This melting depression can be explained 18 within the framework of Lindemann's Law for a Debye-like solid. The transition of iron 19 from high to low spin configuration reduces the molar volume and the bulk modulus of the 20 crystal, leading to a decrease in Debye frequency and consequently lowering the melting 21 temperature. Thermodynamically, the melting depression likely derives from a more 22 negative Margules parameter for a liquid mixture of high- and low-spin endmembers as 23 compared to that of a solid mixture. This melting depression across the spin transition of 24 iron may be the process responsible for the formation of a deep molten layer during the 25 crystallization of a magma ocean in the past, and a reduced viscosity layer at present.

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Introduction

28 Many minerals in Earth's mantle are believed to contain both ferrous and/or ferric 29 iron. Specifically, for the lower mantle, the iron content of the two major constituents, 30 (Mg,Fe)SiO₃ bridgmanite and (Mg,Fe)O ferropericlase are estimated to be 4-10 atomic% and 20-30 atomic%, respectively (Lee et al., 2004; Muir and Brodholt, 2016). Both Fe²⁺ 31 and Fe^{3+} are characterized by the partially-filled 3d electron shells and thus multiple 32 33 electronic spin states. The ionic radii and magnetic moments of iron ions with different electronic configurations in the same crystallographic site are intrinsically distinct. As 34 35 such, the spin transition of iron is expected to affect the properties of lower mantle 36 minerals. Indeed, recent experiments and first-principles simulations confirm that the spin 37 transition of iron could result in substantial changes in physical (i.e., density and bulk 38 modulus) (Tsuchiya et al., 2006; Crowhurst et al., 2008; Wentzcovitch et al., 2009; Liu et 39 al., 2018), transport (i.e., diffusivity, viscosity, electrical/thermal conductivity) (Ohta et al., 40 2007; Saha et al., 2011), and chemical (e.g., element partitioning) properties of minerals 41 (Badro et al., 2003; Shim et al., 2017).

42 Nevertheless, the effect of spin transitions on melting temperature, a fundamental 43 thermodynamic property, remains poorly constrained. Intuitively, anomalous melting 44 behavior is anticipated for a spin-crossover system like (Mg,Fe)O. This is because melting 45 is essentially governed by the energetics of the solid and liquid phases that have been 46 shown to strongly depend on the spin state of the system (Wentzcovitch et al., 2009; 47 Holmström and Stixrude, 2015; Ghosh and Karki, 2016).

48 Recently, Deng and Lee (2017) observed a pronounced melting temperature
49 depression of ferropericlase of Earth-relevant compositions at pressures greater than ~40

50 GPa where the spin transition of Fe^{2+} occurs, creating local minima in the solidus and 51 liquidus fusion curves. To our knowledge, this is the first time the effects of spin transition 52 on melting have been proposed.

53 In order to further explore the effects of the spin transition on the melting 54 temperature, we utilize the semi-empirical Lindemann's Law which states that melting 55 occurs if the mean square amplitude of atomic vibrations exceeds a critical fraction f of the 56 interatomic distance in the crystal (Lindemann, 1910; Gilvarry, 1956b). As the properties 57 of the liquid states are not explicitly considered. Lindemann's Law lacks a legitimate 58 physical basis as pointed out by many studies (e.g., Wolf and Jeanloz, 1984; Wallace, 59 1991). However, the applicability of the Lindemann's Law has been well tested for many 60 systems and some general trends have emerged. Lawson (2009) demonstrated that 61 Lindemann's Law follows from straightforward thermodynamic considerations for 62 elements of simple structure, although it does fail for others with more complicated 63 structures (Wolf and Jeanloz, 1984). Anderson (1995) concluded that Lindemann's Law is 64 applicable to densely packed (i.e., packing fraction is large) Debye-like solids for which a 65 single value of Debye temperature would suffice to describe the thermoelastic properties. 66 For example, MgO, FeO and MgSiO₃ bridgmanite are typical Debye-like solids (Anderson, 67 1998) and the predicted melting curves based on Lindemann's Law exhibit good agreement 68 with the experiments and first-principles computations (Poirier, 1989; Speziale et al., 2001; 69 Fischer and Campbell, 2010). In addition, bridgmanite with 10 atomic% iron is also 70 characterized by Debye-like thermoelastic properties (Anderson and Hama, 1999). 71 Similarly, the (Mg,Fe)O solid solution may also be a Debye-like solid given its two Debye-72 like endmembers (Anderson, 1995). As a result, Lindemann's Law is likely applicable to

ferropericlase and bridgmanite of Earth-relevant compositions before the spin crossover.
Upon the spin transition, components with different spin states are admixed, modifying the
atomic vibrations and free energies of the systems. Thus, it is uncertain whether
Lindemann's Law would still apply.

In this study, we first investigate the fusion curves of iron-bearing ferropericlase using Lindemann's Law and compare with experimental results. We focus on the spintransition pressure range and examine whether Lindemann's Law provides a satisfying prediction of the melting curve response to the spin crossover. This analysis allows us to generalize the effects of spin transitions of iron on melting temperatures. Finally, we analyze the thermodynamic meaning of melting depression and compare with other spintransition induced thermoelastic anomalies.

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Lindemann's Law

For a Debye-like solid, Lindemann's Law may be expressed as (Gilvarry, 1956a;
Gilvarry, 1956b),

88
$$T_m = C f^2 V^{2/3} \Theta_D^2$$
, (1)

89 where $T_{\rm m}$ is the melting temperature; Θ_D and V are the Debye temperature and molar 90 volume respectively at fusion; f is the critical fraction of the mean square amplitude of 91 atomic vibrations; C is a constant for a given system. Θ_D of the solid at melting is given by

92
$$\Theta_D = C' S K_T^{1/2} V^{1/6} , \qquad (2)$$

where $K_{\rm T}$ is the isothermal bulk modulus at melting; *S* is a function of Poisson's ratio and can be approximated as a constant for the Debye-like solids (Gilvarry, 1956b); *C'* is a constant for a given system.

96 Combining the above two equations yields the differential Lindemann equation97 (Gilvarry, 1956b),

98
$$\frac{d\ln T_m}{dP} = \frac{1}{K_T} (\frac{dK_T}{dP} - 1)$$
, (3)

99 where *P* is pressure. From this equation, we can infer that the melting slope is 0 if K_T' (= 100 $\frac{dK_T}{dP}$) is equal to 1.

101 We choose the differential Lindemann equation in this study to estimate the melting 102 curves for (Mg,Fe)O and (Mg,Fe)SiO₃. This is because while solid ferropericlase and bridgmanite appear to have a nearly constant K'_T (= $\frac{dK_T}{dP}$) at pure high or pure low spin 103 state, K'_r changes dramatically in the pressure range of the spin transition where the spin 104 105 state is mixed (Crowhurst et al., 2008; Marguardt et al., 2009a; Wentzcovitch et al., 2009; 106 Catalli et al., 2010; Hsu et al., 2011) and therefore should be treated as a free variable. The 107 disadvantage of this treatment is that the evaluation of $T_{\rm m}$ critically hinges on the scarcity 108 of high temperature (i.e., close to melting temperature) K'_{τ} data.

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110 Melting of (Mg,Fe)O ferropericlase across the spin transition

111 The spin transition of Fe^{2+} in (Mg,Fe)O ferropericlase is a gradual process and the 112 transition pressure range tends to broaden with increasing temperatures (Lin et al., 2007;

Glazyrin et al., 2016). The thermoelastic properties of (Mg,Fe)O ferropericlase approaching, during and upon completion of the spin-state crossover at room temperature have been extensively studied in the last decade (e.g., Crowhurst et al., 2008; Marquardt et al., 2009a; Marquardt et al., 2009b; Yang et al., 2015; Marquardt et al., 2018). The current agreement is that the spin transition strongly softens the bulk modulus while only marginally affects the shear modulus. Additionally, first-principles computations show that the softening gradually diminishes with increasing temperature (Wentzcovitch et al., 2009).

120 To our best knowledge, so far the only available bulk modulus data at high 121 temperature (close to melting temperatures) and pressure (across the spin transition 122 pressure) of $(Mg_{1-x}Fe_x)O$ ferropericlase is reported by (Wentzcovitch et al., 2009) for x = 123 0.1875. It is noted that at some low pressure and high temperature conditions (e.g., T =124 3000 K, P< \sim 50 GPa and T = 4000 K, P< 90 GPa), the quasiharmonic approximation 125 (QHA) is claimed to be invalid (Wentzcovitch et al., 2009). These P-T conditions which 126 lay outside of the QHA are inferred based on thermal expansivity, which is known to be a 127 sensitive parameter to anharmonic effects. In contrast, the bulk modulus is insensitive to 128 the anharmonicity as manifested by the relatively small temperature derivative of bulk 129 modulus (dK_s/dT) for the high-spin (Mg,Fe)O, i.e., ~-0.01-0.02 GPa/K (Yang et al., 2016). 130 Additionally, ferropericlase of (mostly) high-spin state at P-T conditions outside the 131 validity regime of the QHA exhibits similar dK_s/dT (Wentzcovitch et al., 2009). Therefore, 132 we conclude that the valid P-T conditions of the QHA reported by (Wentzcovitch et al., 133 2009) is only directly relevant to the thermal expansivity. The QHA implemented by 134 (Wentzcovitch et al., 2009) has adequately taken into account the anharmonic effects for 135 bulk modulus even at P-T conditions outside the validity range of the QHA.

136 Since only the adiabatic bulk modulus (K_s) is provided (Wentzcovitch et al., 2009), 137 we first convert $K_{\rm S}$ to $K_{\rm T}$ through $K_{\rm T} = K_{\rm S} / (1 + \alpha \gamma T)$, where α is the thermal expansion 138 coefficient, and γ is the thermodynamic Grüneisen parameter. As this study focuses on the 139 temperatures close to the melting temperatures (2000-4000 K) and pressures similar to 140 those in experiments by Deng and Lee (2017), we average the α and γ at these P-T conditions reported by Wu et al. (2009) and obtain $\alpha = 2.2 \times 10^{-5}$ K⁻¹ and $\gamma = 1.6$. These 141 142 values are very close to values determined experimentally (Tange et al., 2009; Mao et al., 143 2011). The resulting K_T' are plotted in Fig. 1a. For all the temperatures considered here 144 (i.e., 300, 1000, 2000, 3000, 4000 K), K'_T remains mostly constant at ~3.3 before ~25 GPa 145 and then gradually decreases to 1 or smaller values, indicating the existence of local 146 extrema in the melting curve according to Eq. 3.

