Iron and aluminum substitution mechanism in the perovskite phase in the system MgSiO₃-FeAlO₃-MgO

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ABSTRACT

Fe,Al-bearing MgSiO₃ perovskite (bridgmanite) is considered to be the most abundant mineral in Earth's lower mantle, hosting ferric iron in its structure as charge-coupled (Fe₂O₃ and FeAlO₃) and vacancy components (MgFeO_{2.5} and Fe_{2/3}SiO₃). We examined concentrations of ferric iron and aluminum in the perovskite phase as a function of temperature (1700–2300 K) in the MgSiO₃-FeAlO₃-MgO system at 27 GPa using a multi-anvil high-pressure apparatus. We found a LiNbO₃-structured phase in the quenched run product, which was the perovskite phase under high pressures and high temperatures. The perovskite phase coexists with corundum and a phase with (Mg,Fe³⁺, \Box)(Al,Fe³⁺)₂O₄ composition (\Box = vacancy). The FeAlO₃ component in the perovskite phase decreases from 69 to 65 mol% with increasing temperature. The Fe₂O₃ component of Fe_{2/3}SiO₃ in the perovskite phase exists as 1–2 mol% at 1700–2000 K, whereas 1 mol% of the oxygen vacancy component of MgFeO_{2.5} appears at higher temperatures, although the analytical errors prevent definite conclusions. The *A*-site vacancy component might be more important than the oxygen vacancy component for the defect chemistry of bridgmanite in slabs and for average mantle conditions when the FeAlO₃ charge-coupled component is dominant.

Keywords: Bridgmanite, phase transition, multi-anvil press, high pressure, substitution mechanism, lower mantle

INTRODUCTION

MgSiO₃ perovskite (bridgmanite) is the most abundant phase in Earth's lower mantle and incorporates Al and Fe by substituting for Si and Mg. The flexible substitution in bridgmanite produces a wide range of compositional variations depending on pressure-temperature-composition conditions. Although the oxidation state in the lower mantle is considered to be below the iron-wüstite buffer (Frost and McCammon 2008), large amounts of ferric iron are expected in bridgmanite due to charge disproportionation of iron (3 FeO \rightarrow Fe₂O₃ + Fe) when aluminum is present (Lauterbach et al. 2000; Frost et al. 2004; Irifune et al. 2010; Huang et al. 2021).

McCammon et al. (1997) reported an increased ferric iron content with increasing Al in pyroxene diamond inclusions with composition (Mg,Fe,Al)(Si,Al)O₃, considered to be derived from bridgmanite. Lauterbach et al. (2000) experimentally also found a positive correlation between Fe³⁺ and Al. These studies suggest that iron favors the ferric state in bridgmanite by mainly forming the FeAlO₃ charge-coupled component, making it a major component in bridgmanite.

The FeAlO₃ component can significantly affect the properties of bridgmanite. For example, incorporating FeAlO₃ decreases the bulk modulus and increases the density (e.g., Boffa Ballaran et al. 2012) and electrical conductivity (e.g., Yoshino et al. 2016). The FeAlO₃ component also affects Mg-Fe partitioning between bridgmanite and other lower-mantle ferromagnesian minerals in peridotite and basalt (e.g., Frost and Langenhorst 2002; Irifune et al. 2010). Thus, understanding the FeAlO₃ component in bridgmanite is essential to argue the structure and dynamics of the lower mantle.

