**Revision 1 MS 5328** 1 2 3 The W-WO<sub>2</sub> oxygen fugacity buffer (WWO) at high pressure and temperature: 4 Implications for fO<sub>2</sub> buffering and metal-silicate partitioning. 5 6 Gregory A. Shofner<sup>1\*</sup>, Andrew J. Campbell<sup>2</sup>, Lisa R. Danielson<sup>3</sup>, Kevin Righter<sup>4</sup>, Rebecca A. Fischer<sup>2</sup>, Yanbin Wang<sup>5</sup>, and Vitali Prakapenka<sup>5</sup> 7 8 9 <sup>1</sup>Department of Physics, Astronomy and Geosciences, Towson University, 8000 York 10 Road, Towson, MD 21252, USA 11 <sup>2</sup>The University of Chicago, Department of the Geophysical Sciences, 5734 South Ellis 12 Avenue, Chicago, IL 60637, USA 13 <sup>3</sup>Jacobs Technology, NASA Johnson Space Center, 2101 NASA Parkway, Houston, TX 14 77058, USA 15 <sup>4</sup>Mailcode KT, NASA Johnson Space Center, 2101 NASA Parkway, Houston, TX 77058, 16 17 USA <sup>5</sup>Center for Advanced Radiation Sources, The University of Chicago, Building 434A, 18 Argonne National Laboratory, 9700 South Cass Ave. Argonne, IL 60439 19 20 **Abstract** 21 Synchrotron x-ray diffraction data were obtained to simultaneously measure unit cell 22 volumes of W and WO<sub>2</sub> at pressures and temperatures up to 70 GPa and 2300 K. Both W 23 and WO<sub>2</sub> unit-cell volume data were fit to Mie-Grüneisen equations of state; parameters for 24 W are  $K_T = 307 ~(\pm 0.4)$  GPa,  $K_T' = 4.05 ~(\pm 0.04)$ ,  $\gamma_0 = 1.61 ~(\pm 0.03)$ , and  $q = 1.54 ~(\pm 0.13)$ . 25 Three phases were observed in WO<sub>2</sub> with structures in the P2<sub>1</sub>/c, Pnma and C2/c space 26 27 groups. The transition pressures are 4 GPa and 32 GPa for the P2<sub>1</sub>/c-Pnma and Pnma-C2/c phase changes, respectively. The P2<sub>1</sub>/c and Pnma phases have previously been described 28 whereas the C2/c phase is newly described here. Equations of state were fitted for these 29 phases over their respective pressure ranges yielding the parameters  $K_T = 238 \ (\pm 7), \ 230$ 30  $(\pm 5)$ , 304  $(\pm 3)$  GPa,  $K_T$ ' = 4 (fixed), 4 (fixed), 4 (fixed) GPa,  $\gamma_0 = 1.45$   $(\pm 0.18)$ , 1.22  $(\pm 0.07)$ , 31

1.21 ( $\pm 0.12$ ), and q = 1 (fixed), 2.90 ( $\pm 1.5$ ), 1 (fixed) for the  $P2_1/c$ , Pnma and C2/c phases, respectively. The W-WO<sub>2</sub> buffer (WWO) was extended to high pressure using these W and WO<sub>2</sub> equations of state. The T-fO<sub>2</sub> slope of the WWO buffer along isobars is positive from 1000 to 2500K with increasing pressure up to at least 60 GPa. The WWO buffer is at a higher fO<sub>2</sub> than the iron-wüstite (IW) buffer at pressures lower than 40 GPa, and the magnitude of this difference decreases at higher pressures. This implies an increasingly lithophile character for W at higher pressures. The WWO buffer was quantitatively applied to W metal-silicate partitioning by using the WWO-IW buffer difference in combination with literature data on W metal-silicate partitioning to model the exchange coefficient (K<sub>D</sub>) for the Fe-W exchange reaction. This approach captures the non-linear pressure dependence of W metal-silicate partitioning using the WWO-IW buffer difference. Calculation of K<sub>D</sub> along a peridotite liquidus predicts a decrease in W siderophility at higher pressures that supports the qualitative behavior predicted by the WWO-IW buffer difference, and agrees with findings of others. Comparing the competing effects of temperature and pressure the results here indicate that pressure exerts a greater effect on W metal-silicate partitioning. Keyword: high pressure, tungsten, oxygen fugacity buffer, equation of state, metal-silicate partitioning

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Knowledge of volumetric properties of metals and oxides at high pressure and temperature contributes to our understanding of metal-silicate equilibria within planetary interiors, the latter of which can exert a strong influence on the chemical potential of oxygen (or oxygen fugacity, fO<sub>2</sub>). The coexistence of a metal and its oxide at equilibrium constitutes an oxygen buffer, and can be used in 1-bar or high pressure experimentation to control or calculate fO<sub>2</sub> (e.g., Cottrell et

al. 2009, 2010; Burkemper et al. 2012; Dobson and Brodholt, 1999; Rubie, 1999). A common example relevant to the deep Earth is the iron–wüstite (IW) buffer which is often used to control and measure the fO<sub>2</sub> of Fe-bearing experiments. However, in non Fe-bearing experiments where fO<sub>2</sub> similar to IW is desired or in cases requiring fO<sub>2</sub> conditions more oxidizing or reducing than IW, an alternative buffer must be used. The fO<sub>2</sub> of the W-WO<sub>2</sub> (WWO) buffer is equal to IW at approximately 1200 K (at 1 bar), and becomes more oxidizing with increasing temperature, becoming approximately one log unit higher at 2200 K. For this reason, the WWO buffer is well-suited to experiments where fO<sub>2</sub> similar to that of IW is required, e.g. Cottrell et al. (2009, 2010) controlled and calculated experimental fO<sub>2</sub> using the WWO buffer in Fe-free, W-bearing melting experiments.

Oxygen fugacity buffers can have significant pressure dependencies. The volume difference between the metal and oxide of a buffer is used to obtain fO<sub>2</sub> along the buffer at high pressures, and therefore differences in compressibility of the metal and oxide can result in significant deviations of calculated fO<sub>2</sub> relative to 1-bar. The WWO buffer has been studied at ambient pressure conditions and at temperatures up to approximately 1700K (O'Neill and Pownceby 1993), but it has no experimental constraints at high pressure. Extension of the 1-bar buffers for application to high pressure experiments or to the conditions of the deep Earth requires precisely determined phase volumes of the metal and oxide phases at high pressure (Campbell et al. 2009), which can be calculated using equations of state.

The equation of state of W has been determined using extensive high pressure and temperature experimental constraints (Houska, 1964; Grimvall et al., 1987; Dewaele et al. 2004; Dorogokupets and Oganov 2007). The equation of state of WO<sub>2</sub>, however, is limited to room-temperature elastic parameters determined from a computational study with no experimental

constraints (Dewhurst and Lowther 2001). Known phases of WO<sub>2</sub> are a  $P2_1/c$  structure at 1-bar (Bolzan et al. 1995) and a Pnma structure that was synthesized at 8 GPa and 1120 K and characterized by x-ray diffraction at 1-bar and room temperature (Sundberg et al. 1994). The  $P2_1/c$  and Pnma structured phases will be referred to as ap-WO<sub>2</sub> and hp-WO<sub>2</sub> following the naming convention of Sundberg et al. (1994). Nothing is known experimentally about WO<sub>2</sub> at pressures and temperatures higher than the studied conditions of the hp-WO<sub>2</sub> phase, and consequently the behavior of the WWO buffer is imprecisely constrained at higher pressures. Therefore, we have conducted high pressure and high temperature experiments to characterize the WWO buffer. The data are also applied to better understand the thermodynamics of W partitioning between metal and silicate under magma ocean conditions. The experimental work to characterize the WWO buffer was conducted using both diamond anvil cell (DAC) and multianvil press (MAP) techniques in conjunction with synchrotron x-ray diffraction.

# **Synchrotron X-ray diffraction experiments**

To obtain thermal equations of state (EOS) and oxygen fugacity buffers for the W-WO<sub>2</sub> system, x-ray diffraction data were collected on coexisting W and WO<sub>2</sub>. The sample materials were mixtures of approximately 1:1 by weight of W:WO<sub>2</sub> using powders acquired from Alfa-Aesar (>99.9% pure). Room-temperature DAC compression experiments included Pt as a pressure standard and the mixture was approximately 1:1:1 by weight of W:WO<sub>2</sub>:Pt. Powders were ground under ethanol in agate mortars to ~1 micron grain size for DAC experiments; for MAP experiments the powder mixtures were ground for approximately 15 minutes to homogenize the distribution of the phases. These data were collected across a wide range of pressures and temperatures (Figure 1) using diamond anvil cells at beamline X17C of the National Synchrotron Light Source (NSLS), Brookhaven National Laboratory, and using

diamond anvil cells and a multi anvil press at beamline 13-ID-D of the Advanced Photon Source (APS), Argonne National Laboratory. Making measurements of both metal and oxide in the same experiment was important because the oxygen fugacity buffer is defined in terms of the equilibrium between metal and oxide. It was also advantageous that both phases are present under the same experimental conditions in EOS calculations because the volume differences (ΔV) between the phases were referenced to exactly the same P-T conditions. This reduced or eliminated uncertainties due to pressure standardization and heterogeneous experimental conditions (P or T gradients) when coupling the two EOS for consideration of the metal-oxide buffer.

### Diamond anvil cell

Room temperature compression provides the foundation for the thermal EOS. Coexisting W and WO<sub>2</sub> were compressed in DACs using an argon pressure medium over a pressure range of approximately 25 to 73 GPa. X-ray diffraction data were collected on beamline X17C at NSLS using angle-dispersive diffraction with diffraction patterns collected on a CCD (MAR) x-ray area detector. These x-ray diffraction data were used to determine unit cell volumes of the individual phases. Experimental pressures were determined using Pt as a pressure standard (Fei et al. 2007). The W data were included in the calculation of the W EOS as discussed in later sections. The room temperature WO<sub>2</sub> data were not included in EOS calculations because robust unit-cell volumes could not be obtained due to a sluggish phase transition from the *ap*-WO<sub>2</sub> to the *hp*-WO<sub>2</sub> phase at room temperature. As discussed in later sections, the *ap*-WO<sub>2</sub> and the *hp*-WO<sub>2</sub> phases coexisted over a pressure range of at least 20 GPa, which was evidenced by peaks for both phases in diffraction patterns over this pressure range.

Laser-heated DAC experiments were conducted at APS on coexisting W and WO2 where x-

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ray diffraction data were collected at temperatures up to approximately 2250 K and at pressures up to approximately 70 GPa. The sample was prepared by compression of the starting mixture into a thin layer that was ~5 µm thick. The sample was loaded into a symmetric-type DAC between layers of NaCl that served as both insulator and as a pressure standard (Decker 1971; Fei et al. 2007). The Pt pressure scale used in the 300 K experiments was calibrated with the NaCl pressure scale used in the high temperature experiments – both used Fei et al. (2007). The sample chamber was made by drilling an 80 micron hole in a pre-indented rhenium gasket and was compressed between diamond anvils with 250 micron culet diameters. The monochromatic x-ray source had a wavelength of 0.3344 Å and was focused to a spot size of ~3 µm diameter. The diffraction data were measured using an angle-dispersive configuration and diffraction patterns were collected using a MAR165 CCD x-ray area detector with the sample to detector distance calibrated by 1-bar CeO<sub>2</sub> diffraction patterns. The sample was heated on both sides using twin ytterbium fiber lasers with approximate spot sizes of 20 microns (Prakapenka et al., 2008). Laser powers were adjusted to equalize the temperatures on the two sample surfaces. The lasers were directed onto the sample using x-ray transparent optics which permitted the laser and x-ray beams to be coaxial, and allowed for collection of x-ray diffraction data at high temperatures (Shen et al. 2001). Temperatures were measured using spectro-radiometry and the resulting thermal emission spectra were fitted to the Planck function using the greybody approximation (Heinz and Jeanloz 1987). These measurements were of the temperature at the interface between the sample and the insulating layer, i.e. at the surface of the sample, and over an area of approximately 5 x 5 microns at the center of the laser-heated spot. The sample in this experiment was opaque and most of the laser radiation was absorbed at the sample surface, and consequently the temperature in the axial center of the sample where it was being probed by the

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x-ray beam was slightly lower than the measured temperature. The reported experimental temperatures were corrected for this axial thermal gradient, which was an approximately three percent decrease from the measured temperatures, based on an approximate sample thickness of 5 microns (Campbell et al. 2007; 2009). Because of technical difficulties with the downstream (relative to the x-ray beam) temperature measurements during these experiments, the temperatures reported here are those measured in the upstream direction only (Fischer et al., 2011). Four heating cycles were made, with starting pressures of approximately 18, 39, 53, and 67 GPa at ambient temperature; these are hereafter referred to as the 20, 40, 55, and 70 GPa cycles. Laser power was gradually increased and diffraction patterns were collected up to the peak temperature for a given pressure step. The laser power was then decreased gradually and diffraction patterns were collected approximately every 100 degrees. The pressure in the diamond cell was increased at room temperature between each heating cycle. The diffraction data from the cooling portion of each heating cycle were used in EOS calculations to minimize uncertainties related to non-hydrostatic stresses, which are greatly reduced after high temperature treatment. Resistively-heated DAC experiments (RHDAC) were made using an external heating system that was developed in the University of Maryland Laboratory for Mineral Physics, which allowed for sample chamber temperatures up to approximately 725 K. This heater design completely enclosed a Tel-Aviv-type DAC, which minimized temperature gradients but caused the pressure to decrease during heating. X-ray diffraction data were collected at beamline X17C at NSLS using this DAC assembly. Diffraction patterns were collected at discrete temperatures and at four different starting pressures. The sample was insulated between layers of NaCl, which also served as a pressure calibrant (Decker 1971; Fei et al. 2007). Temperatures were measured using a type K thermocouple that was placed at the contact between the diamond culets. This was done by wrapping the thermocouple loop around the diamonds and cementing the loop to the gasket using alumina cement obtained from Zircar Ceramics.

# Multi anvil press

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Diffraction patterns were collected using the T25 module in the 1000 ton MAP using a COMPRES octahedral 10/5 assembly (Leinenweber et al. 2006), at beamline 13-ID-D at the Advanced Photon Source. Boron nitride capsules were used because their low mean atomic number results in minimal attenuation of the x-ray beam, and samples were heated with Re or LaCrO<sub>3</sub> (Leinenweber et al., 2006, 2012) heaters. The entire cube assembly was aligned to allow the x-ray beam to pass between the gaps of the WC cubes, the "equatorial" graphite window, and slits in the Re and LaCrO<sub>3</sub> in the octahedral assembly. Diffracted x-rays were detected using a cooled Ge energy-dispersive detector placed at a fixed 20 angle of 6° relative to the incoming xray beam. The sample capsule had two chambers; one contained a mixture of W and WO<sub>2</sub>, and the other contained MgO as a pressure calibrant. The equation of state for MgO of Speziale et al. (2001) was used and is compatible with the Pt and NaCl EOS of Fei et al. (2007) described above. An initial heating cycle was made at a press force of 800 tons corresponding to a pressure of approximately 20 GPa at 2100 K. Similar to LHDAC experiments, data were collected on the heating and cooling portions of this cycle but only the cooling data were used in EOS calculations. It was noted during the second cycle, at 400 tons press force, that the W diffraction peaks were weakening in relative intensity to those of WO<sub>2</sub>. At this point the experiment was decompressed at constant temperature; data obtained at press forces of 350 and 270 tons were used in EOS calculations. Examination of the run product from this experiment revealed no W

metal, which suggests that the metal became oxidized over the course of the experiment which is why the W diffraction intensities decreased so significantly. Tungsten carbide was not observed either. The WO<sub>2</sub> remained a stable phase, consistent with successful indexing of the diffraction data to the published orthorhombic (Pnma) structure (Sundberg et al. 1994). Microprobe analyses of the WO<sub>2</sub> yielded W contents consistent with a stoichiometric phase, but future work may want to examine this in more detail and for all three WO<sub>2</sub> phases.

199 Data Analysis

The foundational data for characterizing the equations of state were x-ray diffraction patterns in the form of either two-dimensional CCD images or one-dimensional energy spectra collected by a solid-state Ge, energy-dispersive detector. The 2-d diffraction patterns were calibrated with CeO<sub>2</sub> and processed using the Fit2D software, which integrates a diffraction image to produce a 1-d spectrum of  $2\theta$  angle versus intensity (Hammersley et al., 1996). The 1-d energy dispersive spectra were converted to *d*-spacing versus intensity spectra by applying energy and  $2\theta$  calibrations. Energy calibrations were based on radioactive <sup>57</sup>Co and <sup>109</sup>Cd sources, and Ag K<sub>\alpha</sub> and K<sub>\beta1</sub> lines. The  $2\theta$  calibration was based on a 1-bar x-ray diffraction pattern of Al<sub>2</sub>O<sub>3</sub>. The x-ray diffraction peaks in the experimental spectra were fitted using the PeakFit<sup>TM</sup> software by SeaSolve Software Inc., which also allowed for background subtraction.

Because the difference in molar volume between the phases is used to calculate the  $fO_2$  of the WWO buffer, the principal information needed was the molar volumes of the W and WO<sub>2</sub> phases at each P-T point. The molar volumes were calculated using the unit cell volumes and the number of formula units per unit cell (Z).

Tungsten, sodium chloride, magnesium oxide, and platinum are cubic and for each reflection a lattice parameter a was calculated from the measured d-spacings and the assigned Miller

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indices  $h \ k \ l$  by the equation,  $a = d_{meas} \sqrt{h^2 + k^2 + l^2}$ . The average of these calculated lattice parameters was taken as the lattice parameter for each phase in each pattern, and uncertainties were calculated as the standard error of the mean. See Supplementary Data for lattice parameters, and experimental pressures and temperatures (Table S1). The pressure was calculated based on the equation of state of W (Dorogokupets and Oganov, 2007). Although other materials with well calibrated equations of state were included in each experiment (MgO in the MAP experiments; NaCl as the insulator / pressure medium in LHDAC/RHDAC experiments; Pt in room temperature DAC experiments), we found that the most reproducible results were obtained using W as the pressure standard, because it was intimately mixed with the WO<sub>2</sub> sample and at identical P-T conditions, whereas the same may not have been the case for MgO and NaCl. The primary difference in experimental conditions between W and either MgO or NaCl was likely temperature, i.e. slightly different physical location in the presence of a thermal gradient resulted in differences in thermal pressures in the phases. Consideration of the experimental configurations in comparison to the differences in pressures calculated using W and either MgO or NaCl supports this interpretation. For example in the MAP experiments the MgO was separate from but adjacent to the sample chamber, and the W and MgO pressures were largely consistent within uncertainties (~1 GPa). The temperature difference across this distance could have been up to approximately 100 K (Leinenweber et al. 2012), which would contribute to an approximately 0.5 GPa difference in calculated pressure of either W or MgO. The NaCl thermal gradient in the RHDAC experiments, in which the entire cell was heated, was likely less than 100 K, and the W and NaCl pressures were likewise consistent within uncertainties. In contrast, the axial thermal gradient through the NaCl layers in the LHDAC experiments was large with a correspondingly higher level of uncertainty on the

range of temperatures of the NaCl probed by the x-ray beam. In the room-temperature DAC experiments, some of the pressures calculated using Pt and W differed outside of uncertainties, probably because of nonhydrostatic stresses at low temperature.

# **Tungsten dioxide phases**

Both monoclinic and orthorhombic WO<sub>2</sub> phases (ap-WO<sub>2</sub> and hp-WO<sub>2</sub>) have been described in the literature (Bolzan et al. 1995, Sundberg et al. 1994). In the present experiments, both of these phases were observed in addition to a previously unpublished higher pressure and temperature monoclinic phase (hpm-WO<sub>2</sub> as described below). Miller indices were assigned to each identified peak in the patterns and lattice parameters were calculated using nonlinear least-squares minimization of the differences ( $\Delta d$ ) of measured and calculated d-spacings.

In the crystal structures of both the *ap*-WO<sub>2</sub> and *hp*-WO<sub>2</sub> phases, the W atoms occupy one half of the octahedral sites. The *ap*-WO<sub>2</sub> structure is characterized by chains of W octahedra in a distorted rutile type structure. The *hp*-WO<sub>2</sub> structure is characterized as a twinned 1-bar structure (Sundberg et al. 1994). The W-W distances in the *hp*-WO<sub>2</sub> structure are shorter than in the *ap*-WO<sub>2</sub> structure by 0.5 to 0.7 Å. This contributes to the higher density of *hp*-WO<sub>2</sub> and therefore its thermodynamic stability at higher pressure.

The higher pressure monoclinic WO<sub>2</sub> phase (hpm-WO<sub>2</sub>) was discovered during peak indexing of the LHDAC data. Comparison of peaks in the 20 GPa heating cycle were made to the 40 GPa heating cycle and it was apparent that the Pnma-structured hp-WO<sub>2</sub> phase was not present (Sundberg et al. 1994). The major orthorhombic peaks, (111) and (230) that were present in all 20 GPa patterns were absent in the 40 GPa and higher pressure data (Figure 2). Some similarities were observed between the 40, 55 and 70 GPa cycles, though additional peaks were present in the 55 and 70 GPa data suggesting that an additional phase was present at pressures

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greater than 55 GPa. The diffraction pattern from this high pressure WO<sub>2</sub> phase was indexed using the method of successive dichotomy as coded in the DICVOL powder indexing software of Boultif and Louer (2004). To assess the robustness of this method, DICVOL pattern indexing was conducted using the patterns from each of the temperatures in the 20 GPa cooling cycle. All solutions were in the orthorhombic crystal system, and ultimately solutions were obtained for multiple diffraction patterns that were in agreement with the *Pnma* structure of Sundberg et al. (1994). The diffraction spectrum for G33 006 (highest temperature pattern) compared to the 1-bar spectrum calculated using the Sundberg et al. (1994) structure data are shown in Figure 3. See Supplementary Data for lattice parameters, and experimental pressure and temperature conditions (Tables S2, S3 and S4). Patterns from the 40 GPa data were likewise analyzed using DICVOL and all solutions were in the monoclinic system. The best solution was indexed with all  $\Delta d$  values less than 0.004 Å. This structure was in the P2/m space group and is here termed hpm-WO<sub>2</sub> (for high pressure monoclinic) following the convention of Sundberg et al. (1994). The P2/m space group of the hpm-WO<sub>2</sub> phase was the reduced cell form. A preferred space group C2/c was determined using the chekcell software (Laugier and Bochu). Solutions determined using DICVOL for all W-oxide peaks in the 55 and 70 GPa data sets were not equivalent with the hpm-WO<sub>2</sub> of the 40 GPa set. This was likely due to a mixing of peaks from multiple phases. Peak indexing of the hpm-WO<sub>2</sub> phase was based on 16 to 19 peaks in the 55 GPa data and 7 to 12 peaks in the 70 GPa data. The uncertainties on the lattice parameters for the 70 GPa data were approximately twice that of the lattice parameters for the 55 GPa data because of larger  $\Delta d$  values and also fewer indexed peaks in the 70 GPa data. The