147 Three points need clarification before proceeding any further. First, Lindemman's 148 Law is generally used for solidus in the case of incongruent melting since it describes the 149 initiation of melting. Therefore, we only consider the solidus melting temperatures hereafter. Second, in principle K_T and K'_T in Eq. 3 should be evaluated at the melting 150 151 temperature. In practice, however, we have to use the K_T and K'_T at constant temperatures 152 (i.e., 2000, 3000, 4000 K) because K_T and K'_T at other temperatures are not available (300 153 K and 1000 K are too cool to be considered relevant here). The solidus melting 154 temperatures of $(Mg_{0.8125}Fe_{0.1875})O$ at pressure < 80 GPa are ~2500-3500 K (Du and Lee, 155 2014; Deng et al., 2017; Deng and Lee, 2017; Deng et al., 2019), enveloped by the temperatures of available K_T and K'_T . It is expected that the solidus predicted by 156 Lindemann's law using K_T and K'_T at 3000 K will show the best agreement with the 157 158 experimental solidus. Third, one melting point is required as the anchor point to integrate

Eq. 3. Here we choose the solidus melting temperature of 3460 K at 40 GPa as the anchor point as most experiments (Deng and Lee, 2017) have been performed at or near this pressure to constrain the phase diagram.

162 The solidus curves calculated using K_T and K'_T at 2000, 3000 and 4000 K are 163 shown in Fig. 1b. For the melting points at pressures less than 40 GPa, experimental results 164 agree very well with the Lindemann's Law prediction regardless of K_T and K'_T used. At 165 pressures greater than 40 GPa, the agreement is best using K_T and K'_T at 2000 K, which 166 appears too low of a temperature for our expectations that the K_T and K'_T values should be 167 at the temperatures of the solid just prior to melting. A much better agreement between the 168 Lindemann's Law predictions using K_T and K'_T at 3000 K and experiments (Du and Lee, 2014; Deng and Lee, 2017) emerges once the thermal pressure (i.e., an additional ~8-13 169 170 GPa) involved in the experiments (Figuet et al., 1996) is taken into consideration (Fig. 1c). 171 Additionally, the good agreement between melting curves calculated based on the bulk 172 modulus at 3000 K and thermal pressure-corrected melting points is not strongly affected 173 by the anchor point used (Fig. S1).

The solidus melting curve predicted by Lindemann's Law with K_T and K'_T at 3000 174 175 K shows a substantial depression between ~50-100 GPa and this depression peaks at ~80 176 GPa. The melting temperature is \sim 700 K lower than that if the melting curve follows the 177 trend of melting curves of either pure high spin (HS) or low spin (LS) (Mg,Fe)O. This 178 depression can be explained as follows. The spin transition of iron from high to low tends 179 to reduce the molar volume of the crystal and significantly soften the bulk modulus, leading 180 to a decrease in Debye temperature (frequency) and consequently lowering the melting 181 temperature according to Eq. 1.

In summary, the melting temperature depression of (Mg,Fe)O across the spin transition observed in the experiments is consistent with the Lindemann's law prediction. The good agreement also validates the application of this semi-empirical law to the solidus of (Mg,Fe)O regardless of the spin crossover. In other words, the spin crossover does not appear to affect the applicability of Lindemann's Law, which may enable us to generalize the effects of the spin transition on the melting temperature.



189 Comparison of (Mg_{0.8125}Fe_{0.1875})O ferropericlase melting curves predicted FIGURE 1. 190 by Lindemann's Law with results based on experimentally-determined phase diagrams 191 (black circles) (Du and Lee, 2014; Deng and Lee, 2017; Deng et al., 2019). (a) The 192 evolution of K'_{τ} with pressure across the spin transition at 300 K (grey solid), 1000 K (grey 193 dash-dotted), 2000 K (black dashed), 3000 K (blue solid) and 4000 K (red dotted). The 194 inset panel shows the intersection of K'_{T} with 1 (horizontal line) for 2000 K, 3000 K, and 195 4000 K isotherms, corresponding to a melting slope of zero (Eq. 3). (b) Solidus curves of 196 (Mg,Fe)O predicted by Lindemann's Law with the anchor point at 40 GPa. The colors 197 represent the calculated bulk moduli at the given temperature used in the melting curve 198 calculations. (c) Same as B except the experimental data (pressures initially reported at

room temperature) are corrected for thermal pressure expected when exposed to hightemperatures (Figuet et al., 1996).

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202 Melting temperature depression for (Mg,Fe)SiO₃ bridgmanite?

 $(Mg,Fe)(Si,Fe)O_3$ bridgmanite has an orthorhombic structure with Fe^{2+} mainly 203 entering the A site (the large 8/12-fold pseudo-dodecahedral site) and Fe³⁺ in both A site 204 205 and B site (the smaller 6-fold octahedral site) depending on the amount of Al-Si 206 substitution (McCammon, 1997; Kupenko et al., 2015). The coexistence of Fe^{2+} and Fe^{3+} 207 and their complicated occupancy states cause a big challenge for the study of spin transitions in bridgmanite. The current consensus is that A-site Fe^{2+} does not undergo spin 208 transition (e.g., Lin et al., 2013; Lin et al., 2016) while the B-site Fe³⁺ undergoes a HS to 209 210 LS transition at high pressures, although the transition pressure in previous studies varies 211 [i.e., 42-63 GPa for bridgmanite of Fe₂O₃ content ~10 mol% (Catalli et al., 2010; Hsu et 212 al., 2011; Tsuchiya and Wang, 2013; Lin et al., 2016; Shukla et al., 2016a; Liu et al., 213 2018)].