There are other minor components in bridgmanite. Experiments in the ternary systems of MgO-SiO₂-Al₂O₃ and MgO-SiO₂-Fe₂O₃ demonstrated that the oxygen vacancy components such as MgAlO_{2.5} and MgFeO_{2.5} are included in bridgmanite (Navrotsky et al. 2003; Kojitani et al. 2007; Liu et al. 2017a; Fei et al. 2020; Ishii et al. 2022a). Oxygen vacancy-bearing bridgmanite should be more compressible than stoichiometric bridgmanite. In addition, an *A*-site vacancy component of Fe³⁺_{2/3}SiO₃ has also been suggested, which should be compressible (Ismailova et al. 2017b). The charge-coupled substitution components Al₂O₃ and Fe₂O₃ can also appear (Kubo and Akaogi 2000; Kojitani et al. 2007; Liu et al. 2017b; Fei et al. 2020). Although the Al and Fe³⁺ substitution mechanisms have been individually investigated in Fe- and Al-free systems, respectively, the substitution mechanisms of these components are still unclear in the Fe-, Al-bearing system.

Liu et al. (2020) investigated the chemistry of the perovskite phase in the MgSiO₃-FeSiO₃-Fe₂O₃-Al₂O₃ system at 27 GPa and 2000 K. They observed 65 mol% of FeAlO₃ with a few percent of the oxygen vacancy and *A*-site vacancy components of MgFeO_{2.5} and Fe_{2/3}SiO₃, respectively, using samples with ferrous iron up to 25%. However, the temperature and pressure dependence of the chemistry of the perovskite phase in these systems is still unknown.

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This study investigated the temperature dependence on the chemistry of the perovskite phase in the ferrous iron-free system MgO-MgSiO₃-FeAlO₃ at 27 GPa and 1700–2300 K using a multi-anvil apparatus. Excess MgO was added to explore the substitution mechanism in mantle assemblages with Mg/Si > 1, such as peridotite.

EXPERIMENTAL PROCEDURES

Starting material and high-pressure experiments

A mixture of MgSiO₃ enstatite, Mg_2SiO_4 forsterite, Al_2O_3 corundum, and Fe_2O_3 hematite with mole proportions of 5:20:37.5:37.5, respectively, was used as a starting material. By following Ishii et al. (2018a, 2019a), the enstatite and forsterite samples were synthesized by dissolving Mg metal in a solution of HNO₃ plus pure water, mixing it with tetraethylorthosilicate [(CH₃CH₂O)₄Si] at Mg/Si ratios of 1 and 2 for enstatite and forsterite, respectively, adding ammonia to the solutions, and heating the resulting gels stepwise to 1700 K. Reagent grades of Al_2O_3 and Fe_2O_3 were dried at 773 K for 24 h before weighing.

High pressure-high temperature syntheses were performed at 27 GPa and 1700, 2000, and 2300 K for 2-20 h using IRIS-15, a 15-MN Kawai-type multianvil press with an Osugi-type guide block system installed at the Bayerisches Geoinstitut, University of Bayreuth (Ishii et al. 2016, 2019b). The starting material was packed in a Pt-tube capsule, closed with two Pt lids. To avoid the reduction of Fe³⁺ to Fe²⁺, which was observed by Liu et al. (2020), an IrO₂ oxidizer was also put at the bottom of the capsule, separating it from the sample using a Pt foil. A Cr-doped MgO octahedron with 7 mm edge lengths was used as a pressure medium. A cylindrical LaCrO3 heater was inserted into the center of the octahedron. An MgO sleeve was placed in the heater to insulate the sample capsule from the heater electrically. Sample temperatures were measured at the surface of the capsule using a W97%Re3%-W75%Re25% thermocouple. The ceramic parts of the cell assemblies were kept at 1273 K for more than 3 h in an oven and taken out just before assembling them. The sample was always kept at 427 K in an oven and taken out just before assembling. The truncation size of the inner anvils was 3.0 mm. The sample was first compressed to 2 GPa (0.3 MN) at room temperature and heated to 600 K at a rate of 100 °C/min. These conditions were kept for 1~2 h to purge adhesive water in the sample and cell components. The assembly was then cooled to room temperature, compressed to 27 GPa (13 MN), and heated to the desired temperature at a rate of 100 °C/min. After keeping the target temperature, the sample was quenched by shutting off the electric power supply of the heater and slowly decompressed for 12-15 h.

To estimate a generated pressure of 27 GPa at 13 MN, we employed a pressure dependence of the alumina content in MgSiO₃ bridgmanite coexisting with corundum together with the decomposition pressure of pyrope to bridgmanite plus corundum (Hirose et al. 2001; Liu et al. 2017b) in separate runs. Pressure calibration has been generally performed using phase boundaries of compounds determined by in situ X-ray diffraction in a multi-anvil press. However, there is no such pressure calibrant to cover the present pressure range (>27 GPa) (Ito 2015). Hirose and Fei (2002) calibrated pressures to 27 GPa using Al₂O₃ content in bridgmanite reported by Hirose et al. (2001). Liu et al. (2017b) extended the pressure range to 52 GPa is most reliable for the time being. Our recent study reproduced 27.1(5) GPa at 13 MN using the same calibrant in the same multi-anvil press (Ishii et al. 2022b), supporting the validity of the present way.

Sample characterization

Phases in the recovered samples were identified using a micro-focused X-ray diffractometer (Bruker, D8 DISCOVER) operated at 40 kV and 500 μ A equipped with a two-dimensional solid-state detector (VÅNTEC500) and a micro-focus source (I μ S) of CoK α radiation. Phase compositions were measured using an electron microprobe analyzer (EPMA) with wavelength-dispersive spectrometers (JEOL, JXA-8200), operated at an accelerating voltage and probe current of 15 kV and 15 nA, respectively. The standards for Mg and Si, Al, and Fe were natural enstatite, synthetic corundum, and synthetic hematite, respectively. Sample textures were observed using a field-emission-type scanning electron (BSE) imaging and an energy-dispersive X-ray spectrometer (Oxford X-Max^N).

Iron valence ratios in the recovered samples were determined by Mössbauer spectroscopy. The recovered samples were polished to 150 μ m thickness. Mössbauer spectra were obtained at room temperature (293 K) in transmission mode

on a constant acceleration Mössbauer spectrometer with a nominal 370 MBq ⁵⁷Co high specific activity source in a 12 µm thick Rh matrix (McCammon et al. 1991; McCammon 1994). The velocities in all spectra were calibrated using a reference spectrum of a 25 µm thick α -Fe foil certified by National Bureau of Standards (now referred to as the National Institute of Standards and Technology, standard reference material no. 1541) at room temperature. Spectra were collected for 1–2 days and fitted with the full transmission integral using MossA software (Prescher et al. 2012).

RESULTS AND DISCUSSION

Tables 1 and 2 summarize experimental conditions, phases present, and chemical compositions of each sample. Figure 1 illustrates the room-temperature Mössbauer spectrum of the sample synthesized at 27 GPa and 2000 K. The hyperfine parameters for Mössbauer spectra of the bulk recovered samples obtained by fitting are also summarized in Table 1. Figures 2 and 3, respectively, show a representative X-ray diffraction (XRD) pattern and backscattered electron (BSE) images of the recovered samples. We applied heating durations of 2–20 h at 1700–2300 K, in which the sample annealed at 2300 K employed only 2 h (Table 1). Many phase-relation studies on multi-component systems such as pyrolite and basaltic crust compositions by multi-anvil press showed chemically homogeneous phases at 2000–2300 K even heated for 2 h or less (Ono et al. 2001; Hirose and Fei 2002; Ishii et al. 2011, 2012,

 TABLE 1.
 Experimental conditions, phase assemblages, and chemical compositions of recovered bridgmanite

		· · · J	
Run no.	I-1003	I-969	I-991
Т (К)	1700	1700 2000	
Heating duration (h)	20	13	2
Phases	LN+Crn+PS	LN+Crn+PS	LN+Crn+PS
n	8 9		12
Composition (wt%)			
MgO	9.44(37)	9.95(30)	10.91(38)
SiO ₂	14.74(62)	15.62(50)	15.59(47)
Al ₂ O ₃	29.05(58)	28.40(35)	27.18(61)
Fe ₂ O ₃	47.61(82)	46.32(65)	45.21(73)
Total	100.85(130)	100.26(122)	98.89(148)
Composition (pfu) (O = 2	3)		
Mg	0.284(9)	0.300(6)	0.333(9)
Si	0.298(14)	0.315(8)	0.319(6)
Al	0.691(6)	0.676(5)	0.656(9)
Fe	0.723(8)	0.704(10)	0.697(12)
Cation total	1.996(7)	1.995(3)	2.005(4)
Mole fraction			
MgSiO₃	28(1)	30(1)	32(1)
FeAlO₃	69(1)	68(1)	65(1)
Fe ₂ O ₃	1.2(9)	0.9(11)	1.3(18)
Fe ³⁺ _{2/3} SiO ₃	1.4(1.7)	1.6(10)	N
MgFeO _{2.5}	N	N	1.4(11)
Fe ³⁺ /ΣFe	100(5)	100(3)	100(5)
Hyperfine parameters			
CS for Fe ³⁺	0.33(1)	0.319(5) ^a	0.32(1)
QS for Fe ³⁺	0.92(2)	0.895(5)	0.92(2)
FWHM	0.48(4)	0.36(2)	0.47(4)

Notes: LN = LiNbO₃-type phase; Crn = corundum; PS = $A^{2+}B_2^{3+}O_4$ post-spinel phase; N = not observed; *n* = number of analyzed points; CS = center shift relative to α -Fe (mm/s); QS = quadrupole splitting (mm/s); FWHM = full-width at half maximum (mm/s). Numbers in parentheses for chemical composition data indicate one standard deviations of the mean in the analyses. Mole fractions of each component were calculated as follows (also see the text):

1. All Al is combined with corresponding amount of Fe^{3*} to form the FeAlO_3 component.

2. The A-site vacancy, corresponding to 1/3 of the A-site, is used to allocate Fe and Si to the $Fe_{2^{+}_{3}}^{2}SiO_{3}$ component.

3. The O-vacancy corresponding to 0.5 of the MgFe³⁺O₂₅ component forms the basis for the allocation of Fe and Mg.

4. The rest of Fe is allocated to the Fe_2O_3 component.

5. The rest of Mg and Si is allocated to the MgSiO₃ component.

^a Broad, weak magnetic Fe^{3+} component with CS = 0.1(1) mm/s was also observed in the fitting (see Fig. 1).

Post-spinel phase, I-1003 (27 GPa, 1700 K), <i>n</i> = 9							
Oxide wt%	MgO	SiO ₂	AI_2O_3	Fe_2O_3	Total		
	21.32(31)	0.86(22)	29.93(52)	45.69(35)	97.81(46)		
Cation number $(O = 4)$	Mg	Si	Al	Fe ³⁺	Total		
	0.921(13)	0.025(6)	1.022(15)	0.996(10)	2.965(5)		
Post-spinel phase, I-969 (27 GPa, 2000 K), n = 8							
Oxide wt%	MaO	SiO	Al ₂ O ₂	Fe ₂ O ₂	Total		
	22.73(38)	0.75(4)	30.39(60)	45.05(48)	98.93(73)		
Cation number $(O = 4)$	Mg	Si	A	Fe ³⁺	Cation		
. ,	0.968(9)	0.022(1)	1.024(14)	0.969(15)	2.982(3)		
Corundum, I-969 (27 GPa, 2000 K), n = 6							
Ovido ut%	MaO		41.0	Fa ()	Total		
Oxide wt%	MgU 4 20(10)	510 ₂ 6 10(27)	AI ₂ O ₃	14 90(56)	10(d)		
Cation number $(0 - 2)$	4.20(10) Ma	0.19(27) Ci	/ 3.04(30) Al	Eo ³⁺	Gation		
Cation number (0 – 3)	0 113(3)	0 112(5)	1 574(12)	0 201(7)	2 000(1)		
	0.115(5)	0.112(3)	1.374(12)	0.201(7)	2.000(1)		
Post-spinel phase, I-991 (27 GPa, 2300 K), <i>n</i> = 8							
Oxide wt%	MqO	SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	Total		
	21.19(18)	1.64(9)	30.44(41)	44.48(41)	97.75(55)		
Cation number $(O = 4)$	Mg	Si	Al	Fe ³⁺	Cation		
	0.910(1)	0.047(2)	1.033(11)	0.964(5)	2.954(3)		
Corundum, I-991 (27 GPa, 2300 K), <i>n</i> = 6							
Oxide wt%	MaO	SiO	Al ₂ O ₂	Fe ₂ O ₂	Total		
	3.73(4)	5.24(17)	74.27(77)	14.49(32)	97.72(92)		
Cation number $(O = 3)$	Ma	Si	Al	Fe ³⁺	Cation		
	0.102(1)	0.096(3)	1.604(4)	0.200(3)	2.002(1)		
Note: $n =$ number of analyzed points. Numbers in parentheses indicate one standard deviations of the mean in the analyses.							

Chemical compositions of recovered post-spinel phases



FIGURE 1. Room-temperature Mössbauer spectrum of the recovered sample synthesized at 27 GPa and 2000 K. The red-shaded area is assigned to non-magnetic Fe^{3+} . The gray shaded area is assigned to weakly magnetic Fe^{3+} . Spectra of samples quenched from 1700 and 2300 K contain only non-magnetic Fe^{3+} . (Color online.)

2018b, 2019c, 2022b). In fact, the well-crystallized texture and homogeneous chemical compositions of the recovered phases (Tables 1 and 2; Fig. 3) suggest reaching equilibrium in the present heating durations at the pressure-temperature conditions used.



FIGURE 2. X-ray diffraction pattern of the recovered sample synthesized at 27 GPa and 2000 K. Stars indicate possible peaks of $(Mg,Al,Fe^{3+})O_4$ post-spinel phase (see text). LN = lithium niobate phase. (Color online.)



FIGURE 3. Backscattered electron images of recovered samples at 27 GPa and 1700–2300 K. White grains are platinum from the platinum capsule after polishing. LN = lithium niobate phase; Crn = corundum; $PS = (Mg,Al,Fe^{3+})O_4$ post-spinel phase.

Ferric iron contents

Mössbauer spectra of the bulk recovered samples can be fitted to one doublet, although one broad peak was also detected only on sample I-969 (Fig. 1). The hyperfine parameters of the center shift and quadrupole splitting are 0.32-0.33 mm/s and 0.90-0.93 mm/s, respectively, which are in good agreement with those of Fe³⁺ in bridgmanite and the LiNbO₃-structured phases (Fei et al. 1994; McCammon et al. 2004; Hummer and Fei 2012; Liu et al. 2020; Huang et al. 2021). The broad peak of sample I-969 can be assigned to a weakly magnetic Fe³⁺ component. All observed peaks were thus assigned to Fe³⁺, showing Fe³⁺/ Σ Fe = 100% in all samples.

Phase identification

Most XRD peaks were assigned to a LiNbO₃-structured phase (Fig. 2), known as a back-transformed phase from a

TABLE 2.

and corundum

perovskite phase (Leinenweber et al. 1991; Akaogi et al. 2017; Ishii et al. 2017a; Liu et al. 2020). Liu et al. (2020) reported that the MgSiO₃-bearing perovskite phase with more than 40% of FeAlO₃ was recovered as a lithium-niobate phase at ambient conditions. Therefore, the chemistry of the LiNbO₃-structured phase should represent that of the perovskite-structured phase under high pressure-temperature conditions. Hereafter, we refer to this phase as the perovskite phase when discussing the crystal chemistry at high pressure and high temperature.

The BSE images showed three phases with different textures and contrasts in addition to the LiNbO3-structured phase. One is a Mg,Al,Fe-rich phase with grain-crack texture. