

INDEXING POWDER PATTERNS FOR CUBIC MATERIALS

F. DONALD BLOSS, *Department of Geological Sciences, Virginia Polytechnic Institute, Blacksburg, Virginia 24060*

ABSTRACT

Powder diffraction patterns for isometric crystals become self-indexing if one calculates the quotients d_1^2/d_1^2 , d_1^2/d_2^2 , \dots , d_1^2/d_n^2 where d_1 is the largest interplanar spacing observed and d_2, \dots, d_n are successively smaller ones. The resultant set of squared quotients will then identify with one of the columns in Table 1 whereupon all lines become indexed. An advantage of this method over the commonly used graphic method is that reflections for which 2θ and $(h^2+k^2+l^2)$ are large are indexed as easily as those for which 2θ and $(h^2+k^2+l^2)$ are small.

INTRODUCTION

Graphical indexing of powder diffraction data for cubic materials by means of the standard chart becomes less satisfactory for hkl reflections wherein $(h^2+k^2+l^2)$ is large in value. Consequently, one sometimes needs to index the simpler hkl reflections first, then calculate a cell edge on the basis of these reflections in order to index the back reflections. By contrast the method to be described indexes these back reflections as easily as it does those forward reflections for which 2θ and $(h^2+k^2+l^2)$ are small in value.

METHOD

To index the powder pattern of a cubic material, first determine the interplanar spacings $d_1, d_2, d_3, \dots, d_n$, where d_1 is the largest spacing observed and d_2, d_3, \dots, d_n are successively smaller spacings. Next compute $d_1^2/d_1^2, d_1^2/d_2^2, d_1^2/d_3^2, \dots, d_1^2/d_n^2$. This set of squared quotients will identify with one of the columns in Table 1—that is, all values present in the set will be present in that column. The column so identified then permits an indexing of the lines of the diffraction record by inspection.

An example will illustrate the simplicity of the method. Table 2 contains $d_1^2/d_1^2, d_1^2/d_2^2, \dots, d_1^2/d_n^2$ values as computed for synthetic spinel, $MgAl_2O_4$, from the interplanar spacings measured from a routine Debye-Scherrer powder photograph (114.6 mm diameter camera, $CuK\alpha$ radiation). This set of squared quotients is seen to be drawn from the population of numbers represented by column (3) in Table 1. Hence diffraction indices hkl are assignable to each d spacing, these values being those entered in the hkl column in Table 2. Note that, for the spinel data, the numerous hkl extinctions provide no difficulty in indexing whatsoever. As a check, the cell edge a was calculated for each line indexed from the relationship

$$a = d\sqrt{h^2 + k^2 + l^2} \quad (1)$$

The conformity of these cell-edge values thus confirms the assignment of the individual indices.

The derivation of Table 1 is readily apparent. Let $h_1k_1l_1$ represent the reflection index for the largest spacing d_1 and let hkl be the index corresponding to any other spacing d . For isometric crystals

$$a^2 = d^2(h^2 + k^2 + l^2) = d_1^2(h_1^2 + k_1^2 + l_1^2)$$

Thus

$$\frac{d_1^2}{d^2} = \frac{(h^2 + k^2 + l^2)}{(h_1^2 + k_1^2 + l_1^2)} \quad (2)$$

Depending upon whether the $h_1k_1l_1$ reflection is 100, 110, 111, 200, 210, 211, or 220, $(h_1^2 + k_1^2 + l_1^2)$ in Eq. 2 will respectively equal 1, 2, 3, 4, 5, 6, or 8. Hence the set of quotients represented by $d_1^2/d_1^2, d_1^2/d_2^2, d_1^2/d_3^2, \dots, d_1^2/d_n^2$ will contain only integers (col. 1, Table 1) if $h_1k_1l_1$ is 100, (b) integers plus half intervals (col. 2, Table 1), if $h_1k_1l_1$ is 110, (c) integers plus one-third intervals (col. 3, Table 1), if $h_1k_1l_1$ is 111, (d) integers plus one-quarter intervals (col. 4), if $h_1k_1l_1$ is 200, (e) integers plus one-fifth intervals (col. 5), if $h_1k_1l_1$ is 210 and, in general, integers plus $1/N_1$ th intervals between them where $N_1 = (h_1^2 + k_1^2 + l_1^2)$.

Measurement error is largest for d_1 but successively decreases from d_1 to d_2, \dots, d_n . Thus in obtaining the set of d_1^2/d^2 values, d^2 is known with increasing accuracy as the smaller values near to d_n are considered. Consequently the method indexes diffraction peaks for which 2θ exceeds 90° almost as readily as it indexes peaks for which 2θ is small in value.

Any method of indexing will result in ambiguities if (1) the observed d values contain large experimental errors, especially if (2) $h_1k_1l_1$ represents a reflection for which $(h_1^2 + k_1^2 + l_1^2)$ is relatively large in value. To illustrate this, consider d_1^2/d^2 values for an iron manganese garnet (Table 3) as calculated from d values reported by Vermaas (1952, p. 947). The smallest interplanar spacing, d_1 , is cited as 2.92 \AA whereas it actually is slightly in excess of 2.94 \AA . Moreover, $h_1k_1l_1$ subsequently was found to be 400, which meant that correct d_1^2/d^2 values could differ by as little as $1/16$ or 0.0625 units. Even with this error in d_1 , however, the first six d_1^2/d^2 values for this garnet permitted unequivocal rejection of columns (1) to (6) in Table 1. The observed d_1^2/d^2 values which prompted rejection of columns (7) to (13) are: (7), 1.86; (8), 1.49; (9), 1.24, 1.49; (10), 1.24, 1.49; (11), 1.24; (12), 1.49, 2.35; and (13), 1.24, 1.61. These six d_1^2/d^2 values always fall within 0.02 of a value in column (14) which was thus used to index the first seven lines. If the experimental error in d_1 had gone