Similar to (Mg,Fe)O ferropericlase, the spin transition of the B-site Fe^{3+} in 214 215 (Mg,Fe)(Si,Fe)O₃ bridgmanite is also a smooth transition with wider transition pressure ranges at higher temperatures. The thermoelastic data of Fe^{3+} -bearing bridgmanite at high 216 217 pressure and temperature as computed using density functional theory are available for $(Mg_{0.875}Fe^{3+}_{0.125})(Si_{0.875}Fe^{3+}_{0.125})O_3$ (Hsu et al., 2011; Shukla and Wentzcovitch, 2016), 218 $(Mg_{0.9375}Fe^{3+}_{0.0625})(Si_{0.9375}Fe^{3+}_{0.0625})O_3$ and 219 (Tsuchiya 2013), Wang. and $(Mg_{0.95}Fe^{3+}0.05)(Si_{0.95}Fe^{3+}0.05)O_3$ (Shukla et al., 2016a). Experimental studies on the 220

221	melting of Fe-bearing bridgmanite are available for (Mg _{0.9} Fe _{0.1})SiO ₃ (Heinz and Jeanloz,
222	1987) and (Mg _{0.88} Fe _{0.12})SiO ₃ (Knittle and Jeanloz, 1989; Zerr and Boehler, 1993). Here we
223	focus on the thermoelastic properties of $(Mg_{0.9375}Fe^{3+}_{0.0625})(Si_{0.9375}Fe^{3+}_{0.0625})O_3$ (Tsuchiya
224	and Wang, 2013) and $(Mg_{0.95}Fe^{3+}_{0.05})(Si_{0.95}Fe^{3+}_{0.05})O_3$ (Shukla et al., 2016a) for a direct
225	comparison.

226 Following the same protocol as for (Mg,Fe)O, we derive K'_T and integrate Eq. 3 to 227 obtain the melting temperature. Since the melting temperatures of bridgmanite of ~ 10 228 mol% iron are above 2000 K (Heinz and Jeanloz, 1987; Knittle and Jeanloz, 1989; Zerr 229 and Boehler, 1993), only the bulk modulus data at temperatures > 2000 K are suitable to 230 calculate the melting temperature using Lindemann's Law. We thus only present the results 231 based on the high temperature bulk modulus data (> 2000 K) (Fig. 2). The reference 232 melting point we choose is 3000 K and 24 GPa (Zerr and Boehler, 1993). For completeness, 233 we also present the analyses of literature results (Hsu et al., 2011; Tsuchiya and Wang, 234 2013; Shukla et al., 2016b; Shukla and Wentzcovitch, 2016) at lower temperatures in Fig. 235 S2 a-d.

 K'_{T} of $(Mg_{0.9375}Fe^{3+}_{0.0625})(Si_{0.9375}Fe^{3+}_{0.0625})O_{3}$ at 3000 and 4000 K and ($Mg_{0.95}Fe^{3+}_{0.05})(Si_{0..95}Fe^{3+}_{0.05})O_{3}$ at 2700 K decrease with pressure and does not show any obvious anomalies as we find with (Mg,Fe)O. This is because spin transition only marginally affects the bulk modulus of bridgmanite of ~10 mol% iron content is negligibly small at these high temperatures (Tsuchiya and Wang, 2013; Shukla et al., 2016a). As such, the spin transition of iron cannot be the main cause of the flat melting curve of bridgmanite observed by Heinz and Jeanloz (1987) and Knittle and Jeanloz (1989). The melting curves

calculated based on bulk modulus at high temperatures are in good agreement with (Zerr and Boehler, 1993) from 24 GPa to 60 GPa. At lower temperatures (Shukla and Wentzcovitch, 2016) and/or higher Fe³⁺ content (Hsu et al., 2011), a small decrease in K_T across the spin transition is apparent as observed for ferropericlase, however, not directly applicable for comparison to extant experimental data (Fig. S2a,c).

To sum up, Lindemann's Law predicts a relatively large melting slope of bridgmanite with ~10 mol% iron at 25 GPa and supports the melting curves reported by (Zerr and Boehler, 1993). Additionally, although the melting temperature depression caused by the spin transition of iron is negligible for bridgmanite with small amounts of Fe³⁺ in the B site (Hummer and Fei, 2012), melting temperature depression may be substantial when the B site Fe³⁺ content is greater such that the spin transition has a more pronounced softening on the thermoelastic properties.





258	$(Mg_{0.95}Fe^{3+}_{0.05})(Si_{0.95}Fe^{3+}_{0.05})O_3$ at 2700 K (black solid, S16) by (Shukla et al., 2016a) and
259	for $(Mg_{0.9375}Fe^{3+}_{0.0625})(Si_{0.9375}Fe^{3+}_{0.0625})O_3$ at 3000 and 4000 K (blue solid and red dotted)
260	by (Tsuchiya and Wang, 2013). (b) Solidus curves of bridgmanite predicted by
261	Lindemann's Law with reference point at 24 GPa and 3000 K according to experiments by
262	(Zerr and Boehler, 1993). Previous experimentally determined melting temperatures of
263	bridgmanite are also shown ((Mg _{0.9} Fe _{0.1})SiO ₃ by HJ87 (Heinz and Jeanloz, 1987) (red
264	squares), (Mg _{0.88} Fe _{0.12})SiO ₃ by KJ89 (Knittle and Jeanloz, 1989) (purple diamonds), and
265	$(Mg_{0.88}Fe_{0.12})SiO_3$ by ZB93 (Zerr and Boehler, 1993) (green triangles) where the pressures
266	reported already include thermal pressure. See Fig. S2 for and resulting melting
267	temperature curves computed for other compositions and lower temperatures.

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Thermodynamics of melting depression

Lindemann's Law relates the melting temperature depression caused by the electronic spin transition in iron to the decrease of the vibrational frequency of atoms. In this section, we explore the thermodynamic basis of the melting depression caused by the spin transition. We show that the fundamental thermodynamic source for the melting depression and elastic anomaly are inherently connected. We consider a pseudo-binary of isochemical HS and LS (Mg,Fe)O or (Mg,Fe)(Si,Fe)O₃. The Gibbs free energies for the liquid (*L*) and solid (*S*) are,

277
$$G^{L,S} = (1 - X_{LS})G^{L,S}_{HS} + X_{LS}G^{L,S}_{LS} + G^{L,S}_{mix}$$
(4)

where X_{LS} is the fraction of LS states. Note that for a fixed chemical composition X_{LS} is a function of pressure and temperature. $G_{mix}^{L,S}$ is the free energy of mixing and is given by,

280
$$G_{mix}^{L,S} = H_{mix}^{L,S} - TS_{mix}^{L,S}$$
 (5)

where $H_{mix}(S_{mix})$ is the enthalpy (entropy) of mixing. The volume of a mixture is

282
$$V = \left(\frac{\partial G}{\partial P}\right)_T = \left(\frac{\partial G}{\partial P}\right)_{T,X_{LS}} + \left(\frac{\partial G}{\partial X_{LS}}\right)_{T,P} \left(\frac{\partial X_{LS}}{\partial P}\right)_T,$$

283 Since
$$\left(\frac{\partial G}{\partial X_{LS}}\right)_{T,P} = 0$$
 at equilibrium (Wu *et al.*, 2009), the V is further expressed as

284
$$V = (1 - X_{LS})V_{HS} + X_{LS}V_{LS} + V^E$$
(6)

where $V_{HS/LS}$ is the volume of the HS (LS) endmember and $V^E = (\partial G_{mix}/\partial P)_{T,X_{LS}} =$ $(\partial H_{mix}/\partial P)_{T,X_{LS}}$. The isothermal bulk modulus of a mixture with a fixed chemical composition but varying X_{LS} may be expressed as,

288
$$\frac{1}{K_T} = -\frac{1}{V} \left(\frac{\partial V}{\partial P} \right)_T = \frac{1}{V} \left((1 - X_{LS}) \frac{V_{HS}}{K_{T,HS}} + X_{LS} \frac{V_{LS}}{K_{T,LS}} - \left(\frac{\partial V^E}{\partial P} \right)_T - (V_{LS} - V_{HS}) \left(\frac{\partial X_{LS}}{\partial P} \right)_T \right), (7)$$

where $K_{T,HS/LS}$ is the bulk modulus of the HS (LS) endmember. The bulk modulus depression for ferropericlase and bridgmanite upon spin transition derives from the condition,

292
$$\left(\frac{\partial V^E}{\partial P}\right)_T + \left(V_{LS} - V_{HS}\right) \left(\frac{\partial X_{LS}}{\partial P}\right)_T < 0, \tag{8}$$

The second term, $(V_{LS} - V_{HS})(\partial X_{LS}/\partial P)_T$ is always negative since $V_{LS} < V_{HS}$ and $(\partial X_{LS}/\partial P)_T > 0$ upon spin transition. For solids, the mixing of HS and LS (Mg_{1-x},Fe_x)O has long been assumed to be ideal (Tsuchiya et al., 2006; Wentzcovitch et al., 2009). In this case, the $H_{mix} = 0$ and the condition (8) is trivial. Yet, recent first-principles computations found the mixing of HS and LS (Mg_{1-x},Fe_x)O is non-ideal with $H_{mix} < 0$ and

298 at least for 0 K $\left(\frac{\partial V^E}{\partial P}\right)_T > 0$ (Holmström and Stixrude, 2015). Eq. 8 requires that

299 $(\partial^2 H_{mix}/\partial P^2)_T < (V_{HS} - V_{LS})(\partial X_{LS}/\partial P)_T$. Nevertheless, the observed softening of 300 ferropericlase, bridgmanite, and some other transition metal bearing minerals (Liu et al., 301 2014; Wu et al., 2016) suggests that Eq. 8 is met for these systems.

Both theoretical and experimental studies focus on the elastic anomaly due to spin transition of iron in the solids. For the liquid system with spin transition of iron, $(V_{LS} - V_{HS})(\partial X_{LS}/\partial P)_T < 0$ still holds. Whether or not this elastic depression still exists hinges on the relative largeness of the two terms in Eq. 8 and is unclear so far.

In contrast to the elastic anomaly where the thermodynamic parameters of a single phase (either solid or liquid) are involved, the melting depression involves the thermodynamics of both phases. To simplify the consideration here, we use the regular solution model to describe both liquid and solid phases,

310
$$H_{mix}^{L,S} = a^{L,S} X_{HS}^{L,S} X_{LS}^{L,S} , \qquad (9)$$

where $a^{L,S}$ is the Margules parameter and $X_{HS}^{L,S}(X_{LS}^{L,S})$ is the high (low) spin component fraction. At least for the solid, this simple regular solution model is justified as firstprinciples simulations yield $H_{mix}^{L,S}$ that are nearly symmetric parabolas (Holmström and Stixrude, 2015).

Melting depression discussed in the previous sections means that a portion of the solidus of the HS-LS binary is lower than the melting temperatures of both end-members. Therefore, we focus on the effects of spin states on shape of the phase loops. We first consider the melting depression in the binary system, FeO(HS)-FeO(LS) and the ternary FeO(HS)-FeO(LS)-MgO system.

321 Melting temperature depression in FeO(HS)-FeO(LS) binary system

An example of the G_{mix} -X curves (free energy of mixing-composition) for liquid and solid FeO phases at T₁ is shown in Fig 3a. The common tangent of liquid and solid G-X curves dictates the liquid and solid composition in equilibrium at T₁. The point where these two G-X curves cross yields a midrib curve which necessarily lies within the twophase field in Fig. 3b (Dehoff, 2006).



FIGURE 3. Illustration of the construction of the mid-rib curve. (a) Free energy of mixing for solid (S) and liquid (L) FeO as a function of spin states (HS, high-spin; LS, lowspin) at T_1 and a fixed pressure. The S, L curves are meant to be schematic and should not be extrapolated beyond the composition range considered here. (b) A schematic of the isobaric binary phase diagram of FeO (HS) and FeO (LS). The midrib curve (thin dashed curve) lies in between the liquidus and solidus. The three vertical dotted-dashed lines intersect with the liquidus, midrib, and solidus curves at points *l*, *m*, and *s* respectively. The

- common tangent intersects the G_{mix} of liquid and solid at point *l* and *s*, respectively. The G_{mix} of liquid and solid intersect at point *m*.
- 337 The midrib curve $T_{mid}(X)$ is defined as,

$$338 G_{mix}^S = G_{mix}^L, (10)$$

Note that G_{mix}^{S} and G_{mix}^{L} should have the same references states. Here we define the reference states for both endmembers as solid state. Therefore, for a regular solution model,

341 the Eq. 5 can be further expanded as,

$$342 \qquad \qquad G_{mix}^S = a^S X_{HS}^S X_{LS}^S + RT \left(X_{HS}^S \ln X_{HS}^S + X_{LS}^S \ln X_{LS}^S \right)$$

343
$$G_{mix}^{L} = a^{L} X_{HS}^{L} X_{LS}^{L} + RT (X_{HS}^{L} \ln X_{HS}^{L} + X_{LS}^{L} \ln X_{LS}^{L}) + X_{HS}^{L} \Delta G_{HS}^{0S \to L} + X_{LS}^{L} \Delta G_{LS}^{0S \to L}$$
(11)

344 where $\Delta G_{HS/LS}^{0S \to L}$ is the free energy change during melting for pure HS/LS endmembers and 345 may be expressed as,

346
$$\Delta G_{HS/LS}^{0S \to L} = \Delta S_{HS/LS} (\Delta T_{m,HS/LS} - T) = (S_{HS/LS}^L - S_{HS/LS}^S) (T_{m,HS/LS} - T),$$
(12)

347 where $\Delta S_{HS/LS}$ is the entropy of melting. For midrib curve, $X_{LS}^S = X_{LS}^L = X$ and $X_{HS}^S = X_{HS}^L =$ 348 1 - X. Combining this relation with Eqs. 10, 11, and 12 and solving for T_{mid} ,

349
$$T_{mid} = \frac{(a^L - a^S)X(1 - X) + (1 - X)T_{m,HS}\Delta S_{HS} + XT_{m,LS}\Delta S_{LS}}{(1 - X)\Delta S_{HS} + X\Delta S_{LS}},$$
 (13)

350 The slope of midrib curve is

351
$$\frac{dT_{mid}}{dX} = (\Delta S_{HS} - \Delta S_{LS})[(1 - X)T_{m,HS}\Delta S_{HS} + XT_{m,LS}\Delta S_{HS} + (X - X^{2})(a^{L} - a^{S})] \\
+ (-X\Delta S_{HS} + X\Delta S_{LS} + \Delta S_{HS})[-T_{m,HS}\Delta S_{HS} + T_{m,LS}\Delta S_{LS} + (1 - 2X)(a^{L} - a^{S})] \\
- (-X\Delta S_{HS} + X\Delta S_{LS} + \Delta S_{HS})^{2}$$
(14)

In order to have melting temperature depression, it is necessary to have a minimum point in the phase loops and consequently in the midrib curve as well (Fig. 3a). Mathematically, it requires that

355
$$\frac{dT_{mid}}{dX}\Big|_{X=0} = \frac{(a^L - a^S) - (T_{m,HS} - T_{m,LS})\Delta S_{LS}}{\Delta S_{HS}} < 0$$
(15)

356 and

357
$$\frac{dT_{mid}}{dX}\Big|_{X=1} = \frac{-(a^L - a^S) - (T_{m,HS} - T_{m,LS})\Delta S_{HS}}{\Delta S_{LS}} > 0$$
(16)

358 Eqs. 15 and 16 require that

359
$$(a^L - a^S) < (T_{m,HS} - T_{m,LS})\Delta S_{LS}$$
 (17)

360 and

$$361 (aL - aS) < (Tm,LS - Tm,HS) \Delta SHS (18)$$

respectively. Because $\Delta S_{HS/LS} > 0$, conditions (17) and (18) imply that a^L should be smaller than a^S in order to induce the melting temperature depression.

364 Melting temperature depression in FeO(HS)-FeO(LS)-MgO ternary system

The ternary system of FeO(HS), FeO(LS), and MgO is composed of three binary solid solutions, i.e., FeO(HS)-FeO(LS), FeO(HS)-MgO, and FeO(LS)-MgO. The solidus and liquids surfaces divide the parameter space into three regimes, i.e., pure liquid (above the liquidus surface) and pure solid (below the solidus surface), and the two-phase field where liquid and solid can coexist (Fig. 4). The midrib surface is sandwiched by the solidus and liquidus surfaces (Fig. 4). If the electronic spin crossover causes the melting temperature anomalously depressed, the midrib surface, $T_{\text{mid}}(X_{\text{LS}}, X_{\text{MgO}})$ must obey

$$372 \qquad \left. \frac{dT_{mid}}{dX} \right|_{X_{LS}=0, X_{MgO}=\text{constant}} < 0 \tag{19}$$

373 and

374
$$\frac{dT_{mid}}{dX}\Big|_{X_{LS}=1,X_{Mg0}=\text{constant}} > 0$$
(20)

375 Similar to the binary system, we first derive the expression for midrib surface. As 376 we focus on the effects of spin states on the melting temperatures, only the enthalpy of 377 mixing for FeO(HS)-FeO(LS) is considered to be non-zero for simplicity. The free energies 378 of mixing for solid and liquid are rewritten as (Mukhopadhyay et al., 1993)

$$G_{mix}^{S} = a^{S} X_{HS}^{S} X_{LS}^{S} + RT(X_{HS}^{S} \ln X_{HS}^{S} + X_{LS}^{S} \ln X_{LS}^{S} + X_{MgO}^{S} \ln X_{MgO}^{S})$$

$$G_{mix}^{L} = a^{L} X_{HS}^{L} X_{LS}^{L} + RT(X_{HS}^{L} \ln X_{HS}^{L} + X_{LS}^{L} \ln X_{LS}^{L} + X_{MgO}^{L} \ln X_{MgO}^{L})$$

$$+ X_{HS}^{L} \Delta G_{HS}^{0S \to L} + X_{LS}^{L} \Delta G_{LS}^{0S \to L} + X_{MgO}^{L} \Delta G_{MgO}^{0S \to L}$$
(21)

For a midrib surface at fixed MgO content, the midrib surface degenerates into a midrib curve. The points of this midrib curve require $X_{LS}^S = X_{LS}^L = X$, $X_{MgO}^S = X_{MgO}^L = c$, and $X_{HS}^S = X_{HS}^L = 1 - X - c$. Applying these conditions to Eq. 21, we solve for the midrib curve at constant MgO content and further differentiate it with respect to spin states (X). The results are,

$$385 \qquad \frac{dT_{mid}}{dX} \bigg|_{X=0, X_{MgO}=c} = (\Delta S_{HS} - \Delta S_{LS})[(1-c)T_{m,HS}\Delta S_{HS} + cT_{m,MgO}\Delta S_{MgO}] \\ + \frac{[(1-c)\Delta S_{HS} + c\Delta S_{MgO}][-T_{m,HS}\Delta S_{HS} + T_{m,LS}\Delta S_{LS} + (1-c)(a^{L} - a^{S})]}{(-c\Delta S_{HS} + \Delta S_{HS} + c\Delta S_{MgO})^{2}} < 0$$
(22)

386 and

$$\frac{dT_{mid}}{dX}\Big|_{X=1,X_{MgO}=c} = (\Delta S_{HS} - \Delta S_{LS})[-cT_{m,HS}\Delta S_{HS} + T_{m,LS}\Delta S_{LS} + cT_{m,MgO}\Delta S_{MgO} - (a^{L} - a^{S})c] + (-c\Delta S_{HS} + \Delta S_{LS} + c\Delta S_{MgO})[-T_{m,HS}\Delta S_{HS} + T_{m,LS}\Delta S_{LS} - (a^{L} - a^{S})(c+1)] + (-c\Delta S_{HS} + \Delta S_{LS} + c\Delta S_{MgO})[-T_{m,HS}\Delta S_{HS} + T_{m,LS}\Delta S_{LS} - (a^{L} - a^{S})(c+1)] > 0$$
(23)

As expected, Eqs. 22 and 23 degenerate to Eqs 15 and 16 respectively at c=0. For 0 < c < 1, Eqs. 22 and 23 do not give a simple relation between $a^{L} - a^{S}$ and other thermodynamic parameters. Nevertheless, some general trends could be resolved if one assumes FeO of pure high and low spin states have identical entropy of melting (i.e, $\Delta S_{HS} = \Delta S_{LS} = \Delta S$) given that the chemical species of these two systems are identical. Above inequalities yield,

394
$$a^{L} - a^{S} < \frac{(T_{m,HS} - T_{m,LS})\Delta S}{1 - c}$$
 (24)

395 and

396
$$a^L - a^S < \frac{(T_{m,LS} - T_{m,HS})\Delta S}{c+1},$$
 (25)

where 0 < c < 1. Similar to Eqs. 17, 18, the right hand side of either Eq. 24 or Eq. 25 is negative, which requires that the Margules parameter of liquid smaller than the Margules

399 parameter of solid.



400

401 FIGURE 4. Schematic of isobaric MgO-FeO(HS)-FeO(LS) ternary phase diagram. The
402 midrib surface (thin dashed curve) is located within the two-phase field where liquid (L)
403 and solid (S) coexist.

404 The microscopic meaning of Eqs. 17, 18, 24, and 25 may be described as follows. Margules parameters describe the interaction of the endmember components. Theoretical 405 computations have demonstrated that both Margules parameters a^{L} and a^{S} for the liquid 406 and solid, respectively are negative $(H_{mix}^{L,S} < 0)$ for (Mg,Fe)O at the pressure and temperature 407 conditions where the spin transition of Fe^{2+} is predicted ($G_{mix}^{L,S} < 0$), indicating that for both 408 409 liquid and solid (Mg,Fe)O, HS and LS components tend to form a random mixture 410 (Holmström and Stixrude, 2015; Holmstrom and Stixrude, 2016). Furthermore, Eqs. 17, 411 18, 24, and 25 demonstrate that the melting depression experimentally observed for (Mg,Fe)O and predicted by Lindemann's Law for (Mg,Fe)O and B-site Fe³⁺ bearing 412

413 (Mg,Fe)SiO₃ requires the tendency of forming a random mixture in the liquid phase is414 stronger than that in the solid phase.

Mathematically, the conditions for melting depression (Eqs. 17, 18, 24, 25) and elastic softening (Eq. 8) have similar forms and both are the inequality between $H_{mix}^{L,S}$ and HS/LS endmember properties. This similarity demonstrates that the fundamental source for melting depression and for elastic softening are intimately related, although it is still too early to draw the causality between Eqs. 8 and 17, 18, 24, 25 without a good understanding of the H_{mix}^{L} .

- 421
- 422

Implications

We employed Lindemann's Law to confirm the experimentally determined melting temperature depression for Earth-relevant compositions of (Mg,Fe)O ferropericlase across the spin transition. We find the elastic softening of ferropericlase caused by the electronic spin transition is intimately related to the observed melting depression through Lindemann's Law. In contrast, for Earth-relevant compositions of (Mg,Fe)SiO₃ bridgmanite, Lindemann's Law predicts melting depression would be negligibly small even if the B site Fe³⁺ transitions from the HS to LS state.

In addition to the semi-empirical Lindemann's law, a thermodynamic reasoning has been presented to demonstrate the possible connection between the fundamental sources for elastic softening and melting depression. We found that the enthalpy of mixing plays a critical role for both phenomena. Specifically, for a mixture of HS and LS, the zeroth derivative of H_{mix} governs the melting temperature depression (Eqs. 17, 18, 24, and 25);

the first derivative controls the extra volume depression (Eq. 6); the second derivative dictates the depression of bulk modulus (Eq. 8). It is interesting to note that at least for (Mg,Fe)O, the zeroth, first, and second derivatives of H_{mix} satisfy the inequalities to manifest the depression of melting temperature, volume, and bulk modulus. Whether this is merely a coincidence or a universal phenomenon for the spin transition of iron remains to be tested.

It is noted that apart from (Mg,Fe)O ferropericlase, melting temperature depression has also been observed for some alkali metals (e.g., Na, Li, K, Cs, Rb) (e.g., Young, 1991; Gregoryanz et al., 2005; Raty et al., 2007). Interestingly, these metals also exhibit thermoelastic anomalies (e.g., Martinez-Canales and Bergara, 2008). The spin-transition induced melting temperature depression for lower mantle minerals and observed melting temperature depression for alkali metals may share some fundamental similarities and await future confirmation.

448 While melting depression of ferropericlase and bridgmanite is interesting in its own 449 right, melting depression may affect Earth's overall thermochemical evolution. First, 450 melting temperature is a fundamental material property. As demonstrated above, the scale 451 of melting temperature depression for ferropericlase and bridgmanite of Earth-relevant 452 composition is relatively small as compared to the present geotherm and consequently the 453 depressed melting curves do not intersect with the present geotherm. However, during the 454 crystallization of the magma ocean in an early Earth, the melting depression may have 455 caused the formation of a partial melt layer sandwiched between solid layers within the 456 deep Earth because the crystallization temperatures of especially ferropericlase may be 457 largely depressed at similar depths. This may have some interesting feedback to the

458	evolution of the primordial mantle. Second, melting temperature can be related to other
459	material properties. For example, transport properties (e.g., self-diffusion coefficient and
460	viscosity) may be related to melting temperature through homologous temperature scaling
461	(Deng and Lee, 2017). The melting depression of ferropericlase and bridgmanite upon the
462	spin transition of iron may indicate that these minerals become less viscous (Wentzcovitch
463	et al., 2009; Ammann et al., 2011), which may further influence the mantle convection.
464	
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