High-temperature electrical measurements and thermodynamic properties of Fe₃O₄-FeCr₂O₄-MgCr₂O₄-FeAl₂O₄ spinels

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ABSTRACT

Electrical conductivity and thermopower measurements have been made on Fe₃O₄-FeCr₂O₄, Fe₃O₄-MgCr₂O₄, and Fe₃O₄-FeCr₂O₄-FeAl₂O₄ spinel solid solutions at 600 °C to 1400 °C and 1 atm. Our analysis of the data indicates that these are *n*-type small polaron conductors with, as in Fe₃O₄, electron hopping confined to the octahedral sites. If Cr³⁺ is not involved in the conduction mechanism (i.e., Fe²⁺-Fe³⁺ hopping only) then, with octahedral site hopping, the combined thermopower-electrical conductivity technique enables high-temperature cation distributions to be obtained.

On the Fe₃O₄-FeCr₂O₄ join we have found, from measurements of the independent density of states, that hopping is octahedral and involves Fe^{2+} and Fe^{3+} only at compositions with 40% or more of Fe_3O_4 , but that Cr^{3+} becomes involved in the conduction process at very $FeCr_2O_4$ -rich compositions. We have therefore excluded data on very Crrich compositions, which also exhibit high activation energies, from our estimates of cation distributions.

The thermopower and electrical conductivity data were combined with earlier results on the joins Fe_3O_4 -MgFe₂O₄, Fe_3O_4 -FeAl₂O₄, and Fe_3O_4 -MgAl₂O₄ to estimate cation distributions for compositions within the geologically important system (Mg²⁺,Fe²⁺)-(Fe³⁺,Al³⁺,Cr³⁺)₂O₄. The cation distributions were then combined with activity-composition relations and interphase partitioning data to derive a complete thermodynamic model for the complex system (Mg²⁺,Fe²⁺)(Fe³⁺,Al³⁺,Cr³⁺)₂O₄. The model, which takes explicit account of order-disorder relations, produces and successfully predicts a wide range of macroscopic thermodynamic measurements that have been made on simple and complex spinels. A computer program to generate cation distributions and activities is available from B. J. Wood.

INTRODUCTION

The importance of spinels as furnace smelting products and as petrogenetic indicators in a wide range of igneous and metamorphic rocks has been emphasized in many studies of their thermodynamic properties (e.g., Sack, 1982; Buddington and Lindsley, 1964; Irvine, 1965; Mattioli and Wood, 1988). We recently reported hightemperature thermopower and electrical conductivity measurements on Fe₃O₄-MgFe₂O₄, Fe₃O₄-FeAl₂O₄, and Fe₃O₄-MgAl₂O₄ spinel solid solutions (Nell et al., 1989) and used the results to estimate cation distributions from the model of Mason (1987). The cation distributions were subsequently combined with activity-composition relations and interphase partitioning data to develop an internally consistent thermodynamic model for (Mg²⁺, Fe^{2+})(Fe^{3+} , Al^{3+})₂O₄ spinels (Nell and Wood, 1989). Application of the model to natural spinels is limited, however, since most geologically important systems contain Cr_2O_3 or TiO₂ components. We have therefore extended our electrical measurements to Cr₂O₂-bearing spinels in the system $(Mg^{2+}, Fe^{2+})(Fe^{3+}, Al^{3+}, Cr^{3+})_2O_4$ which closely approximate the compositions of many naturally occurring members of the spinel group.

Characterization of order-disorder relations is central to the understanding of the thermodynamic properties of spinels (O'Neill and Navrotsky, 1983, 1984; Nell et al. 1989). In the system $(Mg^{2+},Fe^{2+})(Fe^{3+},Al^{3+},Cr^{3+})_2O_4$, Fe²⁺, Mg²⁺, and Al³⁺ disorder between tetrahedral and octahedral sites, whereas Cr3+, by virtue of its size and crystal field stabilization, resides on octahedral sites only (O'Neill and Navrotsky, 1983, 1984). Although Cr³⁺ is ordered, its presence influences the partitioning of the other cations between octahedral and tetrahedral sites, as will be discussed further below. In this study, we report high-temperature thermopower and electrical conductivity data on Fe₃O₄-FeCr₂O₄, Fe₃O₄-MgCr₂O₄, and Fe₃O₄-FeAl₂O₄-FeCr₂O₄ solid solutions in an attempt to characterize high-temperature order-disorder relations in $(Mg^{2+},Fe^{2+})(Fe^{3+},Al^{3+},Cr^{3+})_2O_4$ solid solutions. Cation distributions determined from quenched samples are subject to great uncertainties because of reordering during quenching (O'Neill and Navrotsky, 1983) so that in situ, high-temperature measurements are required. These have been attempted for several spinel systems (e.g., Wu and Mason, 1981; Mason, 1987; Nell et al. 1989) by measuring thermopower and electrical conductivity and assum-

		Fe ²⁺ Fe ³⁺ _{2x} Cr ₂₋₂	O4		$Fe_{x}^{2+}Mg_{1-x}Fe_{2x}^{3+}Cr_{2-2x}O_{4}$			
	<i>x</i> = 0.25	<i>x</i> = 0.50	x = 0.75		x = 0.25	<i>x</i> = 0.50	<i>x</i> = 0.75	
FeO	31.72	31.54	31.69		9.65	17.60	25.14	
Fe ₂ O ₃ *	18.51	35.91	52.10		19.85	38.62	55.55	
2 0	(1.02)	(0.76)	(0.68)		(0.30)	(0.40)	(0.56)	
MgO	0.0	0.0	0.0		14.49	9.16	4.36	
0					(0.26)	(0.10)	(0.10)	
Al ₂ O ₃	0.68	0.32	0.19		0.50	0.39	0.36	
2 5	(0.02)	(0.02)	(0.05)		(0.14)	(0.02)	(0.02)	
Cr ₂ O ₃	48.60	32.53	17.05		55.32	34.67	16.45	
2-3	(0.48)	(0.24)	(0.40)		(0.70)	(0.32)	(0.30)	
Total	99.51	100.30	101.03		99.81	100.44	101.86	
No. of analyses**	5	5	5		5	5	6	
Fe ²⁺					-			
Fe ²⁺ + Mg	1.0	1.0	1.0		0.272	0.519	0.764	
Fe ³⁺ Fe ³⁺ + AI + Cr	0.262	0.509	0.741		0.252	0.511	0.758	
Cell edge	8.3997	8.3939	8.3844		8.3661	8.3841	8.3808	
(Å)†	(2)	(3)	(5)		(3)	(5)	(4)	
% density‡	92.0	93.6	95.5		87.3	91.0	90.7	
		²⁺ Fe ³⁺ Al _{1-x} Cr _{1-x} O ₄			$_{6(2-2x)}Cr_{1/6(2-2x)}O_4$	Fe ²⁺ Fe ³⁺ Al _{1/6}	/ /	
	<i>x</i> = 0.25	<i>x</i> = 0.50	<i>x</i> = 0.75	x = 0.25	x = 0.50	x = 0.25	x = 0.50	
FeO	34.71	33.53	32.40	37.11	35.01	32.74	32.76	
Fe ₂ O ₃ *	19.50	38.33	53.95	20.63	39.02	18.71	36.81	
	(0.89)	(0.34)	(0.58)	(0.39)	(0.45)	(0.45)	(0.55)	
MgO	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Al ₂ O ₃	19.08	12.00	5.82	33.00	20.45	5.97	3.96	
	(0.13)	(0.15)	(0.03)	(1.05)	(0.11)	(0.09)	(0.09)	
Cr ₂ O ₃	26.62	16.83	8.42	9.72	6.14	42.64	28.09	
	(0.46)	(0.29)	(0.18)	(0.14)	(0.16)	(0.38)	(0.13)	
Total	99.91	100.69	100.59	100.46	100.62	100.06	101.62	
No. of analyses**	6	5	5	5	6	4	5	
Fe ²⁺								
Fe ²⁺ + Mg	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
$\frac{Fe^{3+}}{Fe^{3+} + AI + Cr}$	0.252	0.512	0.750	0.250	0.504	0.257	0.507	
Cell edge	8.3162	8.3398	8.3618	8.2556	8.3030	8.3729	8.375	
(Å)†	(4)	(6)	(7)	(5)	(3)	(5)	(15)	
V 71	89.0	87.5	92.4	89.0	87.4	90.0	91.2	

TABLE 1. Sample characterization

Note:

* Fe₂O₃ calculated from stoichiometry. Standard deviations are for total Fe.

** $\pm 1 \sigma$ values for each element are given in parentheses.

† Numbers in parentheses are $\pm 1 \sigma$ for the final decimal place.

‡ Percentage of theoretical density.

ing that the spinels are *n*-type small polaron conductors with Fe²⁺-Fe³⁺ electron hopping on octahedral sites only. The approach, in principle, should enable complete characterization of cation distributions over the entire range of compositions studied. We used the same method in our study with apparent success in some cases and in other cases more equivocal results. The data were then used, together with activity-composition measurements and interphase partitioning relations, to generate a complete thermodynamic model of $(Mg^{2+},Fe^{2+})(Fe^{3+},Al^{3+},-Cr^{3+})_2O_4$ solid solutions.

EXPERIMENTAL METHODS

Solid solutions containing x = 0.25; 0.50 and 0.75 in $Fe^{2+}Fe^{3+}_{2x}Cr^{3+}_{(2-2x)}O_4$; $Fe^{2+}_xMg^{2+}_{(1-x)}Fe^{3+}_{2x}Cr^{3+}_{(2-2x)}O_4$; and $Fe^{2+}Fe^{3+}_{2x}Al^{3+}_{(1-x)}Cr^{3+}_{(1-x)}O_4$; as well as x = 0.25 and 0.50 in $Fe^{2+}Fe^{3+}_{2x}Al^{3+}_{3/6(2-2x)}Cr^{3+}_{1/6(2-2x)}O_4$ and $Fe^{2+}Fe^{3+}_{2x}Al^{3+}_{1/6(2-2x)}$ $Cr_{3,6(2-2x)}^{3}O_4$, were used for the electrical measurements. High-density polycrystalline samples were prepared from oxide starting mixes with repeated cycles of firing and grinding in a controlled gas atmosphere. Starting materials were reagent grade Fe₂O₃, Cr₂O₃, MgO, and Al₂O₃. The MgO and Al₂O₃ were obtained from the decarbonation and dehydration of MgCO₃ and Al(OH)₃ at 1200 °C, respectively. The Fe₂O₃ and Cr₂O₃ were dried at 400 °C. All oxides were stored in a desiccator.

Stoichiometric oxide mixtures were pressed into pellets and reacted at a temperature of 1300 °C in a vertical tube furnace through which a gas stream with a CO/CO₂ ratio of 0.3/100 was passed at a flow rate of approximately 1 linear cm/s (log $P_{O_2} = -4.7$). Samples were reacted for 10 h at a time and, after 4 cycles of grinding and firing, single phase spinels were produced for every composition. Once prepared, the samples were crushed in a vibratory mill (using alumina grinding medium) and isostatically cold pressed into pellets at a pressure of 2.75 × 10⁸ Pa. The pellets were subsequently densified through sintering at 1300 °C under an atmosphere with log $P_{0_2} =$ -4.7 for 24 h. Final cell edges and percentages of the theoretical densities for each composition are reported in Table 1.

Thermopower (Q) and electrical conductivity (σ) measurements were conducted using a four-point measurement technique outlined by Nell et al. (1989). At all times, a gas mixture with a CO/CO₂ ratio of 0.3/100 was passed through the furnace at a flow rate of 1 linear cm/s. Measurements were made at 50–100 °C intervals, commencing at 1400 °C after 12 h of annealing to stabilize grain growth, down to approximately 600 °C and up again to 1400 °C. Values were recorded once thermal voltages were stable to $\pm 1\%$ over at least 30 min. Measurements taken in sequence from high to low T generally agreed with those recorded from low to high T, suggesting that equilibrium values were measured.

On the completion of the electrical measurements, the samples used for the measurements were mounted and polished for analysis by electron microprobe. Compositions are given in Table 1. Concentrations of Fe^{3+} have been calculated from stoichiometry. All the samples were chemically homogeneous single-phase spinel. No chemical zoning was observed and potential Fe depletion resulting from assimilation by thermocouple beads could not be detected. Most samples were slightly contaminated with Al_2O_3 derived from the alumina grinding medium used in the vibratory mill. The level of contamination rarely exceeds 1% by mass and is sufficiently low not to affect the electrical measurements.

RESULTS

Thermopower (Q) results for the systems $Fe^{2+}Fe^{3+}$ - $\operatorname{Cr}_{(2-2x)}^{3+}O_4$, $\operatorname{Fe}_x^{2+}\operatorname{Mg}_{(1-x)}^{2+}\operatorname{Fe}_{2x}^{3+}\operatorname{Cr}_{(2-2x)}^{3+}O_4$, $\operatorname{Fe}_{2x}^{2+}\operatorname{Fe}_{2x}^{3+}\operatorname{Al}_{(1-x)}^{3+}$ $Cr_{(1-x)}^{3+}O_4$, $Fe^{2+}Fe_{2x}^{3+}Al_{1/6(2-2x)}^{3+}Cr_{5/6(2-2x)}^{3+}O_4$, and $Fe^{2+}Fe_{2x}^{3+}-$ Al $\frac{3+}{5/6(2-2x)}$ Cr $\frac{3+}{1/6(2-2x)}$ O₄ are presented in Figures 1A, 2A, 3A, 4A, and 5A, respectively. Results obtained for Fe_3O_4 by Nell et al. (1989) are presented on each of the diagrams for comparison. Error bars on the data points correspond to a $\pm 7\%$ uncertainty in the absolute value of Q and represent an uncertainty of ± 1 °C in the maximum temperature gradient for every measurement (Nell et al., 1989). Repeated heating and cooling cycles always produced the same result within experimental uncertainty and, in that sense, the data are reversible. In Fe₂O₄-FeCr₂O₄ and Fe₃O₄-FeAl₂O₄-FeCr₂O₄ solid solutions, there is a systematic decrease in the absolute value of thermopower with Fe₃O₄ dilution (Figs. 1A, 3A, 4A, and 5A). Given the assumption of octahedral Fe²⁺-Fe³⁺ hopping, this decrease results from the substitution of Fe³⁺ by Cr³⁺ and Al3+, which decreases the ratio Fe3+/Fe2+ on octahedral sites. In Fe₃O₄-MgCr₂O₄, solid solutions Fe²⁺ and Fe³⁺ are replaced by Mg²⁺ and Cr³⁺, respectively, and the ratio Fe³⁺/Fe²⁺ on octahedral sites, as well as ther-



Fig. 1. (A) Thermopower measurements in the system Fe_3O_4 (mt)-FeCr₂O₄ (ch) as a function of temperature. Solid and open symbols in Figures 1–5 are down and up temperature measurements, respectively. Data for pure Fe_3O_4 in this and subsequent figures are from Nell et al. (1989). (B) Electrical conductivity data in Fe_3O_4 -FeCr₂O₄ solid solutions as a function of temperature.



Fig. 2. (A) Thermopower measurements in Fe₃O₄ (mt)-MgCr₂O₄ (pc) solid solutions as a function of temperature. Notice the change in sign in the temperature derivative of Q at high temperatures in the sample $(mt)_{0,25}$ (pc)_{0.75}. Error bars on the data have been omitted for clarity. Uncertainties are still, however, $\pm 7\%$ of the absolute value of Q. (B) Electrical conductivity measurements in Fe₃O₄-MgCr₂O₄ solid solutions as a function of temperature.

mopower, remains relatively constant throughout the compositional range investigated (Fig. 2A). Similar behavior has been observed in the system Fe_3O_4 -MgAl₂O₄, where a comparable situation exists (Nell et al., 1989). The 25% sample Fe_3O_4 -75% MgCr₂O₄ displays a reversal in the sign of the derivative of thermopower with respect

to temperature at approximately 1050 °C (Fig. 2A). We consider it likely that this is caused by a change in the conduction mechanism between pure Fe_3O_4 and the MgCr₂O₄-rich end of the series.

Electrical conductivity (σ) data for $Fe^{2+}Fe^{3+}_{2-}Cr^{3+}_{(2-2x)}$ -O₄, $Fe^{2+}_{x}Mg^{2+}_{(1-x)}Fe^{3+}_{2x}Cr^{3+}_{(2-2x)}O_4$, $Fe^{2+}Fe^{3+}_{2x}Al^{3+}_{(1-x)}Cr^{3+}_{(1-x)}O_4$, $Fe^{2+}Fe^{2+}_{2x}Al^{3+}_{1/6(2-2x)}Cr^{3+}_{5/6(2-2x)}O_4$, and $Fe^{2+}Fe^{3+}_{2x}Al^{3+}_{5/6(2-2x)}-Cr^{3+}_{1/6(2-2x)}O_4$ solid solutions are in Figures 1B, 2B, 3B, 4B, and 5B, respectively. Conductivity data from Nell et al. (1989) are on each diagram for comparison. There is a general decrease in the conductivity of spinel solid solutions with magnetite dilution consistent with the expected decrease in the total number of conducting sites ($Fe^{2+} + Fe^{3+}$) present.

Thermopower and conductivity data were fit to the following polynomials:

$$Q = a + b(10^4/T) + c(10^4/T)^2 \qquad \mu V/K \qquad (1)$$

and

$$\ln \sigma T = A + B(10^{4}/T).$$
(2)

The statistical significance of the second-degree term (c) in Equation 1 has been tested with the F-ratio and is only used for the compositions Fe2+Fe3+Cr3+O4 and $Fe_{0.75}^{2+}Mg_{0.25}^{2+}Fe_{1.5}^{3+}Cr_{0.5}^{3+}O_4$ where the confidence level for a quadratic relative to a linear relationship exceeds the 90% confidence level (Bevington, 1969, p. 200). It should be pointed out that, in the small polaron limit of a system with fixed carrier concentration, thermopower is independent of temperature. In Fe₃O₄ and Fe₃O₄ solid solutions, however, the carrier concentrations depend on temperature because of the disordering of Fe2+ and Fe³⁺ between octahedral and tetrahedral sites, and it is the temperature dependence of carrier concentration that is reflected by the polynomial to which thermopower has been fitted in Equation 1. The coefficients a, b, c, A, and B are reported in Table 2, and the resulting regression curves are presented as the solid lines in Figures 1-5. Error bars on the lines in Figures 1B, 2B, 3B, 4B, and 5B are $\pm 15\%$ of the mean values calculated from Equation 2 and represent the observed scatter in conductivity data.

The coefficient B in Equation 2 is proportional to the apparent activation energy (E_a)

$$B = \frac{-E_{a} \cdot e_{o}}{k \cdot 10^{4}} \tag{3}$$

where k is Boltzmann's constant, e_o is the electronic charge, and E_a is the apparent hopping energy in eV obtained from the conductivity data when temperature and compositional dependencies of carrier concentrations are neglected ($\sigma = \exp[A - (E_a \cdot e_o/kT)]/T$). Values of E_a are reported in Table 2.

ELECTRICAL BEHAVIOR AND NONSTOICHIOMETRY

In order to interpret our results, it is first necessary to be sure that the concentrations of the conducting species,



Fig. 3. (A) Thermopower measurements in Fe₃O₄ (mt)-FeAl₂O₄ (hc)-FeCr₂O₄ (ch) solid solutions measured along a pseudobinary section with the ratio of FeCr₂O₄/(FeCr₂O₄ + FeAl₂O₄) = 1/2. (B) Electrical conductivity data for the pseudobinary system (mt)_x (hc)_{1/2(1-x)} (ch)_{1/2(1-x)}.

Fe²⁺ and Fe³⁺, are known precisely. The total Fe content is, of course, known from the starting mixture and from microprobe analysis. The Fe²⁺/Fe³⁺ ratios of single phase spinels depend on f_{O_2} , however, and we wished to maintain essentially the ideal spinel stoichiometry of three cations to four O atoms. Dieckmann (1982) has determined deviations from stoichiometry of pure Fe₃O₄, and, as a starting point, we applied his equations for magnetite to estimate the stoichiometry of our complex spinel solutions. The deviation from stoichiometry, δ [= (cation va-



Fig. 4. (A) Thermopower results in Fe₃O₄-FeAl₂O₄-FeCr₂O₄ solid solutions measured along a pseudobinary section with the ratio of FeCr₂O₄/(FeCr₂O₄ + FeAl₂O₄) = 5/6. (B) Electrical conductivity data for the pseudobinary system $(mt)_x(hc)_{1/6(1-x)}$ - $(ch)_{5/6(1-x)}$.

cancies – Fe interstitials) per lattice molecule] (Dieckmann, 1982), is derived as follows:

$$\delta = \frac{(\mathrm{Fe}_{\mathrm{ss}}^{2+} - \delta)^3}{(\mathrm{Fe}_{\mathrm{ss}}^{3+} + 2\delta)^2} \, \mathrm{K}_{\nu}(a_{\mathrm{O}_2})^{2/3} (a_{\mathrm{Fe}_3\mathrm{O}_4}^{\mathrm{ss}})^{-1/3} - \frac{(\mathrm{Fe}_{\mathrm{ss}}^{3+} + 2\delta)^2}{(\mathrm{Fe}_{\mathrm{ss}}^{2+} - \delta)^3} \, \mathrm{K}_{I}(a_{\mathrm{O}_2})^{-2/3} (a_{\mathrm{Fe}_3\mathrm{O}_4}^{\mathrm{ss}})^{1/3}$$
(4)

where K_{ν} is the vacancy equilibrium constant, K_{I} the



Fig. 5. (A) Thermopower measurements in Fe₃O₄-FeAl₂O₄-FeCr₂O₄ solid solutions measured along a pseudobinary section with the ratio of FeCr₂O₄/(FeCr₂O₄ + FeAl₂O₄) = 1/6. (B) Electrical conductivity data for the pseudobinary system $(mt)_{x}$ -(hc)_{5/6(1-x)}(ch)_{1/6(1-x)}.

interstitial equilibrium constant, and the sub- and superscripts ss refer to the solid solution of interest. As an initial approximation, K_{ν} and K_{I} were assumed to be independent of composition and the f_{02} at which δ equals zero were calculated using the equilibrium constants given by Dieckmann (1982) for pure magnetite. It was found that a CO/CO₂ ratio of approximately 0.3/100 would always yield f_{02} within about two log units of the P_{02} at which δ equals zero for the solid solution compositions of interest to us in this study. This should place the experiments in a plateau region of near zero deviation from stoichiometry (Dieckmann, 1982). The assumption of vacancy and interstitial equilibrium constants that are independent of composition is questionable, however. In order to assess the applicability of the approximation, we conducted thermopower and conductivity measurements on a dilute solid solution containing 25% Fe₃O₄ and 75% MgAl₂O₄ at 900 °C over a range of f_{O_2} of six log units. This composition and temperature was selected because of the availability of Fe₃O₄ activity data (Mattioli and Wood, 1988) and because it represents the most depleted magnetite concentrations examined in our study.

Thermopower and conductivity results are compared with the calculated defect concentration profile as a function of temperature in Figures 6A-6C, respectively. Thermopower follows the defect concentration profile closely while conductivity remains constant within uncertainty over the P_{02} range of our measurements (note that f_0 , more oxidizing than approximately 10⁻⁹ are difficult to achieve with CO-CO₂ mixtures at 900 °C). The pertinent observation is that there is, as in Fe_3O_4 , a welldefined plateau in which both thermopower and electrical conductivity are insensitive to variations in P_{O_2} . This plateau extends over approximately five log units in f_{02} and corresponds to $|\delta| \leq 1 \times 10^{-3}$. The observed correspondence between thermopower and the calculated δ agrees with that expected for small polaron conduction in which Q depends on Fe^{3+}/Fe^{2+} (see Eq. 5 below). The correspondence between the calculated δ and thermopower suggests that neither K_V nor K_I varies greatly with composition, a condition also reported by Erickson and Mason (1985) for the Fe_3O_4 -Co Fe_2O_4 system.

In solid solutions where Fe³⁺ is replaced, but Fe²⁺ contents is unchanged, e.g., Fe₃O₄-FeCr₂O₄, the plateau region is displaced toward more reduced log P_{0} , values by a factor of $\frac{5}{2} \log X_{\text{FerO4}}$ (Nell and Wood, unpublished data; Aragon and McCallister, 1982) if nonstoichiometry is associated only with the Fe₃O₄ component of the solid solution. The width of the plateau region should remain the same, however, at five log units in P_{0} , at 900 °C. In a solid solution containing 25% Fe₃O₄ and 75% FeCr₂O₄, for example, the f_{0_2} at which δ equals zero at 900 °C is at log P_{0} , equal to -12.6 while it is at -10.2 for a 25% $Fe_3O_4-75\%$ MgAl₂O₄ solid solution (Fig. 6C). This is to be compared with the values for pure Fe_3O_4 (log $P_{O_2} =$ -11.1) and the gas mixture we used that gives a log P_{02} at 900 °C of -11.0. We conclude therefore that a gas mixture with a CO/CO₂ ratio of 0.3/100 should be in equilibrium with Fe₃O₄ solid solutions in which the deviation from stoichiometry is less than approximately 0.1% even when Fe_3O_4 content is diluted to 25%. As a check on this assumption, we always varied the gas composition slightly in solid solutions containing 25% Fe₃O₄ in order to test for fluctuations in the value of the thermoelectric coefficient that would serve as an indicator of deviations from stoichiometry approaching the shoulders of the plateau. None were observed. We consider, therefore, that our thermopower and conductivity data refer to stoichiometric spinels of the appropriate compositions, and that, in the region of interest, deviations from stoichiometry yield effects that are within experimental uncertainty (Figs. 6A, 6B). One of the reviewers also commented that the CO/CO₂ equilibrium is strongly temperature dependent and that use of a constant gas mixture could lead to f_{O_2} values not on the plateau at lower temperatures. The relations given by Dieckmann (1982) indicate, however, that curves of constant δ are essentially parallel to $CO-CO_2$ isopleths on a log P_{O_2} vs. temperature diagram, and that it is therefore appropriate to use a fixed gas mixture. We should also point out that our thermopower results for Fe₃O₄ (Nell et al., 1989), using a fixed gas composition, agree with the study of Wu and Mason (1981) in which great care was taken to preserve exact Fe_3O_4 stoichiometry over the temperature range 600-1500 °C.

THERMOPOWER AND CONDUCTIVITY THEORY

Electrical conductivity and thermopower measurements on spinels, although of some inherent mineralogical interest, are of most value if they can be used to cast light on the distribution of charge carriers in the crystal structure. This requires a correct interpretation of the conductivity mechanism, something that is difficult to do meaningfully in these complex phases. However, in the temperature range of our study (600–1400 °C), the measured activation energy of approximately 0.12 eV for electrical conduction in magnetite coupled with the low carrier mobility has been used by many authors to infer a small polaron mechanism. This will be discussed in more detail below.

We begin, however, with a brief review of conduction behavior in Fe_3O_4 at low temperature, where the results are more ambiguous. Kuipers and Brabers (1979) observed thermally activated drift mobilities above and be-



Fig. 6. (A) Thermopower measurements in a solid solution containing 25% Fe₃O₄ and 75% MgAl₂O₄ at 900 °C as a function of log P_{O_2} . (B) Electrical conductivity measurements in Mg_{0.75}Fe_{0.75}Al_{1.5}O₄ as a function of log P_{O_2} . (C) Defect profile for Mg_{0.75}Fe_{0.75}Al_{1.5}O₄ as a function of log P_{O_2} .

TABLE 2.	Polynomial fit p	parameters for th	e thermopower and	conductivity data sets
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System		Fe ²⁺ Fe ³⁺ _{2x} Cr ₂₋	2xO4		Fe ²⁺	Mg _{1-x} Fe ³⁺ _{2x} Cr _{2-2x} O ₄	
Composition	x = 0.25	<i>x</i> = 0.50	<i>x</i> = 0.75	x =	0.25	<i>x</i> = 0.50	<i>x</i> = 0.75
Coefficients							
a	-58.1	-91.9	-100.0	-12	24.0	-106.9	-124.5
b	4.1	6.3	3.0		5.9	2.4	7.4
С	0.0	-0.2	0.0		0.0	0.0	-0.2
A	13.742	13.081	13.389	1	2.002	12.708	13.306
в	-0.547	-0.296	-0.227	-	0.554	-0.345	-0.228
E _e (eV)	0.47	0.255	0.20		0.48	0.30	0.19
System		Fe ²⁺ Fe ³⁺ Al _{1-x} Cr _{1-x}	04	Fe ²⁺ Fe ³⁺ Al _{5/6}	_{3(2-2x)} Cr _{1/6(2-2x)} O ₄	Fe ²⁺ Fe ³⁺ Al	^{1/6(2−2x)} Cr _{5/6(2−2x)} O
Composition	x = 0.25	x = 0.50	x = 0.75	<i>x</i> = 0.25	<i>x</i> = 0.50	x = 0.25	x = 0.50
Coefficients							
а	-51.7	-78.2	-103.8	-46.1	-74.5	-48.0	-77.9
b	1.8	2.5	3.4	1.9	1.9	2.5	1.9
с	0.0	0.0	0.0	0.0	0.0	0.0	0.0
A	12.868	13.278	13,440	13.094	13.278	13.323	13.158
B	-0.447	-0.307	-0.223	-0.478	-0.286	-0.507	-0.285
E _a (eV)	0.38	0.26	0.19	0.41	0.25	0.48	0.25

low the Verwey transition (~120 K) and ascribed conduction to phonon-assisted tunnelling or hopping possibly caused by small polaron formation. Chakraverty (1980), on the other hand, proposed bipolaron formation as a result of ordering between neighboring Fe²⁺-Fe²⁺ pairs, whereas Ihle and Lorenz (1986) interpreted the electrical conductivity in terms of the superposition of small polaron band and small polaron hopping conduction. They noted however that, above 350 K, the small polaron band conduction decreases rapidly in favor of the hopping mechanism. Aragon and Honig (1988) found that the main features of the electrical conductivity and thermoelectric power measurements at temperatures above and below the Verwey transition can be described with a small polaron model when the thermal dependence of the density of states is taken into account. Other mechanisms that have been proposed include intermediate polaron formation with long-range ordered Fe²⁺-Fe³⁺ pairs being responsible for conduction and charge density waves where itinerant electrons are the charge carriers (Goodenough, 1980). Following this analysis, Ghose (1988) also considered the possibility of intermediate polaron formation at low temperatures in his discussion of the electrical conduction of ilvaite. At temperatures above 310 K, however, the gradual loss of long-range order destroys the Fe²⁺-Fe³⁺ pairs, and at temperatures above 405 K, all long-range order is lost and conduction is dominated by small polaron hopping.

Most of the possible low-temperature conduction mechanisms are excluded at the high temperatures (600-1400 °C) at which our experiments were conducted. The loss of long- and short-range Fe³⁺-Fe²⁺ and Fe²⁺-Fe²⁺ order with increasing temperature argues against the presence of intermediate polarons and bipolarons, respectively; whereas, itinerant electron conduction is inconsistent with the small activated drift mobilities observed for magnetite (Dieckmann et al., 1983) and magnetite solid solutions at high temperatures (e.g., Nell et al., 1989). The transition temperature from band type behavior (see below) to hopping motion for small polarons has been estimated to be approximately $\theta/2$ where θ is the Debye temperature (Austin and Mott, 1969). This agrees with the result of Ihle and Lorenz (1986) that conduction resulting from hopping dominates in Fe₃O₄ above 350 K given that θ for Fe₃O₄ is approximately 605 K (Grønvold and Sveen, 1974). Small polaron hopping should therefore dominate in the temperature range of our study, a conclusion reached on the basis of the moderate activation energy and low drift mobility observed by Verwey et al. (1947), Tannhauser (1962), Dieckmann et al. (1983), and Mason and Bowen (1981), among others. The remaining question, however, is whether electron hopping takes place between octahedral sites only, between tetrahedral sites only, or involves both types of sites.

In a study of intervalence charge transfer in silicates, Amthauer and Rossman (1984) found that small polaron hopping between Fe^{2+} and Fe^{3+} only occurs if these ions occupy equivalent or geometrically similar nearest-neighbor sites that share common edges or faces to form infinite chains, sheets, or three-dimensional networks. This observation was explained by the molecular orbital calculations of Sherman (1987) who investigated several mixed valence Fe-O clusters with edge-sharing cation polyhedra. In the case of Fe^{2+} and Fe^{3+} octahedra sharing an edge, the t_{2g} atomic orbitals of the two ions overlap to some extent, giving partial metal-metal bonding thereby facilitating electron transfer. In the spinel structure, octahedral sites form infinite edge-sharing networks with one another, but share corners with tetrahedral sites. The tetrahedral sites are isolated from one another. Therefore in spinel, octahedral-octahedral electron hopping is favored over octahedral-tetrahedral or tetrahedral-tetrahedral transfer.

High-temperature electrical conductivity data for Fe₃O₄ were correlated with the product of the concentrations of Fe²⁺ and Fe³⁺ on octahedral sites only by Tannhauser (1962), Dieckmann et al. (1983), and Mason and Bowen (1981) while Verwey et al. (1947) and Bannerjee et al. (1967) also interpreted their conductivity results in terms of electron hopping on octahedral sites based on the assumption (now known to be a poor approximation) of inverse cation distributions at high temperatures. In all studies, the hopping energy was found to be approximately 0.12 eV. Independent evidence for electron hopping between octahedral sites in magnetite has been provided by Mössbauer studies where absorption ascribed to Fe^{2,5+} on the octahedral sites is observed (e.g., Kündig and Hargrove, 1969). Thermally activated electron hopping on octahedral sites was also observed by Lotgering and Van Diepen (1977) in a Mössbauer study of Zn-Ti ferrites between 78 K and 300 K. We infer therefore that experimental and theoretical evidence is heavily in favor of octahedral hopping in pure Fe₃O₄ and presumably also in ferrites close to magnetite in composition.

The assumption of electron hopping on octahedral sites only enabled Wu and Mason (1981) to estimate the partitioning of Fe^{2+} and Fe^{3+} between octahedral and tetrahedral sites in magnetite from their measurements of the thermoelectric coefficient. Given that there is no local Fe^{2+} - Fe^{3+} order in the structure and that electron-electron repulsion is sufficiently large to prevent double occupancy of a given site, the thermoelectric coefficient (Q) for an *n*-type small polaron conductor is given by

$$Q = -\frac{k}{e_{o}} \left\{ \ln \left[2 \left(\frac{1^{6} F e^{3+}}{1^{6} F e^{2+}} \right) \right] + A \right\} \quad V/K$$
 (5)

(Chaikin and Beni, 1976; Wu and Mason, 1981; Austin and Mott, 1969) where k is Boltzmann's constant, e_o is the electronic charge, and A is the vibrational entropy associated with the ions surrounding a polaron on a given site. If conduction takes place in systems where the conducting sites all have approximately the same energy (e.g., the octahedral spinel sublattice) A is assumed to be negligibly small (Austin and Mott, 1969; Emin, 1975). From Equation 5 it is clear that the thermoelectric coefficient directly gives the ratio (Fe³⁺/Fe²⁺) on octahedral sites. provided the conditions of disorder and single occupation are fulfilled. In that case Q is sufficient to fully characterize cation distributions in Fe₃O₄ and in solid solutions such as Fe₃O₄-FeCr₂O₄ where only Fe²⁺ and Fe³⁺ are disordered between octahedral and tetrahedral sites. Wu and Mason (1981) measured the thermoelectric coefficient of magnetite at high temperature and, based on the assumption of octahedral site electron hopping, showed that the Fe²⁺-Fe³⁺ distribution changes as anticipated from almost completely inverse (low 16]Fe3+/16]Fe2+) at low temperatures to essentially completely disordered at temperatures close to 1500 °C. As Fe₃O₄ is diluted by other components, the same conduction mechanism should apply at least over limited ranges of solid solution, enabling cation distributions to be determined in more complex spinels. In Fe₃O₄-MgCr₂O₄ and Fe₃O₄-FeAl₂O₄-FeCr₂O₄ solid solutions, however, three cations (Fe²⁺, Fe³⁺, Mg²⁺ and Fe²⁺, Fe³⁺, Al³⁺, respectively) are disordered and additional information is required to derive the intersite cation distributions. In these cases, measurement of the electrical conductivity (σ) provides the required data if the conduction mechanism is unchanged.

In the adiabatic limit of small polaron transport, the probability that an electron will respond rapidly enough to a coincidence event to execute a successful hop is approximately equal to 1 (Holstein, 1959; Tuller and Nowick, 1977), and the electrical conductivity for the small polaron conductor in this limit is given by

$$\sigma = \frac{Nc'(1 - c')ga^2e_{o}^2\nu_o}{kT}\exp\left(\frac{-E_H}{kT}\right) \quad (\Omega \text{cm})^{-1} \quad (6)$$

(Tuller and Nowick, 1977; Dieckmann et al., 1983), where g is a geometric factor that is constant for a given system, a is the jump distance (cm), v_0 is the lattice vibration frequency, N is the density of conducting sites (cm⁻³), c'is the fraction of conducting sites occupied by charge carriers, (1 - c') is the fraction of available jump sites, E_{μ} is the hopping energy, and the remaining terms have their usual meaning. In the case of spinels with electron hopping on octahedral sites only, $c' = {}^{[6]}Fe^{2+}/({}^{[6]}Fe^{2+} +$ ${}^{[6]}\text{Fe}^{3+}$, $(1 - c') = {}^{[6]}\text{Fe}^{3+}/({}^{[6]}\text{Fe}^{2+} + {}^{[6]}\text{Fe}^{3+})$, and N becomes the total concentration ${}^{[6]}Fe^{2+} + {}^{[6]}Fe^{3+}$. By normalizing the electrical conductivity of a mixed spinel to that of pure Fe_3O_4 (N = 2.0), the total concentration of ${}^{[6]}Fe^{2+} + {}^{[6]}Fe^{3+}$ can be calculated for the composition of interest (Mason, 1987; Nell et al., 1989). Measurement of ${}^{[6]}Fe^{3+/[6]}Fe^{2+}$ and ${}^{[6]}Fe^{2+} + {}^{[6]}Fe^{3+}$ allows complete calculation of cation distributions in Fe₃O₄-MgCr₂O₄ and Fe_3O_4 -FeAl₂O₄-FeCr₂O₄ solid solutions.

In our previous work (Nell et al., 1989) on the joins Fe_3O_4 -MgFe₂O₄, Fe_3O_4 -FeAl₂O₄, and Fe_3O_4 -MgAl₂O₄, we found that dilution of Fe_3O_4 with the additional components brought changes in Q and σ which are consistent with the conduction mechanism remaining unchanged from $X_{Fe_3O_4}$ of 1.0 down to at least 0.25. By assuming that only octahedral hopping occurs and using Equations 5

and 6, we obtained cation site occupancies and activation energies that varied monotonically with composition. Furthermore, partitioning of Fe^{2+} and Fe^{3+} between octahedral and tetrahedral sites was found to closely obey the spinel model of O'Neill and Navrotsky (1983, 1984), which was derived from a wide variety of data on a large number of unary and binary spinels. Our results are therefore consistent with octahedral hopping only of Fe^{2+} - Fe^{3+} in these systems.

Although octahedral hopping appears to dominate in spinels, application of Equations 5 and 6 may still become invalid if other electron donors or acceptors, such as Cr³⁺ or Ti⁴⁺, are present and involved in conduction. Bannerjee et al. (1967) and Verwey et al. (1947), for example, found evidence for a transition from octahedral site electron hopping between Fe²⁺ and Fe³⁺ to a different type of conduction mechanism with increasing magnetite dilution in the systems Fe₃O₄-Fe₂TiO₄ and Fe₃O₄-Mg- Cr_2O_4 , respectively. In both systems, inflection points in plots of the activation energy of hopping vs. composition indicate a transition from hopping of Fe²⁺-Fe³⁺ between octahedral sites (activation energies of approximately 0.15 to 0.25 eV) to a different type of conduction mechanism (activation energies of approximately 0.4-0.5 eV). In view of the large energy barriers expected for tetrahedral and mixed site electron hopping, the observed second conduction mechanisms can probably be attributed to electron hopping between Fe²⁺ and Ti⁴⁺ and Fe²⁺ and Cr³⁺, respectively (D. Sherman, personal communication). Large compositional dependencies of activation energy are not, however, observed in any of the systems in which Fe²⁺ and Fe³⁺ are diluted by Mg²⁺ and Al³⁺ (Nell et al., 1989), presumably because neither of the latter ions can contribute to conduction.

Our data support the suggestion that Cr3+ becomes involved in the electron hopping process. Figure 7 shows activation energy as a function of composition for the join Fe₃O₄-FeCr₂O₄. In the FeCr₂O₄-rich region of the join ($X_{\text{FeCr}_2O_4} \ge 0.75$), activation energies for conduction are constant at approximately 0.5 eV. In more Fe₃O₄-rich compositions, activation energy increases monotonically from 0.13 eV to 0.25 eV with increasing FeCr₂O₄ content. There appears to be a region of rapidly increasing activation energy between 0.6 and 0.75 $X_{\text{FeCr}_{2}O_4}$. Our provisional interpretation of the data was that in the region 0 $\leq X_{\text{FeCr}_2O_4} \leq 0.6$, conduction is by octahedral hopping between Fe²⁺ and Fe³⁺ only, whereas the more Cr-rich compositions exhibit mixed Fe²⁺-Fe³⁺-Cr³⁺ electron transfer. As a test of this hypothesis, we applied Equations 5 and 6 to the values of thermopower and electrical conductivity of Fe₃O₄-FeCr₂O₄ solid solutions. In this case, if octahedral hopping between Fe²⁺ and Fe³⁺ is the sole mechanism, then with Cr present only on octahedral sites, Equations 5 and 6 enable us to calculate N, the densities of conducting $(Fe^{2+} + Fe^{3+})$ sites and to compare them with the expected values of 1.5, 1.0, and 0.5 for 75, 50, and 25 mol% Fe₃O₄, respectively. The data reveal excellent agreement between calculated and nominal N values



Fig. 7. Apparent hopping energies in the system Fe_3O_4 -FeCr₂O₄ as a function of composition.

over the entire temperature range 600 °C to 1400 °C for solid solutions containing 75 and 50% Fe₃O₄. For the composition containing 25 mol% Fe₃O₄ however, the data give physically impossible values requiring a change in conduction mechanism. We conclude therefore that octahedral Fe²⁺-Fe³⁺ hopping almost certainly occurs at Fe_3O_4 concentrations to 40% on this join but not at more FeCr₂O₄-rich compositions. We also consider that inflection points in plots of activation energy vs. composition (Fig. 7) are likely wherever there is a change in the conduction mechanism. Such inflections in activation energy were found in the binaries Fe₃O₄-FeCr₂O₄ and Fe₃O₄-MgCr₂O₄ and for two joins we studied in the Fe₃O₄-FeAl₂O₄-FeCr₂O₄ ternary (Table 2). In the case of Mg- Cr_2O_4 , unusual thermopower results were also observed in the 25% Fe₃O₄ composition (Fig. 2A).

In conclusion, we should state that we are unable to prove conclusively that octahedral Fe²⁺-Fe³⁺ hopping is the sole mechanism operating in the complex spinels we have studied. The experimental and theoretical evidence in favor of its operating in pure Fe₃O₄ is, however, overwhelming. Furthermore, conductivity results on the joins Fe₃O₄-FeAl₂O₄, Fe₃O₄-MgFe₂O₄, and Fe₃O₄-MgAl₂O₄ exhibit only small increases in activation energy with Fe₃O₄ dilution, and calculated cation distributions are crystallographically reasonable. On the Fe₃O₄-FeCr₂O₄ join, the assumption of Fe²⁺-Fe³⁺ hopping gives the correct concentration of $(Fe^{2+} + Fe^{3+})$ on octahedral sites at up to 50% FeCr₂O₄ substitution, confirming octahedral Fe²⁺-Fe³⁺ hopping. Changes in conduction mechanism have also been recognized by sharp increases in activation energy and independently confirmed on the Fe₃O₄-FeCr₂O₄ join from the density of states calculations. We therefore believe that, after excluding data at 75% Cr3+ substitution for Fe³⁺, we are justified in using Equations 5 and 6 to estimate cation distributions in these complex spinels.

CATION DISTRIBUTIONS

Cation distributions in Fe_3O_4 -FeCr $_2O_4$, Fe_3O_4 -Mg-Cr $_2O_4$, and Fe_3O_4 -FeAl $_2O_4$ -FeCr $_2O_4$ solid solutions were



Fig. 8. (A) Cation distributions on the join $\text{Fe}_3\text{O}_4\text{-}\text{Fe}\text{Cr}_2\text{O}_4$ at 1400 °C plotted as a function of $\text{Fe}\text{Cr}_2\text{O}_4$ mole fraction (X_{chr}) . Solid curves are distributions calculated from the model (see text). (B) Activity-composition relations in $\text{Fe}_3\text{O}_4\text{-}\text{Fe}\text{Cr}_2\text{O}_4$ solid solutions calculated at 1227 °C. Also shown are data from Katsura et al. (1975) at 1227 °C and Petric and Jacob (1982a) at 1400 °C.

calculated from the mass-balance, charge-balance, and stoichiometry conditions listed in Table 3. At fixed mole fraction (x) of Fe₃O₄ in Fe₃O₄-FeCr₂O₄ solid solutions, only the thermoelectric coefficient is required to determine cation distributions since $N = {}^{[6]}\text{Fe}^{2+} + {}^{[6]}\text{Fe}^{3+} = 2X_{\text{Fe}_3\text{O}_4}$. In Fe₃O₄-MgCr₂O₄ and Fe₃O₄-FeAl₂O₄-FeCr₂O₄ solid solutions, N was calculated from electrical conductivity measurements (Nell et al., 1989; Mason, 1987), which then allowed calculation of cation distributions



Fig. 9. Cation distributions on the join $\text{Fe}_3\text{O}_4\text{-MgCr}_2\text{O}_4$ at 1000 °C plotted as a function of mole fraction MgCr_2O_4 (X_{pchr}). Solid curves are distributions calculated from the model.

through the relationships in Table 3. Uncertainties in the cation distributions were calculated by considering maximum uncertainties in the thermopower and conductivity measurements as outlined by Nell et al. (1989). Results for each system are presented in Figures 8A, 9, and 10 together with calculated distribution curves (see below).

THERMODYNAMIC MODEL

Our estimates of cation distributions may be combined with data on activity-composition relations and interphase partitioning to construct a thermodynamic model for (Mg²⁺,Fe²⁺)(Fe³⁺,Al³⁺Cr³⁺)₂O₄ spinels that makes explicit provision for all order-disorder relations. We will commence with outlining the approach. The thermodynamic properties were formulated as an extension of our previous work on (Mg²⁺,Fe²⁺)(Fe³⁺,Al³⁺)₂O₄ solid solutions (Nell and Wood, 1989). There are ten independent fictive normal and inverse reference components in (Mg²⁺,Fe²⁺)(Fe³⁺,Al³⁺Cr³⁺)₂O₄ solid solutions that were used to derive mixing properties (Table 4). The reference components are related through three independent compositional exchange vectors, $Fe^{2+}(Mg^{2+})_{-1}$, $Al^{3+}(Fe^{3+} +$ $(Cr^{3+})_{-1}$, and $(Cr^{3+}(Al^{3+} + Fe^{3+})_{-1})$, and three compositional parameters are required to express the bulk chemical composition of any particular phase. These parameters are labeled r_1 , r_2 , and r_3 and are defined as follows:

and

$$r_3 = {}^{[6]}X_{\rm Cr}$$
 (7)

where ^[6]X_{Cr} refers to the atomic fraction of Cr³⁺ on oc-

 $r_{1} = 1 - ({}^{[4]}X_{Mg} + 2{}^{[6]}X_{Mg})$ $r_{2} = {}^{1/2}({}^{[4]}X_{A1} + 2{}^{[6]}X_{A1})$



Fig. 10. Cation distributions along the pseudobinary system $(mt)_x(hc)_{1/2(1-x)}(ch)_{1/2(1-x)}$ at 1100 °C plotted as a function of $(1 - mole fraction Fe_3O_4, i.e., 1 - X_{mt})$. Solid curves are model calculations.

tahedral sites. There are also four intersite cation exchange reactions between the reference end-member components, three of which are independent. The three selected order parameters are labeled s_1 , s_2 , and s_3 and are defined as follows (s_3 was formulated as an absolute rather than a difference quantity in order to facilitate comparison between the series expansion model and our earlier O'Neill-Navrotsky formalism, Nell et al., 1989):

 $S_1 = {}^{[6]}X_{A1} - {}^{1}/{2}{}^{[4]}X_{A1}$

 $S_2 = {}^{[6]}X_{Fa3+} - {}^{1/2}{}^{[4]}X_{Fa3+}$

and

$$s_3 = 2^{[6]} X_{Mg}.$$
 (8)

TABLE 3. Compositional relations and constraints in Fe_3O_4 -FeCr₂O₄, Fe₃O₄-MgCr₂O₄, and Fe₃O₄-FeAl₂O₄-Fe-Cr₂O₄ solid solutions

$(Fe_{3}O_{4})_{x}(FeCr_{2}O_{4})_{1-x}$ $Fe_{a}^{2+}Fe_{3}^{3+}(Fe_{\sigma}^{2+}Fe_{\sigma}^{3+}Cr_{n})_{2}O_{4}$ $a + b = 1$ $d + e + n = 2$ $2(a + d) + 3(b + e + n) = 8$
b+e=2x
$(Fe_3O_4)_x(MgCr_2O_4)_{1-x}$
Fe ²⁺ _a +Fe ³⁺ Mg _c (Fe ²⁺ _d +Fe ³⁺ Mg _i Cr _n) ₂ O ₄
a+b+c=1
d + e + f + n = 2
2(a + d + c + f) + 3(b + e + n) = 8
a+b+d+e=3x
b+e=2(a+d)
$(Fe_{3}O_{4})_{x}(FeAl_{2}O_{4})_{y(1-x)}FeCr_{2}O_{4(1-y)(1-x)}$
Fe ²⁺ _a Fe ³⁺ _b Al _c (Fe ²⁺ _d Fe ³⁺ _a Al _t Cr _n) ₂ O ₄
a+b+c=1
d + e + f + n = 2
2(a + d) + 3(b + c + e + f + n) = 8
b + e = 2x
(c+f)/(c+f+n)=y

Compo- nent*										
	Mg(AI) ₂ O ₄	Al(MgAl)O₄	Fe ²⁺ (Fe ³⁺) ₂ O ₄	Fe ³⁺ (Fe ²⁺ Fe ³⁺)O ₄	Fe ²⁺ (AI) ₂ O₄	AI(Fe ²⁺ AI)O ₄	Mg(Fe ³⁺)₂O₄	Fe ³⁺ (MgFe ³⁺)O ₄	Fe(Cr) ₂ O₄	Mg(Cr) ₂ O
Number	1	2	3	4	5	6	7	8	9	10
Parameter	r									
<i>r</i> ₁	0	0	1	1	1	1	0	0	1	0
r2	1	1	0	0	1	1	0	0	0	0
r3	0	0	0	0	0	0	0	0	1	1
S	1	0	0	0	1	0	0	0	0	0
S2	0	0	1	0	0	0	1	0	0	0
5.	0	1	0	0	0	0	0	1	0	0

TABLE 4. Fictive end-members of normal and inverse spinel in Fe₃O₄-FeAl₂O₄-MgFe₂O₄-MgAl₂O₄-FeCr₂O₄-MgCr₂O₄ solid solutions

Six parameters are thus required to characterize composition and order in $(Mg^{2+},Fe^{2+})(Fe^{3+},Al^{3+}Cr^{3+})_2O_4$ spinels. The coordinates of the reference components in the six parameter space are in Table 4, and cation fractions per structural formula unit are in Table 5. From the information in Table 5, the configurational entropy of a solid solution (S_{conf}) may be expressed as a function of order and compositional parameters through the equation

$$S_{\text{conf}} = -\mathbf{R} \sum_{a} \sum_{i} n_{a} X_{i,a} \ln(X_{i,a})$$
(9)

where n_a is the number of sites (a) per formula unit and $X_{i,a}$ is the mole fraction of component i on site a.

The vibrational part of the Gibbs free energy (G^*) is obtained from a second-degree Taylor series expansion in terms of compositional and order parameters (Thompson, 1969; Sack, 1982; Nell and Wood, 1989):

$$G^{\star} = g_{0} + g_{r_{1}}r_{1} + g_{r_{2}}r_{2} + g_{r_{3}}r_{3} + g_{s_{1}}s_{1} + g_{s_{2}}s_{2} + g_{s_{3}}s_{3} + g_{r_{1}r_{1}}r_{1}^{2} + g_{r_{2}r_{2}}r_{2}^{2} + g_{r_{3}r_{3}}r_{3}^{2} + g_{s_{1}s_{1}}s_{1}^{2} + g_{s_{2}s_{2}}s_{2}^{2} + g_{s_{3}s_{3}}s_{3}^{2} + g_{r_{1}r_{2}}r_{1}r_{2} + g_{r_{1}r_{3}}r_{1}r_{3} + g_{r_{1}s_{1}}r_{1}s_{1} + g_{r_{1}s_{2}}r_{1}s_{2} + g_{r_{1}s_{3}}r_{1}s_{3} + g_{r_{2}r_{3}}r_{2}r_{3} + g_{r_{2}s_{1}}r_{2}s_{1} + g_{r_{2}s_{2}}r_{2}s_{2} + g_{r_{2}s_{3}}r_{2}s_{3} + g_{r_{3}s_{1}}r_{3}s_{1} + g_{r_{3}s_{2}}r_{3}s_{2} + g_{r_{3}s_{3}}r_{3}s_{3} + g_{s_{1}s_{2}}s_{1}s_{2} + g_{s_{1}s_{3}}s_{1}s_{3} + g_{s_{2}s_{3}}s_{2}s_{3}$$
(10)

where the g_n terms are series expansion coefficients. The Gibbs free energy (G) of a solid solution is then obtained from Equations 9 and 10 through the relation

$$G = G^* - TS_{\text{conf}}.$$
 (11)

TABLE 5. Cation fractions per structural formula unit*

Nonideal mixing in the second-degree expansion can be identified with symmetric binary interaction parameters and reciprocal reaction terms (Thompson, 1969; Nell and Wood, 1989). In our previous paper, we derived a solution set for the 21 series expansion coefficients that do not involve the r_3 parameter. By considering the 17 possible binary solid solutions involving reference components $FeCr_2O_4$ and $MgCr_2O_4$ (Table 4), the coefficients involving the r_1 parameter were likewise determined. The complete set for the series expansion coefficients expressed in terms of on-site regular symmetric interaction parameters and reciprocal reaction energies is given in Appendix 1. The subscripts to the reciprocal reaction terms refer to the reference end-member components defined in Table 4, whereas the formulation of the reciprocal reaction terms and the interaction parameters were discussed in detail in our previous paper (Nell and Wood, 1989).

Equilibrium conditions

Equilibrium in $(Mg^{2+}, Fe^{2+})(Fe^{3+}, Al^{3+}Cr^{3+})_2O_4$ solid solutions is achieved when, at fixed temperature, pressure and composition, the following conditions are satisfied:

$$\begin{pmatrix} \frac{\partial G}{\partial s_1} \end{pmatrix}_{T,P,r_1,r_2,r_3,s_2,s_3} = \begin{pmatrix} \frac{\partial G}{\partial s_2} \end{pmatrix}_{T,P,r_1,r_2,r_3,s_1,s_3}$$
$$= \begin{pmatrix} \frac{\partial G}{\partial s_3} \end{pmatrix}_{T,P,r_1,r_2,r_3,s_1,s_3} = 0.$$
(12)

Substituting Equations 9 and 10 into 11 and differenti-

lon	Tetrahedral site	Octahedral site	Sum
Mg	$1 - r_1 - s_3$	S 3	$1 - r_1$
AI	$r_2 - s_1$	$r_2 + s_1$	$2r_2$
Fe ²⁺	$r_1 + r_3 + s_1 + s_2 + s_3 - 1$	$1 - r_3 - s_1 - s_2 - s_3$	<i>r</i> ₁
Fe ³⁺	$1 - s_2 - r_2 - r_3$	$1 + s_2 - r_2 - r_3$	$2 - 2r_2 - 2r_3$
Cr	0	2r ₃	2r ₃
Sum	1	2	3

* Given as a function of compositional parameters (r_1 , r_2 , and r_3) and order parameters (s_1 , s_2 , and s_3).

ating gives the equilibrium conditions in terms of expansion coefficients and cation site fractions:

$$\begin{pmatrix} \frac{\partial G}{\partial s_1} \end{pmatrix}_{T,P,r_1,r_2,r_3,s_2,s_3} = g_{s_1} + 2g_{s_1s_1}s_1 + g_{r_1s_1}r_1 + g_{r_2s_1}r_2 + g_{r_3s_1}r_3 + g_{s_1s_2}s_2 + g_{s_1s_3}s_3 + RT \ln \frac{(^{(4)}Fe^{2+})(^{(6)}A|^{3+})}{(^{(6)}Fe^{2+})(^{(4)}A|^{3+})} = 0 (13) $\left(\frac{\partial G}{\partial s_2} \right)_{T,P,r_1,r_2,r_3,s_1,s_3} = g_{s_2} + 2g_{s_2s_2}s_2 + g_{r_1s_2}r_1 + g_{r_2s_2}r_2 + g_{r_3s_2}r_3 + g_{s_1s_2}s_1 + g_{s_2s_3}s_3 + RT \ln \frac{(^{(4)}Fe^{2+})(^{(6)}Fe^{3+})}{(^{(6)}Fe^{2+})(^{(4)}Fe^{3+})} = 0$ (14)$$

and

$$\begin{pmatrix} \frac{\partial G}{\partial s_3} \end{pmatrix}_{T,P,r_1,r_2,r_3,s_1,s_2} = g_{s_3} + 2g_{s_3s_3}s_3 + g_{r_1s_3}r_1 + g_{r_2s_3}r_2 + g_{r_3s_3}r_3 + g_{s_1s_3}s_1 + g_{s_2s_3}s_2 + RT \ln \frac{({}^{(4)}\mathrm{Fe}^{2+})({}^{(6)}\mathrm{Mg}^{2+})}{({}^{(6)}\mathrm{Fe}^{2+})({}^{(4)}\mathrm{Mg}^{2+})} = 0.$$
 (15)

Equations 13–15 were used to calculate intersite cation distributions in $(Mg^{2+},Fe^{2+})(Fe^{3+},Al^{3+}Cr^{3+})_2O_4$ spinels after the following substitutions for the compositional parameters r_1 to r_3 were made:

$$r_1 = X_{\text{Fe3O4}} + X_{\text{FeAl}_2\text{O4}} + X_{\text{FeCr}_2\text{O4}}$$
$$r_2 = X_{\text{FeAl}_2\text{O4}} + X_{\text{MgAl}_2\text{O4}}$$

and

$$r_3 = X_{\text{FeCr}_2\text{O}_4} + X_{\text{MgCr}_2\text{O}_4}.$$
 (16)

All but the $g_{r_3s_1}$, $g_{r_3s_2}$, and $g_{r_3s_3}$ parameters in Equations 13–15 were derived in our previous study (Nell and Wood, 1989). The new coefficients ($g_{r_3s_1}$, $g_{r_3s_2}$, and $g_{r_3s_3}$) describe the effects of Cr³⁺ substitution on intersite partitioning involving Fe²⁺-Al³⁺, Fe²⁺-Fe³⁺, and Fe²⁺-Mg²⁺, respectively. It follows therefore that, unless all these parameters are equal to zero, the substitution of Cr³⁺ must affect cation distributions despite the fact that it does not, itself, disorder.

Activity-composition relations

There are six compositional series expansion coefficients available to model activity-composition relations along the 15 binary solid solutions in the trigonal prism Fe_3O_4 - $FeAl_2O_4$ - $MgFe_2O_4$ - $MgAl_2O_4$ - $FeCr_2O_4$ - $MgCr_2O_4$. The values of three of these coefficients were determined from our work in the quaternary (Mg^{2+} , Fe^{2+})(Fe^{3+} , Al^{3+})₂ O_4 (Nell and Wood, 1989). Three additional coef-

ficients $(g_{r_{3'3}}, g_{r_{1'3}}, \text{and } g_{r_{2'3}})$ are required to describe activity-composition relations along the eight binary Cr-bearing solid solutions where the r_3 compositional exchange vector is operative.

Substituting Equations 9 and 10 into Equation 11 and differentiating with respect to r_1 , r_2 , and r_3 gives

$$\begin{pmatrix} \frac{\partial G}{\partial r_1} \end{pmatrix}_{T,P,r_2,r_3,s_1,s_2,s_3} = g_{r_1} + 2g_{r_1r_1}r_1 + g_{r_1r_2}r_2 + g_{r_1r_3}r_3 + g_{r_1s_1}s_1 + g_{r_1s_2}s_2 + g_{r_1s_3}s_3 + RT \ln \frac{(^{(4)}\text{Fe}^{2+})}{(^{(4)}\text{Mg}^{2+})}$$
(17)
$$\begin{pmatrix} \frac{\partial G}{\partial r_2} \end{pmatrix}_{T,P,r_1,r_3,s_1,s_2,s_3} = g_{r_1} + 2g_{r_2r_3}r_2 + g_{r_1r_2}r_1 + g_{r_2r_3}r_3 + g_{r_2r_3}s_1$$

+
$$g_{r_{2}s_{2}}s_{2}$$
 + $g_{r_{2}s_{3}}s_{3}$ + RT ln $\frac{({}^{(4)}A{}^{(3+)})({}^{(6)}A{}^{(3+)})}{({}^{(4)}Fe^{3+})({}^{(6)}Fe^{3+})}$ (18)

and

$$\frac{\partial G}{\partial r_{3}}\Big|_{r,P,r_{1},r_{2},s_{1},s_{2},s_{3}} = g_{r_{3}} + 2g_{r_{3}r_{3}}r_{3} + g_{r_{1}r_{3}}r_{1} + g_{r_{2}r_{3}}r_{2} + g_{r_{3}s_{1}}s_{1}
+ g_{r_{3}s_{2}}s_{2} + g_{r_{3}s_{3}}s_{3}
+ RT \ln \frac{(^{[4]}Fe^{2+})(^{[6]}Cr^{3+})^{2}}{(^{[4]}Fe^{3+})(^{[6]}Fe^{2+})}.$$
(19)

Chemical potentials of fictive reference components are obtained by partial differentiation of the free energy with respect to each of the order and compositional parameters:

$$\mu_{a,b,c,d,e,f} = G + (a - r_1) \left(\frac{\partial G}{\partial r_1} \right)_{T,P,r_2,r_3,s_1,s_2,s_3} + (b - r_2) \left(\frac{\partial G}{\partial r_2} \right)_{T,P,r_1,r_3,s_1,s_2,s_3} + (c - r_3) \left(\frac{\partial G}{\partial r_3} \right)_{T,P,r_1,r_2,s_1,s_2,s_3} + (d - s_1) \left(\frac{\partial G}{\partial s_1} \right)_{T,P,r_1,r_2,r_3,s_2,s_3} + (e - s_2) \left(\frac{\partial G}{\partial s_2} \right)_{T,P,r_1,r_2,r_3,s_1,s_3} + (f - s_3) \left(\frac{\partial G}{\partial s_3} \right)_{T,P,r_1,r_2,r_3,s_1,s_2}$$
(20)

where the coefficients a-f are coordinates of a phase in $r_1-r_2-r_3-s_1-s_2-s_3$ space. Chemical potentials of the reference end-member components obtained from Equation 20 are presented in Table 6. Reference components 1–8 are, of



Fig. 11. (A) Cation distributions on the join $FeAl_2O_4$ -Fe-Cr₂O₄ at 1100 °C obtained from a Gibbs-Duhem integration of the partial molar magnetite entropies in Fe₃O₄-FeAl₂O₄-FeCr₂O₄ solid solutions. Results are plotted as a function of mole fraction $FeCr_2O_4$ (X_{chr}). Solid lines are model calculations. (B) Activitycomposition relations in FeAl₂O₄-FeCr₂O₄ solid solutions at 1100 °C. Data are from Petric and Jacob (1982b) and solid lines are calculated from the model.

course, fictive and do not refer to the actual standard states of MgAl₂O₄, Fe₃O₄, FeAl₂O₄, and MgFe₂O₄ at the conditions of interest. Chemical potentials relative to real MgAl₂O₄, Fe₃O₄, FeAl₂O₄, and MgFe₂O₄ standard states at the conditions of interest are obtained through the substitution in Equation 20 of the values of the order and composition parameters a-f, which correspond to those end-members. The activities of MgAl₂O₄, Fe₃O₄, Fe

 Al_2O_4 , and MgFe₂O₄ relative to disordered pure endmember standard states at the temperature and pressure of interest as well as the activities of FeCr₂O₄ and Mg-Cr₂O₄ relative to normal standard state end-members are in Table 7.

CONSTRAINT OF MODEL PARAMETERS

Values of the coefficients involving the r_3 parameter were derived as an extension of the parameters obtained in our earlier work (Nell and Wood, 1989). The $g_{r_{331}}$ and $g_{r_{332}}$ parameters were constrained from our cation distribution data for Fe₃O₄-FeAl₂O₄-FeCr₂O₄ and Fe₃O₄-Fe-Cr₂O₄ solid solutions, respectively. Data for Fe₃O₄-MgCr₂O₄ solid solutions suggest that the $g_{r_{333}}$ parameter is effectively equal to zero, indicating that the substitution of Cr³⁺ does not affect the partitioning of Fe²⁺ and Mg²⁺ between octahedral and tetrahedral sites (Eq. 15).

The g_{rav} parameter was constrained from activity-composition relations in Fe₃O₄-FeCr₂O₄ solid solutions at 1227 °C (Katsura et al., 1975) and 1400 °C (Petric and Jacob, 1982a). The g_{rora} coefficient was determined from Al³⁺-Cr3+ partitioning experiments between clinopyroxene and MgAl₂O₄-MgCr₂O₄ solid solutions at 1100 °C (Webb and Wood, 1986), whereas $g_{\mu\nu}$ was estimated from experiments on the partitioning of Fe²⁺-Mg²⁺ between olivine and MgAl₂O₄-FeAl₂O₄-FeCr₂O₄-MgCr₂O₄ solid solutions at 800 °C and 900 °C (Engi, 1983). The fitted values of the $g_{r_3r_3}, g_{r_3s_1}, g_{r_3s_2}, g_{r_3s_3}, g_{r_3r_3}, g_{r_1r_3}$, and $g_{r_2r_3}$ parameters were finally tested and refined by comparing observed and calculated cation distributions, activity-composition relations, and interphase partitioning coefficients in Fe₃O₄- $FeCr_2O_4$, Fe_3O_4 -MgCr_2O_4, Fe_3O_4 -FeAl₂O₄-FeCr₂O₄, MgAl₂O₄-MgCr₂O₄, and FeAl₂O₄-FeCr₂O₄ solid solutions. The standard state chemical potentials of the reference end-member components were set to zero and the values of the g_0 , g_{r_1} , g_{r_2} , and g_{r_3} coefficients were subsequently constrained to be consistent with the values of the higher order expansion coefficients. These values are reported in Table 8 together with the values of the coefficients obtained in our earlier study (Nell and Wood, 1989). The estimated uncertainties in Table 8 reflect ranges over which the values may be varied while preserving a reasonable fit to the data. The coefficients are highly correlated (Nell and Wood, 1989) and the uncertainties are not intended to represent those correlations.

Application of the model to $FeCr_2O_4$ - and $MgCr_2O_4$ -bearing solid solutions

Cation distributions and activity-composition relations in Fe_3O_4 - $FeCr_2O_4$, Fe_3O_4 - $MgCr_2O_4$, Fe_3O_4 - $FeAl_2O_4$ - $Fe-Cr_2O_4$, and $MgAl_2O_4$ - $MgCr_2O_4$ solid solutions were calculated from the values of the expansion coefficients in Table 8. Equations 13–15 were used to calculate cation distributions for a given temperature. A Newton-Raphson method (e.g., Gerald and Wheatley, 1984, p. 133– 159) was used to solve the nonlinear equations resulting in the solid lines in Figures 8A, 9, 10, and 11A. In all four systems, the data were used to constrain model pa-

TABLE 6. Chemical potentials of reference end-member components

μ _{Al(MgAl)O4} =	$f_{1} + g_{i_{2}} + g_{s_{3}} - g_{i_{1}i_{1}}r_{1}^{2} - g_{i_{2}i_{2}}r_{2}^{2} - g_{s_{3}s_{3}}s_{1}^{2} - g_{s_{3}s_{3}}s_{2}^{2} - g_{s_{3}s_{3}}s_{3}^{2}$	
	$\begin{array}{l}g_{r_1s_1}r_1s_1-g_{r_1s_2}r_1s_2-g_{s_1s_2}s_1s_2+(2g_{r_2r_2}+g_{r_2s_3})r_2+(g_{r_1r_2}+g_{r_1s_3})r_3\\(g_{r_2s_1}+g_{s_1s_3}s_1+(g_{r_2s_2}+g_{s_2s_3})s_2+(2g_{s_3s_3}+g_{r_2s_3})s_3-g_{r_1r_2}r_1r_2\end{array}$	1
	$\begin{array}{l}g_{\prime_2 s_1} r_2 s_1 - g_{\prime_2 s_2} r_2 s_2 - g_{\prime_1 s_3} r_1 s_3 - g_{\prime_2 s_3} r_2 s_3 - g_{s_1 s_3} s_1 s_3 - g_{s_2 s_3} s_2 s_3 \\g_{\prime_3 \prime_3} r_3^2 - g_{\prime_1 \prime_3} r_1 r_3 + (g_{\prime_2 \prime_3} + g_{\prime_3 s_3}) r_3 - g_{\prime_2 \prime_3} r_2 r_3\end{array}$	
	$g_{rss}r_3s_1 - g_{rss}r_3s_2 - g_{rss}r_3s_3$	
μ _{Mg(AlABO,} =	$ \begin{array}{l} \bar{R} T_1^{}[\ln(^{i4} A)(^{i6} \tilde{A})(^{i6} Mg) - 2 \ln 2] \\ + g_{r_2} + g_{s_1} - g_{r_1r_1}r_1^2 - g_{s_2r_2}r_2^2 - g_{s_1s_1}s_1^2 - g_{s_2s_2}s_2^2 - g_{s_3s_2}s_3^2 \end{array} $	
	$g_{r_1s_2}r_1s_2 - g_{r_1s_2}r_1s_3 - g_{s_2s_3}s_2s_3 + (2g_{r_2r_2} + g_{r_2s_1})r_2 + (g_{r_1r_2} + g_{r_1s_1})r_3$	1
	$\begin{array}{l}(g_{r_2s_1}+2g_{s_1s_1})s_1+(g_{r_2s_2}+g_{s_1s_2})s_2+(g_{s_1s_3}+g_{r_2s_3})s_3-g_{r_1r_2'}r_{1r_2}\\g_{r_2s_1}r_2s_1-g_{r_2s_2}r_2s_2-g_{r_1s_1}r_{1}s_1-g_{r_2s_2}r_2s_3-g_{s_1s_2}s_1s_3-g_{s_1s_2}s_1s_2\end{array}$	
	$g_{r_3r_3}r_3^2 - g_{r_1r_3}r_1r_3 - g_{r_2r_3}r_2r_3 + (g_{r_2r_3} + g_{r_3s_1})r_3$	
	$\begin{array}{l} g_{r_3 s_1} r_3 s_1 - g_{r_3 s_2} r_3 s_2 - g_{r_3 s_2} r_3 s_3 \\ R7[2 \ln^{(6)}Al) + \ln^{(4)}Mg) - 2 \ln 2] \end{array}$	
μ _{Fe³⁺(Fe²⁺Fe³⁺)O₄}	$g_{1} + g_{r_{1}} - g_{r_{1}r_{1}}r_{1}^{2} - g_{r_{2}r_{2}}r_{2}^{2} - g_{s_{1}s_{3}}s_{1}^{2} - g_{s_{2}s_{3}}s_{2}^{2} - g_{s_{3}s_{3}}s_{3}^{2} - g_{s_{3}s_{3}}s_{3}^{2} - g_{s_{1}s_{3}}r_{1} + g_{r_{1}s_{2}}s_{2} + g_{r_{1}s_{3}}s_{3} - g_{r_{1}s_{2}}r_{1}r_{2} - g_{r_{1}s_{1}}r_{1}s_{1}$	
	$g_{r_2s_1}r_2s_1 - g_{r_1s_2}r_1s_2 - g_{r_2s_2}r_2s_2 - g_{s_1s_2}s_1s_2 - g_{s_2s_3}s_2s_3$	
	$\begin{array}{l}g_{r_1s_1}r_1s_3 - g_{r_2s_3}r_2s_3 - g_{s_1s_2}s_1s_3 - g_{s_3r_1}r_3^2 + g_{r_1r_3}r_3(1-r_1)\\g_{r_2r_3}r_2r_3 - g_{r_3s_1}r_3s_1 - g_{r_3s_2}r_3s_2 - g_{r_3s_3}r_3s_3\end{array}$	
HE-24/E-24/E-24/0	$\begin{array}{l} RT[In({}^{(e)}Fe^{3+})({}^{(e)}Fe^{2+}) - 2In2]\\ {}_{0}+g_{r_{1}}+g_{s_{2}}-g_{r_{1}r_{1}}r_{1}^{2}-g_{r_{2}r_{2}}r_{2}^{2}-g_{s_{3}s_{3}}s_{1}^{2}-g_{s_{3}s_{3}}s_{2}^{2}-g_{s_{3}s_{3}}s_{3}^{2}\end{array}$	
L.Lev. (Lev. Lev.)04	$(2g_{r_1r_1} + g_{r_1s_2})r_1 + (g_{r_1r_2} + g_{r_2s_2})r_2 + (g_{r_1s_1} + g_{s_1s_2})s_1 + (g_{r_1s_2} + 2g_{r_1s_2})s_1$	s2s2)S2
	$\begin{array}{l} (g_{r_1s_3}+g_{s_2s_3})s_3-g_{r_1r_2}r_1r_2-g_{r_1s_1}r_1s_1-g_{r_2s_1}r_2s_1-g_{r_1s_2}r_1s_2-g_{r_2s_2}\\ g_{s_1s_2}s_1s_2-g_{s_2s_3}s_2s_3-g_{r_1s_2}r_1s_3-g_{r_2s_2}r_2s_3-g_{s_1s_3}s_1s_3-g_{r_3r_3}r_3^2\end{array}$	r ₂ s ₂
	$\begin{array}{l} (g_{r_{1}r_{3}}+g_{r_{3}s_{2}})r_{3}-g_{r_{1}r_{3}}r_{1}r_{3}^{-}-g_{r_{3}}r_{2}r_{3}^{-}-g_{r_{3}s_{1}}r_{3}s_{1}-g_{r_{3}s_{4}}r_{3}s_{2}-g_{r_{3}s_{1}}r_{3}s_{1}-g_{r_{3}s_{4}}r_{3}s_{2}-g_{r_{3}s_{4}}r_{3}s_{2}^{-}-g_{r_{3}s_{4}}r_{3}s_{4}^{-}-g_{r_{3}s_{4}}r_{3}s_{2}^{-}-g_{r_{3}s_{4}}r_{3}s_{2}^{-}-g_{r_{3}s_{4}}r_{3}s_{2}^{-}-g_{r_{3}s_{4}}r_{3}s_{3}^{-}-g_{r_{3}s_{4}}r_{3}s_{4}^{-}-g_{r_{3}s_{4}}r_{3}s_{$	3 S 3
HAKFe2+AI)O4	$g_{1} + g_{r_{1}} + g_{r_{2}} - g_{r_{1}r_{1}}r_{1}^{2} - g_{r_{2}r_{2}}r_{2}^{2} - g_{s_{1}s_{1}}s_{1}^{2} - g_{s_{2}s_{2}}s_{2}^{2} - g_{s_{3}s_{3}}s_{3}^{2}$	
	$\begin{array}{l} (2g_{r_1r_1}+g_{r_1r_2})r_1+(2g_{r_2r_2}+g_{r_1r_2})r_2+(g_{r_1s_1}+g_{r_2s_1})s_1+(g_{r_1s_2}+g_{r_1})s_1+(g_{r_1s_2}+g_{r_2})s_3+(g_{r_1s_2}+g_{r_1})s_1+(g_{r_1s_2}+g_{r_2})s_1+(g_{r_1s_2}+g_{r_2})s_1+(g_{r_1s_2}+g_{r_2})s_1+(g_{r_1s_2}+g_{r_2})s_1+(g_{r_1s_2}+g_{r_2})s_1+(g_{r_1s_2}+g_{r_2})s_1+(g_{r_1s_2}+g_{r_2})s_1+(g_{r_1s_2}+g_{r_2})s_1+(g_{r_1s_2}+g_{r_2})s_1+(g_{r_1s_2}+g_{r_2})s_1+(g_{r_2s_2}+g_{r_2s_2}+g_{r_2s_2}+g_{r_2})s_1+(g_{r_2s_2}+g_{r_2s_2}+g_{r_2s_2}+g_{r_2s_2})s_1+(g_{r_2s_2}+g_$, _{s2})S2
	$g_{r_2s_1}r_2s_1 - g_{s_2s_2}r_2s_2 - g_{r_3s_3}r_2s_3 - g_{s_1s_2}s_1s_2 - g_{s_1s_3}s_1s_3 - g_{s_2s_3}s_2s_3$	
	$\begin{array}{l}g_{i_{2}i_{3}}r_{3}^{2}+(g_{i_{1}i_{3}}+g_{i_{2}i_{3}})r_{3}-g_{i_{1}i_{3}}r_{1}r_{3}-g_{i_{2}i_{3}}r_{2}r_{3}\\g_{i_{3}s_{1}}r_{3}s_{1}-g_{i_{3}s_{2}}r_{3}s_{2}-g_{i_{3}s_{1}}r_{3}s_{3}\end{array}$	
HE-2+(AIADO	$\begin{array}{l} R\mathcal{T}[In({}^{(6)}Fe^{2+})({}^{(6)}A)({}^{(4)}A))-2In2]\\ {}_{0}+g_{r_{1}}+g_{r_{2}}+g_{s_{1}}-g_{r_{1}r_{1}}r_{1}^{2}-g_{r_{2}r_{2}}r_{2}^{2}-g_{s_{1}s_{1}}s_{1}^{2}-g_{s_{2}s_{2}}s_{2}^{2}-g_{s_{3}s_{4}}s_{3}^{2}\end{array}$	2
(Add)-4	$(2g_{r_1r_1} + g_{r_1r_2} + g_{r_1s_1})r_1 + (2g_{r_2r_2} + g_{r_1r_2} + g_{r_2s_1})r_2$,
	$\begin{array}{l} (2g_{\mathfrak{s},\mathfrak{s}_1}+g_{\mathfrak{r},\mathfrak{s}_1}+g_{\mathfrak{r}_2\mathfrak{s}_1})\mathfrak{s}_1+(g_{\mathfrak{r},\mathfrak{s}_2}+g_{\mathfrak{r}_2\mathfrak{s}_2}+g_{\mathfrak{s},\mathfrak{s}_2})\mathfrak{s}_2\\ (g_{\mathfrak{r},\mathfrak{s}_2}+g_{\mathfrak{r}_2\mathfrak{s}_2}+g_{\mathfrak{s},\mathfrak{s}_2})\mathfrak{s}_3-g_{\mathfrak{r},\mathfrak{r}_2}\mathfrak{r}_1\mathfrak{r}_2-g_{\mathfrak{r},\mathfrak{s}_1}\mathfrak{r}_1\mathfrak{s}_1-g_{\mathfrak{r},\mathfrak{s}_2}\mathfrak{r}_1\mathfrak{s}_2-g_{\mathfrak{r},\mathfrak{s}_1}\mathfrak{r}_1\mathfrak{s}_3\end{array}$	1
	$\begin{array}{l}g_{r_{2}s_{1}}r_{2}s_{1}-g_{r_{2}s_{2}}r_{2}s_{2}-g_{r_{2}s_{3}}r_{2}s_{3}-g_{s_{1}s_{2}}s_{1}s_{2}-g_{s_{1}s_{3}}s_{1}s_{3}-g_{s_{2}s_{3}}s_{2}s_{3}\\g_{r_{3}r_{3}}r_{3}^{2}+(g_{r_{1}r_{3}}+g_{r_{2}r_{3}}+g_{r_{3}s_{3}})r_{3}-g_{r_{1}r_{3}}r_{1}r_{3}-g_{r_{2}r_{3}}r_{2}r_{3}\end{array}$	
	$g_{r_1s_1}r_3s_1 - g_{r_1s_2}r_3s_2 - g_{r_1s_2}r_3s_3$	
μ _{Fe³⁺(Fe³⁺Mq)O₄}	$ \begin{array}{l} \bar{R}\bar{T}[2\ln(^{(\mathrm{s})}\bar{A})] &+ \ln(^{(\mathrm{s})}\bar{Fe}^{2+}) - 2\ln2] \\ _{2} + g_{s_{0}} - g_{r_{1}r_{1}}r_{1}^{2} - g_{s_{2}r_{2}}r_{2}^{2} - g_{s_{1}s_{1}}s_{1}^{2} - g_{s_{2}s_{2}}s_{2}^{2} - g_{s_{3}s_{3}}s_{3}^{2} \end{array} $	
	$g_{r_1s_3}r_1 + g_{r_2s_3}r_2 + g_{s_1s_3}s_1 + g_{s_2s_3}s_2 + 2g_{s_3s_3}s_3$	
	$\begin{array}{l}g_{r_1r_2}r_1r_2-g_{r_1s_1}r_1s_1-g_{r_1s_2}r_1s_2-g_{r_1s_3}r_1s_3-g_{r_2s_1}r_2s_1\\g_{r_2s_2}r_2s_2-g_{r_2s_3}r_2s_3-g_{s_1s_2}s_1s_2-g_{s_1s_3}s_1s_3-g_{s_2s_3}s_2s_3\end{array}$	
	$\begin{array}{l}g_{r_{0}s_{1}}r_{3}^{2}-g_{r_{1}s_{1}}r_{1}s-g_{r_{2}s_{3}}r_{2}r_{3}-g_{r_{3}s_{1}}r_{3}s_{1}\\g_{r_{5}s_{2}}r_{3}s_{2}-g_{r_{5}s_{1}}r_{3}(s_{3}-1)\end{array}$	
	$RT[ln({}^{[4]}Fe^{3+})({}^{[6]}Fe^{3+})({}^{[6]}Mg) - 2 ln 2]$	
MMg(Fe ³⁺ Fe ³⁺)O ₄	$g_{r_1s_2} - g_{s_1s_1}r_1^2 - g_{r_2r_2}r_2^2 - g_{s_1s_1}s_1^2 - g_{s_2s_2}s_2^2 - g_{s_3s_5}s_3^2 - g_{s_3s_5}s_3^2 - g_{s_3s_5}s_3^2$ $g_{r_1s_2}r_1 + g_{r_2s_2}r_2 + g_{s_1s_2}s_1 + 2g_{s_2s_2}s_2 + g_{s_2s_3}s_3$	
	$\begin{array}{l}g_{r_1r_2}r_1r_2-g_{r_1s_1}r_1s_1-g_{r_1s_2}r_1s_2-g_{r_1s_3}r_1s_3-g_{r_2s_1}r_2s_1\\g_{r_2s_2}r_2s_2-g_{r_2s_3}r_2s_3-g_{s_1s_2}s_1s_2-g_{s_1s_3}s_1s_3-g_{s_2s_1}s_2s_3\end{array}$	
	$g_{r_0r_0}r_3^2 - g_{r_0r_0}r_1r_3 - g_{r_0r_0}r_2r_3 - g_{r_0s_0}r_3s_1$	
	$g_{r_3s_1}r_3(s_2-1) - g_{r_3s_1}r_3s_3$ R T[2 ln(^(t) Fe ³⁺) + ln(⁽⁴⁾ Mg) - 2 ln 2]	
µ _{FeCr2O4}	$g_{1} + g_{r_{1}} + g_{r_{3}} - g_{r_{1}r_{1}}r_{1}^{2} - g_{r_{2}r_{2}}r_{2}^{2} - g_{r_{3}r_{3}}r_{3}^{2} - g_{s,s_{5}}s_{1}^{2} - g_{s_{2}s_{2}}s_{2}^{2}$ $g_{s_{3}s_{5}}s_{3}^{2} + (2g_{r_{1}r_{1}} + g_{r_{1}r_{3}})r_{1} + (g_{r_{1}r_{2}} + g_{r_{3}r_{3}})r_{2} + (2g_{r_{3}r_{3}} + g_{r_{1}r_{3}})r_{3}$	
	$(g_{r_1s_1} + g_{r_3s_1})s_1 + (g_{r_1s_2} + g_{r_3s_2})s_2 + (g_{r_1s_3} + g_{r_3s_3})s_3 - g_{r_1r_2}r_1r_2$	
	$\begin{array}{l}g_{r_1r_2}r_1r_3-g_{r_1s_4}r_1s_1-g_{r_1s_2}r_1s_2-g_{r_1s_5}r_1s_3-g_{r_2s_4}r_2r_3\\g_{r_2s_4}r_2s_1-g_{r_2s_2}r_2s_2-g_{r_2s_5}r_2s_3-g_{r_3s_4}r_3s_1-g_{r_3s_2}r_3s_2\end{array}$	
	$\begin{array}{l} g_{i_{1}s_{1}}r_{3}s_{3}-g_{s_{1}s_{2}}s_{1}s_{2}-g_{s_{1}s_{2}}s_{1}s_{3}-g_{s_{2}s_{3}}s_{2}s_{3}\\ R\Pi[2\ln({}^{(6)}\text{Cr})+\ln({}^{(4)}\text{Fe}^{2+})-2\ln2] \end{array}$	
HMgCr204	$g_1 + g_{r_3} - g_{r_1r_1}r_1^2 - g_{r_2r_2}r_2^2 - g_{r_3r_3}r_3^2 - g_{s_1s_1}s_1^2 - g_{s_2s_2}s_2^2$	
	$\begin{array}{l}g_{s_{3}s_{3}}s_{3}^{2}+2g_{s_{3}s_{1}}-g_{r_{1}s_{2}}r_{1}r_{2}+g_{r_{1}s_{1}}r_{1}(1-r_{3})-g_{r_{3}s_{1}}r_{1}s_{1}\\g_{r_{1}s_{2}}r_{1}s_{2}-g_{r_{1}s_{2}}r_{1}s_{3}+g_{r_{2}s_{2}}r_{2}(1-r_{3})-g_{r_{2}s_{1}}r_{2}s_{1}-g_{r_{2}s_{2}}r_{2}s_{2}\end{array}$	
	$g_{r_2s_3}r_2s_3 + g_{r_3s_3}s_{1}(1-r_3) + g_{r_3s_2}s_{2}(1-r_3) + g_{r_3s_3}s_{3}(1-r_3)$	
	$\begin{array}{l}g_{s_1s_2}s_1s_2-g_{s_1s_3}s_1s_3-g_{s_1s_3}s_2s_3\\ RT[2In^{(0)}Cr)+In^{(4)}Mg)-2In2]\end{array}$	

rameters, and the calculated lines are thus fitted. Fe_3O_4 , $FeAl_2O_4$, $MgFe_2O_4$, $MgAl_2O_4$, $FeCr_2O_4$, and $MgCr_2O_4$ activities were calculated from the equations in Tables 6 and 7 and are presented as solid lines in activity-com-

position diagrams (Figs. 8B and 11B) and interphase partition plots (Figs. 12, 13A, and 13B). The data in Figures 8B and 13A were used to derive values of the model coefficients and the calculated lines in these figures are

 TABLE 7.
 Activities of spinel, magnetite, hercynite, magnesioferrite, chromite and picrochromite relative end-member standard states at the temperature and pressures of interest

$$\begin{aligned} & \mathsf{RT}\ln a_{\mathsf{dep}(q_{1})} = g_{\mathsf{e}}(2, \overline{q}) = g_{\mathsf{e}}(2, \overline$$

Note: The superscripts ss, sp, mt, hc, and mf refer, respectively, to solid solutions, pure spinel, pure magnetite, pure hercynite, and pure magnesioferrite, wherease the superscript 0 on the order parameters s_1 , s_2 , and s_3 indicates values in pure disordered end-member spinels.



Fig. 12. Predicted values of $\ln K_d^{el-Crsp} [K_d = (X_{FeG_{2}O_4}^{en}) \cdot (X_{M_gSi_0,5O_2}^{el})/(X_{FeG_{2}O_4}^{el}) \cdot (X_{el}^{el})$ compared to the data of Engi (1983) at 700 °C, and 900 °C. Calculations were performed at 700 °C and take account of the nonideality (W_{ol} on a 1 atom basis) in olivine. Directions of approach to equilibrium in the experimental measurements are indicated by arrows on the error bars.

TABLE 8.	Internally consistent	values	of the	Taylor	series	ex-
	pansion coefficients					

Coefficient	Value (kJ/mol)
g _o	2.9 ± 5.5
g _r ,	7.1 ± 4.5
g_{r_2}	33.5 ± 19.8
g_{r_3}	35.5 ± 2.5
g_{s_1}	14.7 ± 0.5
g_{s_2}	44.5 ± 4.5
g _{s3}	34.0 ± 2.5
$g_{r_1r_1}$	-10.0 ± 1.0
$g_{r_{2}r_{2}}$	-38.0 ± 2.0
$g_{r_3r_3}$	-35.0 ± 2.0
g_{s,s_1}	-25.7 ± 1.5
$g_{s_2 s_2}$	-26.6 ± 1.3
$g_{s_3 s_3}$	-15.0 ± 3.0
$g_{r_1r_2}$	10.0 ± 3.0
9r113	-0.5 ± 0.2
$g_{r_{1}s_{1}}$	-7.1 ± 0.5
$g_{r_1s_2}$	-25.0 ± 3.5
$g_{r_1s_3}$	-15.0 ± 2.0
g _{r2r3}	-25.0 ± 2.0
$g_{r_{2}s_{1}}$	5.5 ± 3.0
g1282	-16.6 ± 4.0
$g_{r_2s_3}$	-11.9 ± 2.0
$g_{r_{3}s_{1}}$	-24.8 ± 1.5
$g_{r_3s_2}$	-38.0 ± 1.0
g _{r3s3}	0.0 ± 1.0
$g_{s_1s_2}$	-16.0 ± 12.0
$g_{s_1s_3}$	-15.0 ± 3.0
$g_{s_2 s_3}$	-24.6 ± 2.0



Fig. 13. (A) Calculated values of $\ln K_{\rm G}^{\rm opx-CrAlsp} [K_{\rm d} = (X_{\rm Mac}^{\rm crAlsp}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm Spa}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm Spa}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm Spa}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm Spa}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm Spa}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm Spa}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Mac}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Mac}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Mac}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Mac}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Mac}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Mac}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Mac}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm Na}) \cdot (X_{\rm Mac}^{\rm cr}_{\rm Na}) = (X_{\rm Mac}^{\rm cr}_{\rm$

therefore fitted. The solid lines in Figures 11B, 12, and 13B are predicted because the data shown were not used to constrain model parameters.

FeCr₂O₄-MgCr₂O₄-MgAl₂O₄-FeAl₂O₄ solid solutions

Engi (1983) performed experiments on the exchange of $Fe^{2+}-Mg^{2+}$ between olivine and $FeCr_2O_4-MgCr_2O_4$ solid solutions and between olivine and $(Fe^{2+},Mg^{2+})-(Al^{3+},Cr^{3+})_2O_4$ solid solutions with approximate compositions at the intersection of the $FeCr_2O_4-MgAl_2O_4$ and $MgCr_2O_4$ -FeAl₂O₄ tie lines at temperatures ranging between 650 °C and 900 °C and pressures between 300 and 1000 bars. There is no cation disordering in the system $FeCr_2O_4-MgCr_2O_4$ and the only adjustable parameter in

the modeling of activity-composition relations along this binary is the $g_{r_1r_1}$ coefficient which has been constrained by the mixing properties of Fe₃O₄-MgFe₂O₄ and Mg-Al₂O₄-FeAl₂O₄ solid solutions (Nell and Wood, 1989). Fe²⁺-Mg²⁺ partitioning between olivine (ol) and FeCr₂O₄-MgCr₂O₄ solid solution (Crsp) is given by

$$\ln K_{d}^{\text{ol-Crsp}} = \ln \frac{(X_{\text{FeGr}2O_4}^{\text{FeGr}2O_4})(X_{\text{MgSi}_0,5O_2}^{\text{ol}})}{(X_{\text{MgCr}_2O_4}^{\text{Crsp}})(X_{\text{FeSi}_0,5O_2}^{\text{ol}})}$$
$$= \ln K_{a}^{\text{ol-Crsp}} + \ln \left(\frac{\gamma_{\text{MgCr}_2O_4}}{\gamma_{\text{FeCr}_2O_4}}\right) - \frac{W_{\text{ol}}}{RT}$$
$$+ \frac{2W_{\text{ol}}}{RT} (X_{\text{MgSi}_0,5O_2}^{\text{ol}})$$
(21)

where $K_a^{\text{ol-Crsp}}$ is the equilibrium for the olivine-spinel exchange reaction, $X_{\text{Fedr}_{2}O_4}^{\text{Crsp}}$ is the mole fraction of chromite in the spinel solid solution, $\gamma_{\text{FeCr}_2O_4} = (a_{\text{FeCr}_2O_4}/$ $X_{\text{FeCr}_{2}O_{4}}^{\text{Crsp}}$ is the activity coefficient of chromite in the spinel solid solution, and W_{ol} is the regular solution interaction parameter for Fe-Mg olivine. Predicted $K_d^{ol-Crsp}$ values at fixed spinel composition were calculated from Equation 21 using $\gamma_{\text{FeCr}_2O_4}$ and $\gamma_{\text{MgCr}_2O_4}$ values from our activity-composition relations. The regular solution interaction parameter (W_{ol}) in olivine was assumed to be 4.5 ± 1.0 kJ/mol on a 1 atom basis (Nafziger and Muan, 1967; O'Neill and Wall, 1987) and the mean value for ln $K_a^{\text{ol-Crsp}}$ was calculated to be 3.0. Predicted ln $K_d^{\text{ol-Crsp}}$ values at 700 °C are in good agreement with experimental measurements at 700 °C and 800 °C (Fig. 12). Three data points at 900 °C are, however, inconsistent with the lower temperature results and would require a much smaller value of the $g_{r_1r_1}$ coefficient. The $g_{r_1r_1}$ coefficient is given by $-W_{[4]Fe^{2+}-[4]Mg^{2+}}$ (Appendix 1) and our value of -10.0 \pm 1.0 kJ/mol is in good agreement with a recent estimate of approximately 8.2 kJ/mol for $W_{\text{Fe}^{2+}-Mg^{2+}}^{\text{spinel}}$ (Sack and Ghiorso, 1989). The three anomalous data points at 900 °C are therefore, in the context of our model, inconsistent with a wide range of activity-composition, as well as partitioning data summarized in our earlier paper (Jamieson and Roeder, 1984; Lehmann and Roux, 1986; Shishkov et al., 1980; and Trinel-Dufour and Perrot, 1977 summarized in Nell and Wood, 1989).

Data points at the intersection of the FeCr₂O₄-MgAl₂O₄ and MgCr₂O₄-FeAl₂O₄ tie lines were used to constrain the value of the $g_{r_{1}r_{3}}$ parameter by formulating equilibria similar to Equation 21 for the FeCr₂O₄-MgCr₂O₄ and Mg-Al₂O₄-FeAl₂O₄ components in equilibrium with olivine. Our model calculates equal ratios for ln $\frac{\gamma_{MgAl_2O_4}}{\gamma_{FeAl_2O_4}}$ and ln $\frac{\gamma_{MgCr_2O_4}}{\gamma_{FeCr_2O_4}}$, but the data are poorly reversed and do not provide a stringent test for our model.

Fe₃O₄-FeCr₂O₄ solid solutions

Calculated cation distributions at 1400 °C (Fig. 8A) agree with our results obtained from thermopower measurements. Activity-composition relations calculated at

1227 °C are shown in Figure 8B together with the data of Katsura et al. (1975) and Petric and Jacob (1982a). Uncertainties in the latter data were estimated from the experimental method in which spinel solid solutions and Pt-Fe alloys were equilibrated at a fixed P_{o_2} . The uncertainty in the value of log $a_{\rm Fe}$ is approximately ± 0.06 log units (Nell and Wood, 1989) resulting in the error bars presented in Figure 8B.

Fe₃O₄-MgCr₂O₄ and Fe₃O₄-FeAl₂O₄-FeCr₂O₄ solid solutions

Cation distributions in Fe₃O₄-MgCr₂O₄ solid solutions calculated at 1000 °C are compared with measured values in Figure 9. Measured and calculated cation distributions in Fe_3O_4 -FeAl₂O₄-FeCr₂O₄ solid solutions along a pseudobinary section with the ratio of $Cr_2O_3/(Cr_2O_3 + Al_2O_3)$ = 1/2 at 1100 °C are in Figure 10. Data in this system were collected along three pseudobinary sections taken at constant ratios of FeAl₂O₄/(FeAl₂O₄ + FeCr₂O₄) = 1/6, 1/1, and 5/6, respectively. This was done to facilitate integration of a three-component Gibbs-Duhem equation (Darken, 1950) for the excess partial molar entropy of Fe_3O_4 in solution that in turn was used to calculate partial molar entropies and cation distributions in FeAl₂O₄-FeCr₂O₄ solid solutions (Fig. 11A). Uncertainties in the cation distributions obtained from the Gibbs-Duhem integration were estimated in our previous paper (Nell and Wood, 1989) and are indicated on Figure 11A. In situ high-temperature cation distributions in solid solutions that do not contain both Fe²⁺ and Fe³⁺ (e.g., FeCr₂O₄-FeAl₂O₄) are not amenable to direct measurement using the thermopower-conductivity technique, and this provides a feasible, if ponderous, way of obtaining high-temperature cation distributions in such systems.

Activity-composition relations modeled for FeCr₂O₄-FeAl₂O₄ solid solutions at 1100 °C are compared to the measurements of Petric and Jacob (1982b) in Figure 11B. Error bars on the data points correspond to an uncertainty of $\pm 10\%$ in the measured activities.

MgAl₂O₄-MgCr₂O₄ solid solutions

 Al^{3+} -Cr³⁺ partitioning experiments between spinel and clinopyroxene at 1100 °C and 25 kbar pressure (Webb and Wood, 1986) were used to constrain activity-composition relations in MgAl₂O₄-MgCr₂O₄ solid solutions. Assuming ideal mixing in clinopyroxene solid solutions, equilibrium between NaAlSi₂O₆-NaCrSi₂O₆ (cpx) and MgAl₂O₄-MgCr₂O₄ (CrAlsp) is given by

$$\ln K_{d}^{\text{cpx}-\text{CrAlsp}} = \ln \frac{(X_{\text{MgCr}2O_4}^{\text{CrAlsp}})(X_{\text{MacAISi}2O_6}^{\text{px}})}{(X_{\text{MgAI}2O_4}^{\text{CrAlsp}})(X_{\text{NaCrSi}_2O_6}^{\text{cpx}})}$$
$$= \ln K_{a}^{\text{cpx}-\text{CrAlsp}} + \frac{\ln}{2} \left(\frac{\gamma_{\text{MgAI}_2O_4}}{\gamma_{\text{MgCr}_2O_4}}\right). \quad (22)$$

Theoretical ln $K_{G^{\text{px-CrAlsp}}}^{\text{cpx-CrAlsp}}$ values at fixed spinel compositions were calculated from our activity-composition re-

lations at 1100 °C and the results are shown in Figure 13A together with the data of Webb and Wood (1986). The mean value of $K_a^{\text{pex-CrAlsp}}$ was found to be 1.05.

The model was also used to predict Cr^{3+} - Al^{3+} partitioning behavior between MgAl₂O₄-MgCr₂O₄ and Al₂O₃- Cr_2O_3 solid solutions. Oka et al. (1984) crystallized Cr-Al gels and reported partitioning data for this system based on their synthesis experiments at 1250, 1050, and 796 °C at 25 kbar pressure. Equilibrium between asymmetric sesquioxide solid solutions (cor) and symmetric Mg-Al₂O₄-MgCr₂O₄ solid solutions (CrAlsp) is given by the following relationship:

 $\ln K_{\rm d}^{\rm cor-CrAlsp}$

$$= \ln \frac{(X_{MgCr_{2}O_{4}}^{CrAlsp}(X_{Al_{2}O_{3}}^{Cor})}{(X_{MgCr_{2}O_{4}}^{CrAlsp})(X_{Cr_{2}O_{3}}^{cor})}$$

$$= \ln K_{a}^{cor-CrAlsp} + \frac{\ln}{2} \left(\frac{\gamma_{MgAl_{2}O_{4}}}{\gamma_{MgCr_{2}O_{4}}} \right)$$

$$+ \frac{3(W_{Cr_{2}O_{3}}^{cor} - W_{Al_{2}O_{3}}^{cor})}{2RT} (X_{Al_{2}O_{3}}^{cor})^{2}$$

$$+ \frac{(4W_{Al_{2}O_{3}}^{cor} - 2W_{Cr_{2}O_{3}}^{cor})}{2RT} X_{Al_{2}O_{3}}^{cor} - \frac{W_{Al_{2}O_{3}}^{cor}}{2RT} (23)$$

where $W_{\text{alg}O_3}^{\text{or}}$ and $W_{\text{cr}O_3}^{\text{or}}$ are asymmetric interaction parameters in Al₂O₃-Cr₂O₃ solid solutions. We calculated ln $K_a^{\text{cor}-\text{CrAlsp}}$ values following the approach outlined above for FeCr₂O₄-MgCr₂O₄ solid solutions. $W_{\text{Alg}O_3}^{\text{cor}}$ and $W_{\text{Cr}O_3}^{\text{cor}}$ values were obtained from Jacob (1978) and Chatterjee et al. (1982) while $K_a^{\text{cor}-\text{CrAlsp}}$ was set to zero. Our predicted partition coefficients at 1050 °C are in good agreement with data from Oka et al. (1984) at 1050 °C and 1250 °C given the range of possible values for the asymmetric interaction parameters in the sesquioxide (Fig. 13B).

CONCLUSIONS

We have presented a large body of thermopower and electrical conductivity data on spinel in the systems Fe₃O₄-FeCr₂O₄, and Fe₃O₄-MgCr₂O₄ and the ternary Fe₃O₄-FeAl₂O₄-FeCr₂O₄. From both experimental data and theoretical calculations we have argued that most of the data are consistent with octahedral site electron hopping between Fe²⁺ and Fe³⁺ analogous to that which is observed in pure Fe₃O₄. Activation energies for conduction increase slowly and monotonically away from Fe_3O_4 , and cation distributions calculated from the data are consistent with the formalism of O'Neill and Navrotsky (1983, 1984), which is a good description of unary and binary spinels. On the Fe_3O_4 -FeCr₂O₄ join, we were able to conduct an independent test of the Fe2+-Fe3+ hopping mechanism and found agreement between calculated and nominal concentrations of Fe at FeCr₂O₄ contents between 0 and 60%. More Cr-rich compositions cannot, however, be described by this conduction mechanism, and we believe it likely that Cr^{3+} is involved at more dilute concentrations of Fe₃O₄.

We used the data to calculate octahedral-tetrahedral cation distributions for these compositions where octahedral Fe²⁺-Fe³⁺ electron hopping appears to hold. The cation distribution data were then combined with activity-composition relations and interphase partitioning data for chrome-bearing spinels in a model that extends our previous work in (Mg²⁺,Fe²⁺)(Fe³⁺,Al³⁺)₂O₄ solid solutions (Nell and Wood, 1989) to the geologically important system $(Mg^{2+}, Fe^{2+})(Fe^{3+}, Al^{3+}, Cr^{3+})_2O_4$. We used a second-degree Taylor series expansion of the vibrational part of the Gibbs free energy in terms of order and composition parameters and constrained the values of the series expansion coefficients to be consistent with cation distribution data, activity-composition relations, and element partitioning data. The model reproduces the data from which the values of coefficients were obtained and also successfully predicts data that were not used to constrain the fit parameters.

A computer program in Fortran 77 has been written to calculate cation distributions and activities in the $(Mg^{2+}, Fe^{2+})(Fe^{3+}, Al^{3+}, Cr^{3+})_2O_4$ system. It is available on diskette or tape from the second author.

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APPENDIX 1.

Thermodynamic coefficients in a second-degree Taylor series expansion for the vibrational part of the Gibbs free energy of Fe_3O_4 -Mg Fe_2O_4 -Fe Al_2O_4 -Mg Al_2O_4 -Fe Cr_2O_4 -Mg Cr_2O_4 solid solutions.

$$\begin{split} g_{0} &= \mu_{4}^{0} + \mu_{7}^{0} - \mu_{3}^{0} + W_{[0]Mg-(0]Fe^{3}+} - W_{[0]Mg-(0]Fe^{3}+} \\ &- W_{[0]Fe^{3}+} + \Delta G_{3}^{0} - \Delta G_{3}^{0} \\ g_{r_{1}} &= \mu_{3}^{0} - \mu_{3}^{0} + 2W_{[0]Mg-(0]Fe^{3}+} + W_{[0]Fe^{3}+-(0]Fe^{3}+} \\ &- W_{[0]Mg-(0]Fe^{3}+} + \Delta G_{3}^{0} - \Delta G_{3}^{0} \\ g_{r_{2}} &= \mu_{6}^{0} - \mu_{4}^{0} + W_{[0]Mg-(0]A1} + W_{[0]A1-(0]Fe^{3}+} \\ &+ W_{[0]Fe^{3}+-(0]Fe^{3}+} - W_{[0]Mg-(0]Fe^{3}+} - W_{[0]Mg-(0]Fe^{3}+} \\ &+ \frac{W_{[0]A1-(0]Fe^{3}+}}{2} + \Delta G_{3}^{0} \\ g_{r_{3}} &= \mu_{9}^{0} - \mu_{4}^{0} + 2W_{[0]Fe^{2}+-(0]Fe^{3}+} + W_{[0]Mg-(0]Fe^{2}+} \\ &- W_{[0]Mg-(0]Fe^{3}+} + W_{[0]Fe^{2}+-(0]Fe^{3}+} + W_{[0]Mg-(0]Fe^{2}+} \\ &- W_{[0]Mg-(0]Fe^{3}+} + W_{[0]Fe^{2}+-(0]Fe^{3}+} + W_{[0]Mg-(0]Fe^{2}+} \\ &- W_{[0]A1-(0]Fe^{2}+} - W_{[0]Mg-(0]Fe^{2}+} \\ &+ W_{[0]A1-(0]Fe^{2}+} - W_{[0]He^{2}+-(0]Fe^{3}+} + W_{[0]Mg-(0]Fe^{2}+} \\ &+ \frac{W_{[0]A1-(0]Fe^{3}+} - W_{[0]Fe^{2}+-(0]Fe^{3}+} + W_{[0]Mg-(0]Fe^{2}+} \\ &- W_{[0]Mg-(0]Fe^{3}+} + \frac{W_{[0]Fe^{2}+-(0]Fe^{3}+}}{2} \\ &+ 2\Delta G_{3}^{0} - \Delta G_{3}^{0} \\ g_{r_{2}} &= \mu_{3}^{0} - \mu_{4}^{0} + 2W_{[0]Fe^{2}+-(0]Fe^{3}+} + W_{[0]Mg-(0]Fe^{2}+} \\ &- W_{[0]Mg-(0]Fe^{3}+} + \frac{W_{[0]Fe^{2}+-(0]Fe^{3}+}}{2} \\ &+ 2\Delta G_{3}^{0} - \Delta G_{3}^{0} \\ g_{r_{3}} &= \mu_{3}^{0} - \mu_{4}^{0} + 2W_{[0]He^{2}+-(0]Fe^{3}+} + W_{[0]He^{2}+-(0]Fe^{3}+} \\ &- W_{[0]Mg-(0]Fe^{3}+} + \frac{W_{[0]Fe^{2}+-(0]Fe^{3}+}}{2} \\ &+ 2\Delta G_{3}^{0} + \Delta G_{12}^{0} - \Delta G_{4}^{0} \\ g_{r_{3}} &= \mu_{3}^{0} - \mu_{4}^{0} + 2W_{[0]Mg-(0]Fe^{2}+} + W_{[0]Fe^{2}+-(0]Fe^{3}+} \\ &- W_{[0]Mg-(0]Fe^{3}+} + \frac{W_{[0]Mg-(0]Fe^{2}+}}{2} \\ &+ \Delta G_{3}^{0} + \Delta G_{12}^{0} - \Delta G_{4}^{0} \\ g_{r_{3}} &= -W_{[0]A1-(0]Fe^{3}+} - \frac{W_{[0]A1-(0]Fe^{3}+}}{2} - \Delta G_{16}^{0} \\ g_{r_{3}r_{3}} &= -W_{[0]A1-(0]Fe^{3}+} - \frac{W_{[0]A1-(0]Fe^{3}+}}{2} - \Delta G_{3}^{0} \\ g_{r_{3}r_{3}} &= -W_{[0]He^{2}+-(0]Fe^{3}+} - \frac{W_{[0]Mg-(0]Fe^{2}+}}{2} - \Delta G_{3}^{0} \\ g_{r_{3}r_{3}} &= -W_{[0]Fe^{2}+-(0]Fe^{3}+} - \frac{W_{[0]Mg-(0]Fe^{2}+}}{2} - \Delta G_{3}^{0} \\ g_{r_{3}r_{3}} &= W_{[0]Mg-(0]Fe^{2}+} - \frac{W_{[0]Mg-(0]Fe^{2}+}}{2} - \Delta G_{3}^{0} \\ g_{r_{3}r_{3}} &=$$

$$\begin{split} g_{1/2} &= W_{[0]AL-[0]Fe^{2+}} + W_{[0]Mg-(0]Fe^{2+}} - W_{[0]Mg-(0]A]} \\ &- W_{[0]Fe^{2+}-(0]Fe^{3+}} \\ g_{1/3} &= W_{[0]Mg-(0]Fe^{3+}} - W_{[0]Mg-(0]Fe^{2+}} - W_{[0]Fe^{2+}-(0]Fe^{3+}} \\ &+ \Delta G_{47}^{0} - \Delta G_{57}^{0} - \Delta G_{54}^{0} - \Delta G_{19}^{0} \\ g_{1/3} &= W_{[0]Mg-(0]Fe^{2+}} - W_{[0]Mg-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{2+}} \\ &+ \Delta G_{47}^{0} - \Delta G_{54}^{0} \\ g_{1/2} &= W_{[0]Mg-(0]Fe^{2+}} - W_{[0]Mg-(0]Fe^{2+}} - W_{[0]Fe^{2+}-(0]Fe^{3+}} \\ &+ \Delta G_{47}^{0} - \Delta G_{34}^{0} \\ g_{1/3} &= -2W_{[0]Mg-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{3+}} - W_{[0]Fe^{2+}-(0]Fe^{3+}} \\ &+ W_{[0]Cr-(0]A} - W_{[0]Fe^{3+}-(0]Fe^{3+}} - W_{[0]AL-(0]Fe^{3+}} \\ &+ W_{[0]Cr-(0]A} - W_{[0]Fe^{3+}-(0]Fe^{3+}} - W_{[0]AL-(0]Fe^{3+}} \\ &+ W_{[0]Cr-(0]A} - W_{[0]Fe^{3+}-(0]Cr} \\ &+ \frac{W_{[0]Fe^{3+}-(0]Fe^{3+}} - W_{[0]AL-(0]Fe^{3+}} - W_{[0]AL-(0]Fe^{3+}} \\ &+ \Delta G_{34}^{0} + \Delta G_{37}^{0} + \Delta G_{49}^{0} \\ g_{723} &= W_{[0]AL-(0]Fe^{3+}} + W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{3+}} \\ &+ \frac{W_{[0]Fe^{3+}-(0]Fe^{3+}} - W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{3+}} \\ &+ \frac{W_{[0]Fe^{2+}-(0]Fe^{3+}} - W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{3+}} \\ &+ \Delta G_{36}^{0} - \Delta G_{36}^{0} \\ g_{723} &= W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{3+}} - W_{[0]AL-(0]Fe^{3+}} \\ &+ \frac{W_{[0]Fe^{2+}-(0]Fe^{3+}} - \Delta G_{34}^{0} \\ g_{723} &= W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{3+}} - W_{[0]AL-(0]Fe^{3+}} \\ &+ \frac{W_{[0]Fe^{2+}-(0]Fe^{3+}} - \Delta G_{34}^{0} \\ g_{734} &= W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{2+}} \\ &+ \Delta G_{36}^{0} - \Delta G_{35}^{0} - \Delta G_{35}^{0} \\ g_{734} &= W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{2+}} \\ &+ W_{[0]Fe^{2+}-(0]Fe^{3+}} - \Delta G_{34}^{0} \\ g_{734} &= W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{2+} \\ &+ W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{2+}} - W_{[0]AL-(0]Fe^{2+} \\ \\ &+ M_{0}G_{34} - \Delta G_{37}^{0} \\ g_{7342} &= -2W_{[0]Fe^{2+}-(0]Fe^{3+} - W_{[0]Fe^{2+}-(0]Fe^{3+} - W_{[0]AL-(0]Fe^{2+} \\ \\ &+ M_{0}(AL-(0]Fe^{2+} + W_{[0]AL-(0]Fe^{2+} - W_{[0]AL-(0]Fe^{2+} + W_{[0]AL-(0]Fe^{2+} \\ \\ &+ M_{0}$$

$$- W_{16]Fe^{2+}-16]Cr} + \Delta G_{810}^{0} + \Delta G_{16}^{0} + \Delta G_{28}^{0}$$
$$- \Delta G_{49}^{0} - \Delta G_{12}^{0} - \Delta G_{46}^{0}$$
$$g_{s_1s_2} = W_{14]A1-14]Fe^{3+}} - W_{14]Fe^{2+}-14]Fe^{3+}} - W_{14]A1-14]Fe^{2+}}$$
$$+ \frac{W_{16]A1-16]Fe^{3+}} - W_{16]A1-16]Fe^{2+}} - W_{16]Fe^{2+}-16]Fe^{3+}}}{2}$$
$$+ \Delta G_{28}^{0} - \Delta G_{45}^{0} - \Delta G_{36}^{0}$$

 $g_{s_1s_3} = W_{{}^{[4]}Mg^{-[4]}Al} - W_{{}^{[4]}Mg^{-[4]}Fe^{2+}} - W_{{}^{[4]}Al^{-[4]}Fe^{2+}}$

$$+ \frac{W_{[6]_{Mg}-[6]_{Fe^{3+}}} - W_{[6]_{Fe^{2+}-[6]_{Fe^{3+}}}} - W_{[6]_{Mg}-[6]_{Fe^{2+}}}}{2} + \Delta G_{16}^{0} - \Delta G_{56}^{0}$$

$$g_{s_{2}s_{3}} = W_{[4]Mg-[4]Fe^{3+}} - W_{[4]Mg-[4]Fe^{2+}} - W_{[4]Fe^{2+}-[4]Fe^{3+}}$$

$$+\frac{W_{[6]Mg-[6]A1}-W_{[6]A1-[6]Fe^{2+}}-W_{16]Mg-[6]Fe^{2+}}}{2}$$

$$+ \Delta G_{16}^{0} + \Delta G_{78}^{0} - \Delta G_{34}^{0} - \Delta G_{12}^{0}$$