TABLE 1. SETS OF d_1^2/d^2 QUOTIENTS FOR INDEXING POWDER DIFFRACTION PATTERNS OF ISOMETRIC CRYSTALS

| | | True reflection index corresponding to d_1 : | | | | | | | | | | | | | |
|------------------|---------------------------|--|---------|---------|---------|---------|---------|---------|-----------------|---------|----------|----------|----------|----------|----------|
| hkl for d | Lattice Type ^a | 100 (1) | 110 (2) | 111 (3) | 200 (4) | 210 (5) | 211 (6) | 220 (7) | 300, 221 (8) | 310 (9) | 311 (10) | 222 (11) | 320 (12) | 321 (13) | 400 (14) |
| 100 | | 1 | | | | | | | | | | | | | |
| 110 | I | 2 | 1 | | | | | | | | | | | | |
| 111 | F | 3 | 1.5 | 1 | | | | | | | | | | | |
| 200 | I, F | 4 | 2 | 1.33 | 1 | | | | | | | | | | |
| 210 | | 5 | 2.5 | 1.67 | 1.25 | 1 | | | | | | | | | |
| 211 | I | 6 | 3 | 2 | 1.5 | 1.2 | 1 | | | | | | | | |
| 220 | I, F | 8 | 4 | 2.67 | 2 | 1.6 | 1.33 | 1 | | | | | | | |
| 300, 221 | | 9 | 4.5 | 3 | 2.25 | 1.8 | 1.5 | 1.12 | 1 | | | | | | |
| 310 | I | 10 | 5 | 3.33 | 2.5 | 2 | 1.67 | 1.25 | 1.11 | 1 | | | | | |
| 311 | F | 11 | 5.5 | 3.67 | 2.75 | 2.2 | 1.83 | 1.37 | 1.22 | 1.10 | 1 | | | | |
| 222 | I, F | 12 | 6 | 4 | 3 | 2.4 | 2 | 1.5 | 1.33 | 1.20 | 1.09 | 1 | | | |
| 320 | | 13 | 6.5 | 4.33 | 3.25 | 2.6 | 2.17 | 1.62 | 1.44 | 1.30 | 1.18 | 1.08 | 1 | | |
| 321 | I | 14 | 7 | 4.67 | 3.5 | 2.8 | 2.33 | 1.75 | 1.56 | 1.40 | 1.27 | 1.17 | 1.08 | 1 | |
| 400 | I, F | 16 | 8 | 5.33 | 4 | 3.2 | 2.67 | 2 | 1.78 | 1.60 | 1.45 | 1.33 | 1.23 | 1.14 | 1 |
| 410, 322 | | 17 | 8.5 | 5.67 | 4.25 | 3.4 | 2.83 | 2.12 | 1.89 | 1.70 | 1.55 | 1.42 | 1.31 | 1.21 | 1.06 |
| 411, 330 | I | 18 | 9 | 6 | 4.5 | 3.6 | 3 | 2.25 | 2.00 | 1.80 | 1.64 | 1.50 | 1.38 | 1.29 | 1.13 |
| 331 | F | 19 | 9.5 | 6.33 | 4.75 | 3.8 | 3.17 | 2.37 | 2.11 | 1.90 | 1.73 | 1.58 | 1.46 | 1.36 | 1.18 |
| 420 | I, F | 20 | 10 | 6.67 | 5 | 4 | 3.33 | 2.5 | 2.22 | 2.00 | 1.82 | 1.67 | 1.54 | 1.43 | 1.25 |
| 421 | | 21 | 10.5 | 7 | 5.25 | 4.2 | 3.5 | 2.62 | 2.33 | 2.10 | 1.91 | 1.75 | 1.62 | 1.50 | 1.31 |
| 332 | I | 22 | 11 | 7.33 | 5.5 | 4.4 | 3.67 | 2.75 | 2.44 | 2.20 | 2.00 | 1.83 | 1.69 | 1.57 | 1.38 |
| 422 | I, F | 24 | 12 | 8 | 6 | 4.8 | 4 | 3 | 2.67 | 2.40 | 2.18 | 2.00 | 1.85 | 1.71 | 1.50 |
| 500, 430 | | 25 | 12.5 | 8.33 | 6.25 | 5 | 4.17 | 3.12 | 2.78 | 2.50 | 2.27 | 2.08 | 1.92 | 1.79 | 1.56 |
| 510, 431 | I | 26 | 13 | 8.67 | 6.5 | 5.2 | 4.33 | 3.25 | 2.89 | 2.60 | 2.36 | 2.17 | 2.00 | 1.86 | 1.63 |
| 511, 333 | F | 27 | 13.5 | 9 | 6.75 | 5.4 | 4.5 | 3.37 | 3.00 | 2.70 | 2.45 | 2.25 | 2.08 | 1.93 | 1.69 |
| 520, 432 | | 29 | 14.5 | 9.67 | 7.25 | 5.8 | 4.83 | 3.62 | 3.22 | 2.90 | 2.64 | 2.42 | 2.23 | 2.07 | 1.81 |
| 521 | I | 30 | 15 | 10 | 7.5 | 6 | 5 | 3.75 | 3.33 | 3.00 | 2.73 | 2.50 | 2.31 | 2.14 | 1.88 |
| 440 | I, F | 32 | 16 | 10.67 | 8 | 6.4 | 5.33 | 4 | 3.56 | 3.20 | 2.91 | 2.67 | 2.46 | 2.29 | 2.00 |
| 522, 441 | | 33 | 16.5 | 11 | 8.25 | 6.6 | 5.5 | 4.12 | 3.67 | 3.30 | 3.00 | 2.75 | 2.54 | 2.36 | 2.06 |
| 530, 433 | I | 34 | 17 | 11.33 | 8.5 | 6.8 | 5.67 | 4.25 | 3.78 | 3.40 | 3.09 | 2.83 | 2.62 | 2.43 | 2.13 |
| 531 | F | 35 | 17.5 | 11.67 | 8.75 | 7 | 5.83 | 4.37 | 3.89 | 3.50 | 3.18 | 2.92 | 2.69 | 2.50 | 2.19 |
| 600, 442 | I, F | 36 | 18 | 12 | 9 | 7.2 | 6 | 4.5 | 4.00 | 3.60 | 3.27 | 3.00 | 2.76 | 2.57 | 2.25 |
| 610 | | 37 | 18.5 | 12.33 | 9.25 | 7.4 | 6.17 | 4.62 | 4.11 | 3.70 | 3.36 | 3.08 | 2.85 | 2.64 | 2.31 |
| 611, 532 | I | 38 | 19 | 12.67 | 9.5 | 7.6 | 6.33 | 4.75 | 4.22 | 3.80 | 3.45 | 3.17 | 2.92 | 2.71 | 2.38 |
| 620 | I, F | 40 | 20 | 13.33 | 10 | 8 | 6.67 | 5 | 4.44 | 4.00 | 3.64 | 3.33 | 3.08 | 2.86 | 2.50 |
| 443, 621, 540 | | 41 | 20.5 | 13.67 | 10.25 | 8.2 | 6.83 | 5.12 | 4.56 | 4.10 | 3.73 | 3.42 | 3.15 | 2.93 | 2.56 |
| 541 | I | 42 | 21 | 14 | 10.5 | 8.4 | 7 | 5.25 | 4.67 | 4.20 | 3.82 | 3.50 | 3.23 | 3.00 | 2.63 |
| 533 | F | 43 | 21.5 | 14.33 | 10.75 | 8.6 | 7.17 | 5.37 | 4.78 | 4.30 | 3.91 | 3.58 | 3.31 | 3.07 | 2.69 |
| 622 | I, F | 44 | 22 | 14.67 | 11 | 8.8 | 7.33 | 5.5 | 4.89 | 4.40 | 4.00 | 3.67 | 3.38 | 3.14 | 2.75 |
| 630, 542 | | 45 | 22.5 | 15 | 11.25 | 9 | 7.5 | 5.62 | 5.00 | 4.50 | 4.09 | 3.75 | 3.46 | 3.21 | 2.81 |
| 631 | I | 46 | 23 | 15.33 | 11.50 | 9.2 | 7.67 | 5.75 | 5.11 | 4.60 | 4.18 | 3.83 | 3.54 | 3.29 | 2.88 |

^a Entries in this column indicate whether the reflection index cited at left is possible for a body centered lattice (I) or for a face centered lattice (F) in addition to a primitive lattice.

TABLE 1.—(continued)

| | | True reflection index corresponding to d_1 : | | | | | | | | | | | | | |
|------------------|-----------------|--|------------|------------|------------|------------|------------|------------|--------------------|------------|-------------|-------------|-------------|-------------|-------------|
| hkl for d | Lattice Type | 100 (1) | 110 (2) | 111 (3) | 200 (4) | 210 (5) | 211 (6) | 220 (7) | 300, 221 (8) | 310 (9) | 311 (10) | 222 (11) | 320 (12) | 321 (13) | 400 (14) |
| 444 | I, F | 48 | 24 | 16 | 12 | 9.6 | 8 | 6 | 5.33 | 4.80 | 4.36 | 4.00 | 3.69 | 3.43 | 3.00 |
| 700, 632 | | 49 | 24.5 | 16.33 | 12.25 | 9.8 | 8.17 | 6.12 | 5.44 | 4.90 | 4.45 | 4.08 | 3.77 | 3.50 | 3.06 |
| 710, 550, | | | | | | | | | | | | | | | |
| 543 | I | 50 | 25 | 16.67 | 12.50 | 10 | 8.33 | 6.25 | 5.56 | 5.00 | 4.55 | 4.17 | 3.85 | 3.57 | 3.13 |
| 711, 551 | F | 51 | 25.5 | 17 | 12.75 | 10.2 | 8.5 | 6.37 | 5.67 | 5.10 | 4.64 | 4.25 | 3.92 | 3.64 | 3.19 |
| 640 | I, F | 52 | 26 | 17.33 | 13 | 10.4 | 8.67 | 6.5 | 5.78 | 5.20 | 4.73 | 4.33 | 4.00 | 3.71 | 3.25 |
| 720, 641 | | 53 | 26.5 | 17.67 | 13.25 | 10.6 | 8.83 | 6.62 | 5.89 | 5.30 | 4.82 | 4.42 | 4.08 | 3.79 | 3.31 |
| 721, 633, | | | | | | | | | | | | | | | |
| 552 | I | 54 | 27 | 18 | 13.50 | 10.8 | 9 | 6.75 | 6.00 | 5.40 | 4.91 | 4.50 | 4.15 | 3.86 | 3.38 |
| 642 | I, F | 56 | 28 | 18.67 | 14 | 11.2 | 9.33 | 7 | 6.22 | 5.60 | 5.09 | 4.67 | 4.31 | 4.00 | 3.50 |
| 722, 544 | | 57 | 28.5 | 19 | 14.25 | 11.4 | 9.5 | 7.12 | 6.33 | 5.70 | 5.18 | 4.75 | 4.38 | 4.07 | 3.56 |
| 730 | I | 58 | 29 | 19.33 | 14.5 | 11.6 | 9.67 | 7.25 | 6.44 | 5.80 | 5.27 | 4.83 | 4.46 | 4.14 | 3.63 |
| 731, 553 | F | 59 | 29.5 | 19.67 | 14.75 | 11.8 | 9.83 | 7.37 | 6.56 | 5.90 | 5.36 | 4.92 | 4.54 | 4.21 | 3.69 |
| 650, 643 | | 61 | 30.5 | 20.33 | 15.25 | 12.2 | 10.17 | 7.62 | 6.78 | 6.10 | 5.55 | 5.08 | 4.69 | 4.36 | 3.81 |
| 732, 651 | I | 62 | 31 | 20.67 | 15.5 | 12.4 | 10.33 | 7.75 | 6.89 | 6.20 | 5.64 | 5.17 | 4.77 | 4.43 | 3.88 |
| 800 | I, F | 64 | 32 | 21.33 | 16 | 12.8 | 10.67 | 8 | 7.11 | 6.40 | 5.82 | 5.33 | 4.92 | 4.57 | 4.00 |
| 810, 740, | | | | | | | | | | | | | | | |
| 652 | | 65 | 32.5 | 21.67 | 16.25 | 13 | 10.83 | 8.12 | 7.22 | 6.50 | 5.91 | 5.42 | 5.00 | 4.64 | 4.06 |
| 811, 741, | | | | | | | | | | | | | | | |
| 554 | I | 66 | 33 | 22 | 16.50 | 13.2 | 11 | 8.25 | 7.33 | 6.60 | 6.00 | 5.50 | 5.08 | 4.71 | 4.13 |
| 733 | | 67 | 33.5 | 22.33 | 16.75 | 13.4 | 11.17 | 8.37 | 7.44 | 6.70 | 6.09 | 5.58 | 5.15 | 4.79 | 4.19 |
| 820, 644 | I, F | 68 | 34 | 22.67 | 17 | 13.6 | 11.33 | 8.5 | 7.56 | 6.80 | 6.18 | 5.67 | 5.23 | 4.86 | 4.25 |
| 821, 742 | | 69 | 34.5 | 23 | 17.25 | 13.8 | 11.5 | 8.62 | 7.67 | 6.90 | 6.27 | 5.75 | 5.31 | 4.93 | 4.31 |
| 653 | I | 70 | 35 | 23.33 | 17.5 | 14 | 11.67 | 8.75 | 7.78 | 7.00 | 6.36 | 5.83 | 5.38 | 5.00 | 4.38 |
| 822, 660 | I, F | 72 | 36 | 24 | 18 | 14.4 | 12 | 9 | 8.00 | 7.20 | 6.55 | 6.00 | 5.54 | 5.14 | 4.50 |
| 830, 661 | | 73 | 36.5 | 24.33 | 18.25 | 14.6 | 12.17 | 9.12 | 8.11 | 7.30 | 6.64 | 6.08 | 5.62 | 5.21 | 4.56 |
| 831, 750, | | | | | | | | | | | | | | | |
| 743 | I | 74 | 37 | 24.67 | 18.5 | 14.8 | 12.33 | 9.25 | 8.22 | 7.40 | 6.73 | 6.17 | 5.69 | 5.29 | 4.63 |
| 751, 555 | F | 75 | 37.5 | 25 | 18.75 | 15 | 12.5 | 9.37 | 8.33 | 7.50 | 6.82 | 6.25 | 5.77 | 5.36 | 4.69 |
| 662 | I, F | 76 | 38 | 25.33 | 19 | 15.2 | 12.67 | 9.5 | 8.44 | 7.60 | 6.91 | 6.33 | 5.85 | 5.43 | 4.75 |
| 832, 654 | | 77 | 38.5 | 25.67 | 19.25 | 15.4 | 12.83 | 9.62 | 8.56 | 7.70 | 7.00 | 6.42 | 5.92 | 5.50 | 4.81 |
| 752 | I | 78 | 39 | 26 | 19.5 | 15.6 | 13 | 9.75 | 8.67 | 7.80 | 7.09 | 6.50 | 6.00 | 5.57 | 4.88 |
| 840 | I, F | 80 | 40 | 26.67 | 20 | 16 | 13.33 | 10 | 8.89 | 8.00 | 7.27 | 6.67 | 6.15 | 5.71 | 5.00 |
| 900, 841, | | | | | | | | | | | | | | | |
| 744, 663 | | 81 | 40.5 | 27 | 20.25 | 16.2 | 13.5 | 10.12 | 9.00 | 8.10 | 7.36 | 6.75 | 6.23 | 5.79 | 5.06 |
| 910, 833 | I | 82 | 41 | 27.33 | 20.5 | 16.4 | 13.67 | 10.25 | 9.11 | 8.20 | 7.45 | 6.83 | 6.31 | 5.86 | 5.13 |
| 911, 753 | F | 83 | 41.5 | 27.67 | 20.75 | 16.6 | 13.83 | 10.37 | 9.22 | 8.30 | 7.55 | 6.92 | 6.38 | 5.93 | 5.19 |
| 842 | I, F | 84 | 42 | 28 | 21 | 16.8 | 14 | 10.5 | 9.33 | 8.40 | 7.64 | 7.00 | 6.46 | 6.00 | 5.25 |
| 920, 760 | | 85 | 42.5 | 28.33 | 21.25 | 17 | 14.17 | 10.62 | 9.44 | 8.50 | 7.73 | 7.08 | 6.54 | 6.07 | 5.31 |
| 921, 761, | | | | | | | | | | | | | | | |
| 655 | I | 86 | 43 | 28.67 | 21.50 | 17.2 | 14.33 | 10.75 | 9.56 | 8.60 | 7.82 | 7.17 | 6.62 | 6.14 | 5.38 |
| 664 | I, F | 88 | 44 | 29.33 | 22 | 17.6 | 14.67 | 11 | 9.78 | 8.80 | 8.00 | 7.33 | 6.77 | 6.29 | 5.50 |

unnoticed, column (14) would have misindexed those indices marked *a* in Table 3. However, one would have been alerted to the error because $\Delta d_1^2/d_2$, the difference between d_1^2/d^2 (observed) compared to what it

TABLE 2. OBSERVED 2θ AND CALCULATED d_1^2/d^2 VALUES FOR A POWDER FILM OF SYNTHETIC SPINEL, $MgAl_2O_4$

| 2θ (obs) | d | d_1^2/d^2 | hkl | N^a | a (calc) ^b |
|--------------------|--------|-------------|---------|-------|-------------------------|
| 19.02 α | 4.6658 | 1 | 111 | 3 | 8.0814 |
| 31.30 α | 2.8577 | 2.666 | 220 | 8 | 8.0828 |
| 36.894 α | 2.4365 | 3.667 | 311 | 11 | 8.0810 |
| 44.84 α | 2.0212 | 5.329 | 400 | 16 | 8.0848 |
| 55.702 α | 1.6501 | 7.994 | 422 | 24 | 8.0838 |
| 59.427 α | 1.5553 | 8.999 | 511/333 | 27 | 8.0816 |
| 65.287 α | 1.4291 | 10.659 | 440 | 32 | 8.0842 |
| 68.736 α | 1.3656 | 11.673 | 531 | 35 | 8.0790 |
| 74.19 α | 1.2781 | 13.327 | 620 | 40 | 8.0834 |
| 77.388 α | 1.2331 | 14.317 | 533 | 43 | 8.0860 |
| 82.691 α | 1.1670 | 15.984 | 444 | 48 | 8.0852 |
| 85.78 α | 1.1327 | 16.968 | 711/551 | 51 | 8.0891 |
| 94.171 α_1 | 1.0517 | 19.678 | 731/553 | 59 | 8.7826 |
| 94.451 α_2 | 1.0520 | | | | 8.0806 |
| 99.37 α_1 | 1.0102 | 21.337 | 800 | 64 | 8.0816 |
| 99.72 α_2 | 1.0101 | | | | 8.0808 |
| 107.92 α_1 | .95257 | 23.994 | 822/660 | 72 | 8.0828 |
| 108.327 α_2 | .95248 | | | | 8.0821 |
| 111.26 α_1 | .93318 | 24.995 | 751/555 | 75 | 8.0816 |
| 111.656 α_2 | .93330 | | | | 8.0826 |
| 116.944 α_1 | .90365 | 26.665 | 840 | 80 | 8.0825 |
| 117.45 α_2 | .90345 | | | | 8.0807 |
| 120.50 α_1 | .88719 | 27.667 | 911/753 | 83 | 8.0827 |
| 121.074 α_2 | .88686 | | | | 8.0797 |
| 130.744 α_1 | .84733 | 30.321 | 931 | 91 | 8.0836 |
| 131.366 α_2 | .84734 | | | | 8.0831 |
| 138.028 α_1 | .82497 | 31.987 | 844 | 96 | 8.0830 |
| 138.785 α_2 | .82495 | | | | 8.0828 |

^a $N = h^2 + k^2 + l^2$ ^b $a = d\sqrt{N}$

should be to conform precisely to column (14), systematically increases from 0.01 for 420 to 0.04 for reflection 444. One could correct these observed d_1^2/d^2 values either by (1) taking d as 2.94 and recomputing or (2) adding the value of $\Delta d_1^2/d^2$ for each previously indexed line to the d_1^2/d^2 value for the next higher angle line to be indexed. To illustrate this second method, 0.04 the $\Delta d_1^2/d^2$ value for 444 would be added to the 3.20 value to make it 3.24, which brings it close enough to its error-free

TABLE 3. INDEXING AN IRON MANGANESE GARNET

| Observed | | From Table 1, col. 14 | | | | |
|----------|--|-----------------------|--|--------------------|------------------|----------|
| <i>d</i> | <i>d</i> ₁ ² / <i>d</i> ² | <i>hkl</i> | <i>d</i> ₁ ² / <i>d</i> ² | $\Delta d_1^2/d^2$ | <i>N</i> | <i>a</i> |
| 2.92 | 1 | 400 | 1 | | 16 | 11.68 |
| 2.62 | 1.24 | 420 | 1.25 | 0.01 | 20 | 11.72 |
| 2.39 | 1.49 | 422 | 1.50 | 0.01 | 24 | 11.71 |
| 2.30 | 1.61 | 510, 431 | 1.63 | 0.02 | 26 | 11.73 |
| 2.14 | 1.86 | 521 | 1.88 | 0.02 | 30 | 11.72 |
| 1.906 | 2.35 | 611, 532 | 2.38 | 0.03 | 38 | 11.75 |
| 1.698 | 2.96 | 444 | 3.00 | 0.04 | 48 | 11.76 |
| 1.632 | 3.20 | 640 ^a | 3.25 | 0.05 | 52 | 11.77 |
| 1.574 | 3.44 | 642 ^a | 3.50 | 0.06 | 56 | 11.78 |
| 1.474 | 3.92 | 800 ^a | 4.00 | 0.08 | 64 | 11.79 |
| 1.316 | 4.92 | 840 ^a | 5.00 | 0.08 | 80 | 11.77 |
| 1.288 | 5.14 | 842 ^a | 5.25 | 0.11 | 84 | 11.80 |
| 1.257 | 5.40 | 664 ^a | 5.50 | 0.11 | 88 | 11.79 |
| 1.095 | 7.11 | | | | 116 ^b | 11.79 |
| 1.077 | 7.35 | | | | 120 ^b | 11.80 |
| 1.043 | 7.69 | | | | 128 ^b | 11.80 |
| 0.983 | 8.82 | Beyond Table 1 | | | 144 ^b | 11.80 |
| 0.971 | 9.04 | | | | 148 ^b | 11.81 |
| 0.968 | 9.10 | | | | 149 ^b | 11.82 |

^a Denotes a reflection index which would have been misindexed if the error in *d*₁ (2.92 Å) had not been detected through failure to recognize the systematic increase in error, $\Delta d_1^2/d^2$, where this equals $(d_1^2/d^2)_{\text{Table}}$ minus $(d_1^2/d^2)_{\text{obs.}}$, for *hkl* 400 to 444.

^b These values of *N* lead to values for the cell edge *a* which continue the trend in computed *a* established by reflections for which *N* was 88 or less. Knowledge of these *N* values thus permits indexing the reflections whose *d*₁²/*d*² values exceeded those given in Table 1.

value of 3.25 to permit its ready indexing as 640. Without such correction, column (14) would have misindexed the line as 711, 551. Using such corrections the lines were correctly indexed down to 1.257 Å.

For each of these indexed lines, the cell edge *a* was then computed by using Eq. 1. Taking the value of *a* as 11.80 or 11.79 Å, one can determine *N* for the as yet nonindexed lines because

$$N^2 = \frac{a^2}{d^2}$$

Results again agree with Vermaas' indexing except for *d*=0.968 whose index should be 12.2.1, 10.7.0, 9.8.2 and/or 8.7.6 rather than 12.2.2 and/or 10.6.4.

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