285 changes in density between the 40 and 55 GPa, and 55 and 70 GPa sets were approximately 3 286 and 4 percent, respectively, calculated along isotherms at 1000, 1300, 1700, and 2000 K. 287 Attempts were made to index the higher pressure (>40 GPa) data to a monoclinic WO<sub>3</sub> 288 structure (Bouvier et al. 2002), under the hypothesis that WO<sub>2</sub> may have disassociated to WO<sub>3</sub> 289 and metallic W. However, many prominent peaks could not be indexed and the calculated molar 290 volumes were not reasonable in comparison to the results of Bouvier et al. (2002). The proposed 291 orthorhombic unit cell of Dewhurst and Lowther (2001) also does not fit the high-P-T data 292 collected on WO<sub>2</sub>. 293 Under room temperature compression and at approximately 25 GPa, a structural 294 transformation from monoclinic (ap-WO<sub>2</sub>) to the orthorhombic structure of WO<sub>2</sub> was evident. These two structures coexisted for at least 20 GPa, with the monoclinic phase (ap-WO<sub>2</sub>) mostly 295 296 disappearing above approximately 45 GPa. Indexing the room temperature x-ray diffraction data 297 on the orthorhombic phase was not robust when referenced to either the Sundberg et al. (1994) or 298 Dewhurst and Lowther (2001) high pressure structures. Probable explanations include an 299 incomplete phase transition with a mixture of structural states, and structural distortions due to 300 accumulated strain related to room temperature compression. 301 High pressure x-ray diffraction experiments in a resistively-heated DAC conducted up to approximately 42 GPa and at temperatures up to approximately 725 K also showed the 302 303 coexistence of the monoclinic (ap-WO<sub>2</sub>) and orthorhombic (hp-WO<sub>2</sub>) structured phases above 30 304 GPa. In the highest pressure, high-temperature data, the monoclinic and orthorhombic phases 305 appeared to have roughly equal contributions to the x-ray diffraction patterns as gauged by 306 relative peak intensities. At higher temperatures the monoclinic (ap-WO<sub>2</sub>)-to-orthorhombic (hp-WO<sub>2</sub>) transition was 307

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much faster. In our multi anvil press experiments and the lowest-pressure LHDAC experiments (<25 GPa), hp-WO<sub>2</sub> was easily identified. One or two diffraction peaks in the patterns from these experiments could possibly have been attributed to the ap-WO<sub>2</sub> phase, but the relative intensities of these peaks were extremely low. The hp-WO<sub>2</sub> phase was observed at a pressure of approximately 5 GPa and 300 K in the MAP experiments following a high temperature cycle. This suggests that the ap-WO<sub>2</sub> to hp-WO<sub>2</sub> transition has a kinetic barrier at 300 K, but hp-WO<sub>2</sub> is stable to low pressure and temperature conditions. This is also supported by the fact that Sundberg et al. (1994) recovered their hp-WO<sub>2</sub> phase to ambient conditions for x-ray diffraction analysis and crystal structure refinement. We place the phase boundary for the ap-WO<sub>2</sub> to hp-WO<sub>2</sub> transition at 4 GPa (near 400 K). In the 40 GPa data from the LHDAC experiments, the hpm-WO<sub>2</sub> phase replaced the hp-WO<sub>2</sub> phase present in the 20 GPa data. Some of the peaks for hpm-WO<sub>2</sub> were present in the 55 GPa data, though other peaks in these data could not be indexed as hpm-WO<sub>2</sub> and represent a coexisting phase assumed to be another tungsten oxide. The intensity of W diffraction relative to the oxide decreased in this pressure range, suggesting that perhaps the second, non-hpm-WO<sub>2</sub> oxide phase was the result of the reduction of WO<sub>2</sub> and oxidation of W to form a lower valence tungsten oxide, perhaps W<sub>2</sub>O<sub>3</sub> (W<sup>3+</sup>). The intensity of WC diffraction remained nearly constant across the high pressure data. Plots of the highest temperature spectra from the 20, 40, 55 and 70 GPa data are shown in Figure 4, illustrating the changes in the phase complement in the LHDAC experiments. The diffraction spectra show the change in crystal structure observed for WO<sub>2</sub> from *Pnma* to C2/c, the decrease in W relative peak intensities, and the appearance of WC peaks at 40 GPa. The hpm-WO<sub>2</sub> phase was identified in both 29 GPa and 39 GPa diffraction patterns at 300 K (room temperature compression), but was entirely absent in the high temperature data in the 40

GPa range. This places the possible phase boundary between hp-WO<sub>2</sub> and hpm-WO<sub>2</sub> over a range of ~23 to 39 GPa. Lack of high temperature data in this pressure range leads to the simplest choice for the phase boundary at approximately 32 GPa. A phase diagram for W+WO<sub>2</sub> is shown in Figure 5.

During EOS fitting, described in the following section, the robustness of the hpm-WO<sub>2</sub> phase identification in the 70 GPa data was brought into question. The misfit of the 40, 55 and 70 GPa

identification in the 70 GPa data was brought into question. The misfit of the 40, 55 and 70 GPa data were not randomly distributed and showed distinct groupings above and below the zero axis and the RMSE of the fit was approximately 2 GPa. Fit quality improved when not including the 70 GPa data with a reduction of the RMSE to 0.28 GPa. The additional oxide peaks in the 55 GPa data not belonging to the *hpm*-WO<sub>2</sub> phase were likely from another W-oxide phase. This other phase increased in abundance in the 70 GPa data evidenced by the increase in relative abundance of these peaks and a corresponding decrease in the W peaks. These observations may signal an incomplete phase transition in which the *hpm*-WO<sub>2</sub> phase was transforming to yet another WO<sub>2</sub> structure. Assuming this was this case, the decreased number of *hpm*-WO<sub>2</sub> peaks and increased lattice parameter uncertainties at 70 GPa was the result of a mixed-phase state similar to that observed in low temperature compression where coexisting *ap*-WO<sub>2</sub> and *hp*-WO<sub>2</sub> phases resulted in poorer quality lattice parameter fits for these phases. The 70 GPa were not included in the EOS fit for *hpm*-WO<sub>2</sub>.

Finally, the temperatures and pressures of boundaries between the WO<sub>2</sub> phases (P2/c, Pnma, and C2/c) are not well constrained here (only at ~ 4 GPa and 300-500 K for P2/c and Pnma), and could be a focus of future investigations.

### **Tungsten Carbide**

For the LHDAC experiments, tungsten carbide (WC) was present in all x-ray diffraction

spectra at pressures greater than 40 GPa. The source of the carbon to produce WC was likely from the diamond anvils during laser heating, as has been observed previously in laser heated experiments (e.g., Prakapenka et al. 2003). The diffraction peaks had low relative intensity and remained essentially the same intensity across the high pressure data sets. Lattice parameter values and unit-cell volumes are listed in Supplementary Data (Table S5). WC was also observed in diffraction data in the MAP experiments. Unlike the LHDAC experiments, the small WC peaks observed in multi-anvil runs are most likely due to C source in the assembly such as acetone or adhesive, rather than from the WC cubes or graphite x-ray windows in the assembly.

Results and discussion

## **Equations of state**

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Thermal equations of state (EOS) describe the relationship between pressure, temperature, and volume for a given phase. To calculate the WWO fO<sub>2</sub> buffer (see next section), a thermal EOS for each of the observed WO<sub>2</sub> phases and for W was needed. The P-V-T data for each phase were fit to Mie–Grüneisen equations of state,

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$$P = P_{298}(V) + \left(\frac{\gamma}{V}\right) \left[ E(\theta_D, T) - E_{298}(\theta_D, T = 298) \right]$$
 (1)

where the room-temperature pressure component,  $P_{298}$ , is represented by a 3rd order Birch-369 Murnaghan EOS, and is a function of volume only;  $P_{298} = 3K_T f(1+2f)^{5/2}(1+1.5(K_T-4)f)$ , 370 where  $K_T$  is the isothermal bulk modulus,  $K_{T'}$  is the bulk modulus pressure derivative, and the 371 Eulerian strain (f) =  $0.5((V/V_0)^{-2/3} - 1)$  with V = volume and  $V_0 = \text{zero-pressure}$  volume. A 372 Debye model of vibrational energy, E, was used for the thermal pressure component which 373 includes a Grüneisen parameter  $\gamma = \gamma_0 (V/V_0)^q$  and Debye temperature  $\theta_D = \theta_0 exp[\gamma_0/q (1 - e^{-\beta_0})]$ 374  $(V/V_0)^q$ )] (see Figure S1). For hp-WO<sub>2</sub>, the optimal solution is  $K_T = 230$ ,  $\gamma_0 = 1.22$  and q = 2.9375 with  $K_T$ ' = 4 fixed. Fixing  $q=1,\ K_T$ ' = 4, the best fit  $K_T=222$  and the best fit Grüneisen 376

parameter is  $\gamma_0=1.23$ . The difference in the r.m.s. misfits and the errors on the  $K_T$  and  $\gamma_0$  parameters for these two fits are negligible. A fit with all four parameters free to vary resulted  $K_T=226$ ,  $\gamma_0=1.43$ , and q=5.2 and  $K_T$  unconstrained, which may reflect the relatively small pressure range of data containing this phase and an insufficient number of data to properly fit four parameters. For hpm-WO<sub>2</sub>, the optimal solution is  $K_T=304$ ,  $\gamma_0=1.21$  and  $V_0=18.072$  with  $K_T'=4$  and q=1 fixed; a similar fit with free  $K_T'$  resulted in a larger error on Vo and with  $K_T'$  approximately equal to four, and therefore  $K_T'$  was fixed at 4. A fit with all five parameters free to vary resulted identical K and  $\gamma_0$  values,  $V_0=18.080$ , and q and  $K_T'$  unconstrained. Because of the relatively limited temperature range of the data for ap-WO<sub>2</sub>, the overall fit was relatively insensitive to changes of the Grüneisen parameter. Setting  $\gamma_0=1$  or 2 resulted in an increase of approximately 0.1 GPa r.m.s. misfit with the bulk modulus,  $K_T=238$ , unchanged. These optimal equation of state parameters are listed in Table 1 and the equation of state for WO<sub>2</sub> is plotted along isotherms in Figure 6.

The EOS for W was used as the pressure calibration for our data from MAP and DAC experiments ranging 300 to 2250 K, and 2 to 72 GPa. We refitted the EOS of Dorogokupets and Oganov (2007) to a Mie–Grüneisen EOS. The resulting bulk modulus and pressure derivative were 307 ( $\pm 0.40$ ) GPa and 4.05 ( $\pm 0.04$ ) GPa, respectively, which compared well with the values 306 GPa and 4.17 GPa from Dorogokupets and Oganov (2007). The r.m.s. misfit of our refitted equation of state to the Dorogokupets and Oganov (2007) equation state was only 0.04 GPa over the pressure and temperature range of this study. The overall fit was optimized by inclusion of both thermal parameters. Fitting with q = 1 required a change in  $\gamma_0$  of approximately 0.1 and increased the r.m.s. misfit by the same amount. Fixing  $\gamma_0$  = 1.5 and q = 1 increases r.m.s. by approximately 0.1 GPa.

## The W-WO<sub>2</sub> oxygen fugacity buffer (WWO)

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With equations of state for both W and WO<sub>2</sub>, the 1-bar WWO fO<sub>2</sub> buffer (O'Neill and Pownceby 1993) was extended to high pressures, which allowed for calculating the fO<sub>2</sub> at any P or T conditions (Campbell et al. 2009). The Gibbs free energy difference on the WWO buffer is

$$\Delta G_{WWO} = G_{WO_2} - G_W = RT ln f(O_2)$$
 (2)

Given that  $d(\Delta G) = -\Delta S dT + \Delta V dP$  and that dT = 0 along an isotherm,

$$\Delta G_{WWO(P,T)} = \int_{P=1bar}^{P} \Delta V dP + \Delta G_{WWO(P=1bar,T)}^{*}$$
(3)

which shows that the pressure dependence of the WWO buffer is related to the volume difference ( $\Delta V$ ) between W and WO<sub>2</sub>. Combining Equations 2 and 3 gives:

$$\ln f(O_2) = \left(\ln f(O_2)_{1bar} + \int_{P=1bar}^{P} \Delta V dP\right) / RT \tag{4}$$

The WWO buffer was calculated over a pressure range of 1 bar to 70 GPa in 1 GPa increments and over a temperature range of 250 to 2500 K in 250 K increments. The 1-bar values were calculated using the equation of O'Neill and Pownceby (1993),  $fO_2|_{WWO} = -596,087 + 300.5T - 15.97T * ln(T)$ . Calculations above 1700 K were an extrapolation of the O'Neill and Pownceby (1993) data and were necessary for extension of the 1 bar buffer to higher pressures and temperatures. The  $fO_2$  along the WWO buffer was calculated along isotherms for P > 1 bar using Equation 4 to generate a matrix of  $fO_2$  values. The equations of state for W and  $WO_2$  were inverted to determine the required  $\Delta V$  values to solve the integral in Equation 4. Multiple  $WO_2$  phases made it necessary to apply more than one equation of state. At equilibrium and along the ap- $WO_2$ -hp- $WO_2$  and hp- $WO_2$ -hpm- $WO_2$  phase boundaries, the chemical potentials of the coexisting phases are equal, and therefore the integration in Equation 4 was carried across these phase boundaries.

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The calculations described above produced matrices of fO<sub>2</sub> values with isothermal rows and isobaric columns. These data are adequate for plotting curves, but to facilitate rapid calculation of the fO<sub>2</sub> of the WWO buffer at any P-T condition, the tabular (matrix) data were fit to three polynomial expressions, one each for the three WO<sub>2</sub> phases. The polynomial form used was,  $log fO_2/_{WWO} = (A_0 + A_1P) + (B_0 + B_1P + B_2P^2)/T$ . The temperature and pressure ranges of data used for fits. and the  $logfO_2 = (a_0 + a_1P + a_2P^2 + a_3P^3) + (b_0 + b_1P + b_2P^2 + b_3P^3)/T$  fit parameters and the r.m.s. misfit are shown in Table 2. The WWO buffer was calculated along isobars using these expressions and these are plotted as a function of inverse temperature in Figure 7. Data points from the tabular data are plotted as points on Figure 7 to illustrate the quality of the fits. The fO<sub>2</sub> along the WWO buffer is positively correlated with temperature and pressure indicating that the system becomes more oxidizing at higher temperatures and pressures. The calculated logfO<sub>2</sub> values have very small slope change at the phase transitions in WO2, but these are subtle; for example the different between the curves for the intermediate and high pressure WO<sub>2</sub> calculated at 50 GPa and 1073 K is  $\sim 0.5 \log fO_2$  unit. The difference between the WWO and IW (Campbell et al. 2009) buffers is shown in Figure 8. At pressures lower than 40 GPa, the WWO buffer is at a higher fO<sub>2</sub> than the IW buffer. The magnitude of this difference decreases at higher pressures. The significance of this relationship between the WWO and IW buffers is that it predicts the siderophile character of W. The trend of decreasing siderophile character of W shown here suggests that W will trend toward more lithophile character with increasing pressure and therefore increasing depth within the mantle. As discussed in a later section the prediction of W metal-silicate partitioning based on experimental data agrees with this conclusion.

Our new results can be used in high pressure experimentation to constrain oxygen fugacity where a W capsule has been used (e.g. Cottrell et al., 2009). As one can see from our results (Figure 8) there is little difference in IW-WWO buffer change between 1 bar and 2 GPa, so there is no substantial correction to make to the work of Cottrell et al. (2009). However, if W capsules are used at pressures >20 GPa, the fO<sub>2</sub> should be calculated using our new EOS, because use of 1 bar data will result in erroneous fO<sub>2</sub>.

## Application to W metal/silicate partitioning

Following Campbell et al. (2009), the log of the exchange coefficient  $K_D$  for the Fe-W exchange reaction  $2Fe + WO_2 = 2FeO + W$  as a function of the difference between the W-WO<sub>2</sub> and IW fO<sub>2</sub> buffers and the log of the ratio of activity coefficients is

$$logK_D - (logfO_2^{WWO} - logfO_2^{IW}) = log\left[ \left( \gamma_{WO_2}^{sil} / \gamma_W^{met} \right) / \left( \gamma_{FeO}^{sil} / \gamma_{Fe}^{met} \right)^2 \right]$$
 (5)

Using the measured log K<sub>D</sub> values from metal–silicate experiments and the calculated differences between the WWO and IW buffers at the P-T conditions of those experiments to calculate the left hand side, the right hand side can be rearranged as a sum of activity coefficients, which is related to the molar excess Gibbs energy of mixing of the Fe-W exchange reaction,

$$G^{xs} = RT \sum_{i} log(\gamma_i) = RT \left( log \gamma_{WO_2}^{sil} - log \gamma_{W}^{met} - 2 log \gamma_{FeO}^{sil} + 2 log \gamma_{Fe}^{met} \right)$$
. Oxygen fugacity has a strong effect on W metal-silicate partitioning and this is addressed by the calculated difference of the WWO and IW buffers, which also contains most of the non-linear pressure dependence. We modeled the excess Gibbs energy of mixing to the first order with linear compositional, pressure and temperature dependencies

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$$G^{xs} = RT \sum_{i} log (\gamma_i) = (H^{xs} - S^{xs}T + V^{xs}P)/RT + \sum_{i,j} z_i^j X_i^j$$
 (6)

where i is a component in phase j with mole fraction X, and  $H^{xs}$ ,  $S^{xs}$  and  $V^{xs}$  are the excess enthalpy, entropy and volume of mixing, respectively. The pressure dependence in the W, WO<sub>2</sub>, Fe and FeO activity coefficients is contained in the excess molar volume of mixing term,  $V^{xs}$ .

Tungsten metal-silicate partitioning cast in terms of an Fe-W exchange partition coefficient is:

$$\log K_D = [\log f O_2^{WWO} - \log f O_2^{IW}] + [(H^{xs} - S^{xs}T + V^{xs}P)/RT + \sum_{i,j} z_i^j X_i^j]$$
 (7)

The excess Gibbs energy of mixing was fitted for molar metal–silicate exchange partition coefficients that were calculated from literature data (Walter and Thibault, 1995; Hillgren et al., 1996; Ohtani et al., 1997; Righter and Shearer, 2003; Cottrell et al., 2009; Wade et al., 2012) and from unpublished data of Shofner et al. These partition coefficients were obtained from the measured mole fraction abundances of Fe and W in both the metallic and silicate phases. The phase components modeled as contributing to  $G^{xs}$  were SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub> and CaO in the silicate melt, and S in the metallic melt, and the results of this fit are shown in Table 3. It was assumed that the activity coefficients were the same for all WO<sub>2</sub> phases; this may be unlikely, but in the absence of any information otherwise we make this provisional assumption for these calculations.

The metal/silicate partitioning of W using Equation 7 was calculated along the peridotite liquidus, shown as curve B in Figure 9, and along isobars (Figure 10). A regression based on linear dependencies in all parameters is shown for comparison in Figures 9 and 10; the regression equation

$$log K_D = 2.00 - (3180 / T) - (125 P / T) + (0.52 X_C) - (4.27 X_S)$$
 (8)

was fitted to the data and calculated along the peridotite liquidus, where  $X_C$  and  $X_S$  are the mole fractions of carbon and sulfur, respectively, in the metallic Fe. Partitioning along the liquidus curves using Equations 7 and 8 have generally the same trend, with Equation 7 predicting a

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larger decrease in the siderophility of W with increasing pressure. The slope change in curve B at  $\sim 33$  GPa is due to the difference in  $fO_2$  calculated for the higher pressure form of  $WO_2$ . Early work on W partitioning revealed non-ideality in both the metallic and silicate liquids (e.g., S and C content of metal (Jana and Walker, 1997a,b) and degree of polymerization in silicate melt (Walter and Thibault, 1995)), making isolation of pressure effects difficult and perhaps even unlikely. The agreement between our results on the pressure effects for the metal-oxide end member and multi-component systems is perhaps unexpected and therefore worth highlighting here.

Pressure and temperature have competing effects on the metal/silicate partitioning of W. In the previous paragraph we have demonstrated that log K<sub>D</sub> decreases at higher pressures. Yet, calculated along isobars by Equation 7, log K<sub>D</sub> is positively correlated with temperature where the temperature effect is approximately 0.5 log units at 20 GPa, increasing to approximately 2.5 log units at 60 GPa between 2000 and 3000 K (Figure 10). However, in the more naturally realistic case, along the peridotite liquidus where both pressure and temperature vary, pressure exerts the greater effect. A comparison of Equation 7 to other predictive expressions of K<sub>D</sub><sup>W(met-</sup> sil) (Siebert et al. 2011; Wade et al. 2012) is shown in Figure 11. The prediction of Equation 7 (curve B) is similar to that of Siebert et al. (2011) (curve A) at lower pressures but the curves diverge at higher pressures where the separation of the curves increases to 0.7 log units at 60 GPa. Wade et al. (2012) concluded that W metal-silicate partitioning has no significant pressure dependence and this is shown by the essentially flat trend of curve C in Figure 11 across the pressure range of 0 - 60 GPa. This is contrary to the findings of the present study and that of Siebert et al. (2011). Using a predictive expression for log D<sub>W</sub> from Cottrell et al. (2009, 2010) and calculating W metal-silicate partitioning along the peridotite liquidus indicates an increase in the lithophile behavior of W at higher pressures. While the Cottrell et al. (2009, 2010) expression was not in terms of the Fe-W exchange coefficient, it results in the same trend of decreasing W siderophile behavior at higher pressures.

The difference in the prediction of W metal-silicate partitioning by Equation 7 and Siebert et al. (2011) is likely due to different approaches to modeling the pressure dependence of  $fO_2$ , which has a strong influence on W metal-silicate partitioning. This is better characterized by the measure of the volume difference between WWO and IW buffers as opposed to the simple linear approximation of  $\Delta$ IW. The pressure effect on  $fO_2$  is captured by the equations of state underlying the buffers that more precisely represent the volume changes at higher pressures where non-linearity is more pronounced. The pressure dependence of W metal-silicate partitioning is relatively small and therefore the difference between the linear and non-linear (buffer-based) approaches is correspondingly small. However, it is likely that this difference would be higher for other elements, e.g. Ni which has strong pressure dependence (Campbell et al. 2009). Additional partitioning experiments at pressures higher than 30 GPa should also improve the agreement between the two approaches (e.g., Shofner et al., 2014), since the partitioning data is currently limited to pressures < 25 GPa.

530 Implications

Tungsten is a geochemically important element that has bearing on both the process and timing of core formation in the Earth. The effect of the redox state of W on its geochemical behavior at conditions of the deep Earth are crucial for accurate and precise determination of W properties and behavior in core formation and other geochemical modeling. Extension of the 1-bar WWO buffer to high pressures can improve its application in both deep Earth and high pressure experimental applications. High pressure experimentation in this study identified a previously

unknown high-pressure phase of WO<sub>2</sub> that contributes to better understanding of the WWO buffer at high pressure. Applying the WWO buffer to metal-silicate systems can provide improved determination of the non-linear pressure effect on W metal-silicate partitioning, and of the activity of W in both silicate and metallic phases. The ultimate contribution of this work on the WWO buffer will be to improve constraints on Earth core formation models and to allow for the use of the WWO buffer in high pressure experiments by allowing more precise calculation of fO<sub>2</sub>.

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pressure pattern offset in d-spacing by approximately -0.1 Å relative to 1-bar pattern due to 672 673 compression. 674 **Figure 4.** X-ray diffraction spectra from highest temperature pattern at each pressure range. The 675 d-spacing offset between the spectra is due to compression. The 110 and 211 peaks for W are 676 labeled to show the change in relative intensity of W to the other phases in the two highest 677 pressure data sets. Figure 5. Phase diagram for WO<sub>2</sub>. Space group of phases are indicated in italics. The green 678 symbol indicates the pressure and temperature synthesis conditions of the high pressure 679 orthorhombic phase (Pnma) described by Sundberg et al. (1994). Note that the overlap of data 680 681 near the  $P2_1/c$ -Pnma phase boundary is related to the low temperature phase dynamics as discussed in the text. The various phases and space groups of WO<sub>2</sub> are: ap-WO<sub>2</sub> =  $P2_1/c$ ; hp-682  $WO_2 = Pnma$ ; hpm-  $WO_2 = C2/c$ . Color scheme is the same as in Figure 1. 683 Figure 6. PVT EOS for WO<sub>2</sub> plotted along isotherms as a function of pressure. Each phase is 684 685 plotted for the pressure ranges as shown in Figure 5. The various phases and space groups of  $WO_2$  are: ap- $WO_2 = P2_1/c$ ; hp- $WO_2 = Pnma$ ; hpm-  $WO_2 = C2/c$ . 686 Figure 7. Isobaric plot of the absolute fO<sub>2</sub> (log<sub>10</sub>) of the WWO buffer plotted as a function of 687 688 inverse temperature. Curves were calculated using the polynomial expressions in Table 2, and 689 the points are the fitted data from the tabulated values resulting from the extension of the 1-bar WWO buffer to high pressure. 690 691 **Figure 8.** Difference between WWO and IW buffers plotted as isobars as a function of inverse 692 temperature. WWO was calculated using the polynomial expressions in Table 2, and IW was 693 calculated using the Fe-FeO buffer of Campbell et al. (2009). **Figure 9.** The predicted W metal/silicate partitioning in terms of the log<sub>10</sub> of the Fe-W exchange 694

695	coefficient calculated along a peridotite liquidus (Herzberg and Zhang 1996; Zerr et al. 1998).
696	The red curve (B) was calculated using Equation 7, and for comparison, the blue curve (A) was
697	calculated using Equation 8. The slope change in curve B at $\sim$ 33 GPa is due to the difference in
698	fO <sub>2</sub> calculated for the higher pressure form of WO <sub>2</sub> .
699	Figure 10. Isobaric plots of the predicted W metal/silicate partitioning in terms of the log of the
700	Fe-W exchange coefficient. Solid lines were calculated using Equation 7, and dotted lines were
701	calculated using Equation 8.
702	Figure 11. Comparison of $\log K_D^W$ calculated along the peridotite liquidus as predicted by
703	Siebert et al. (2011) (Curve A), Equation 7 (curve B), and Wade et al. (2012) (Curve C). The
704	liquidus is a fit to data from Herzberg and Zhang (1996) and Zerr et al. (1998).

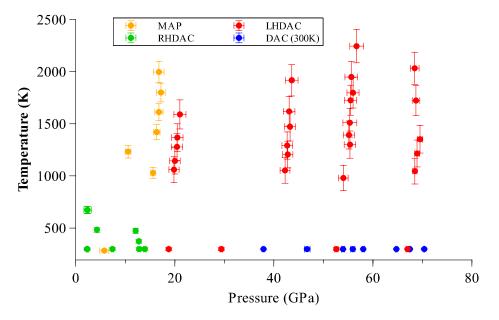


Figure 1

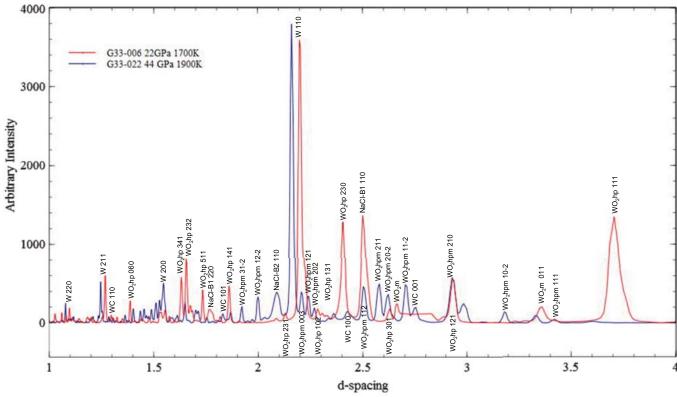


Figure 2

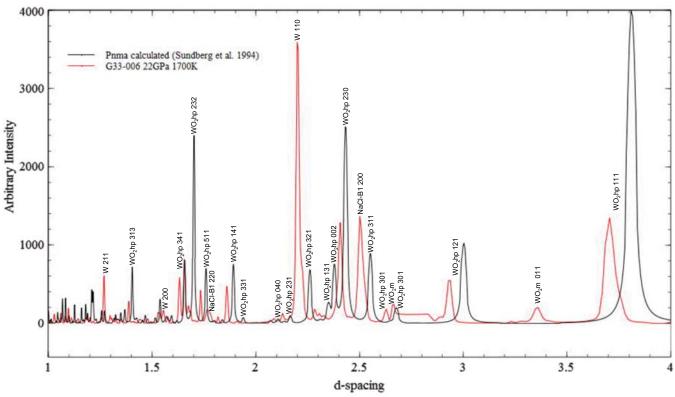
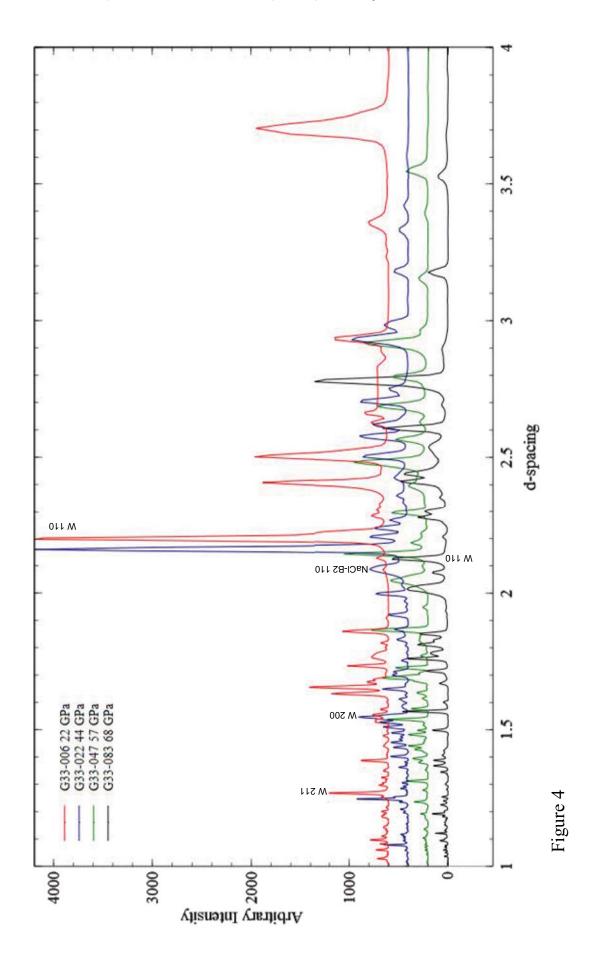


Figure 3



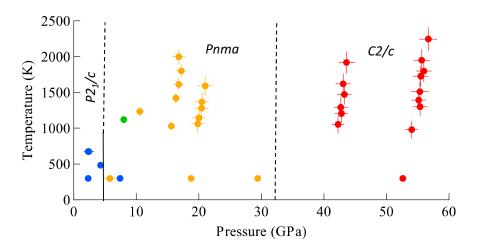


Figure 5

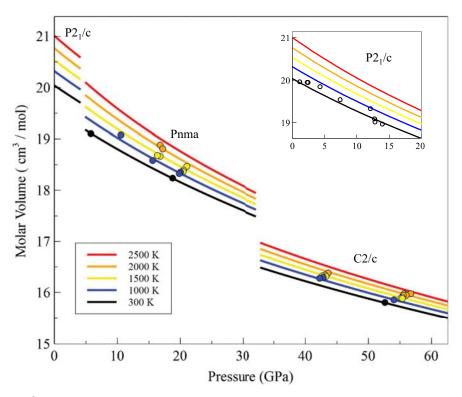


Figure 6

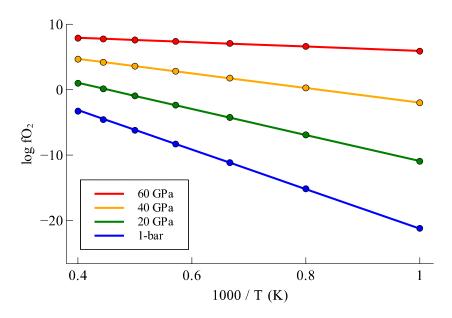


Figure 7

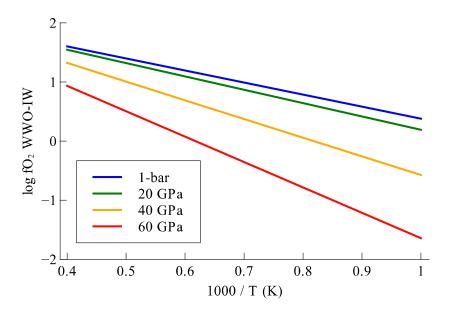


Figure 8

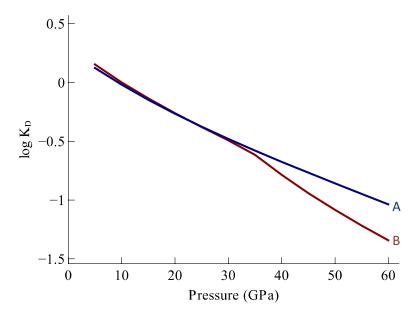


Figure 9

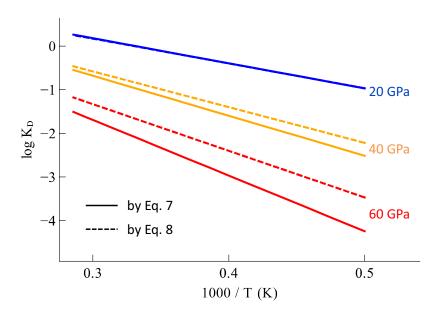


Figure 10

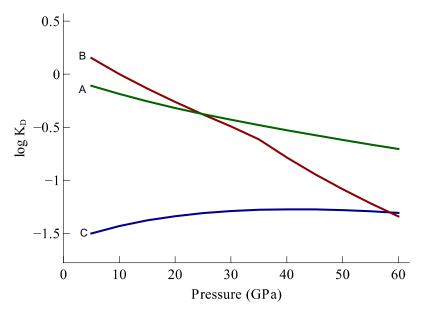


Figure 11

Table 1. Equation of state parameters (Birch-Murnaghan with Grüneisen parameter and Debye temperature). <sup>a</sup>JCPDS card files. <sup>b</sup>Sundberg et al. (1994). <sup>c</sup>Kittel (1996). <sup>d</sup>Goodenough et al. (1984)

	W	ap-WO <sub>2</sub>	hp-WO <sub>2</sub>	hpm-WO <sub>2</sub>
$V_0$ (cm $^3$ /mol)	9.544 <sup>a</sup>	20.037 <sup>a</sup>	19.570 <sup>b</sup>	18.072 ± 0.02
K <sub>T</sub> (GPa)	307 ± 0.40	238 ± 4	230 ± 3	304 ± 3
K <sub>T</sub> ' (GPa)	$4.05 \pm 0.04$	4 (fixed)	4 (fixed)	4 (fixed)
$\theta_D$ (K)	400 <sup>c</sup>	380 ± 15 <sup>d</sup>	380 ± 15 <sup>d</sup>	380 ± 15 <sup>d</sup>
γο	$1.61 \pm 0.03$	1.45 ± 0.18	1.22 ± 0.07	1.21 ± 0.12
q	1.54 ± 0.13	1 (fixed)	2.90 ± 1.5	1 (fixed)
r.m.s. (GPa)	0.04	0.38	0.22	0.14

Table 2. Parameters of polynomial fits of tabulated fO<sub>2</sub> values for  $P2_1/c$ , Pnma, and C2/c WO<sub>2</sub> phases in the high pressure W-WO<sub>2</sub> buffer. log fO<sub>2</sub> |<sub>WWO</sub> = (A<sub>0</sub> + A<sub>1</sub>P) + (B<sub>0</sub> + B<sub>1</sub>P + B<sub>2</sub>P<sup>2</sup>)/T.

WO <sub>2</sub> phase	Parameters			.s.	P range (GPa)	T range (K)
ap-WO <sub>2</sub> (P2 <sub>1</sub> /c)	$A_0$	8.957 B <sub>0</sub>	-30200	0.023	0 - 4	750 - 2000
	$A_1$	0 B <sub>1</sub>	554.2			
		$B_2$	0			
hp-WO <sub>2</sub> (Pnma)	$A_0$	8.860 B <sub>0</sub>	-29947	0.010	5 - 32	1000 - 2250
rip-vvO <sub>2</sub> (i iiiia)	· ·	· ·		0.016	3-32	1000 - 2230
	$A_1$	0.007804 B <sub>1</sub>	524.1			
		$B_2$	-1.178			
hpm-WO <sub>2</sub> (C2/c)	$A_0$	9.000 B <sub>0</sub>	-27954	0.027	33 - 70	1000 - 2250
. 2007	A <sub>1</sub>	0.004493 B <sub>1</sub>	438.8			
		$B_2$	-0.479			

Table 3. Fit parameter for the excess Gibbs energy of mixing in the W-WO2 buffer-based expression of the Fe-W exchange coefficient.

 $-8.27 \pm 1.0$  $-4.49 \pm 0.72$ 

r.m.s.e.

 $7.02 \pm 1.3$ 

zAl<sub>2</sub>O<sub>3</sub> zCaO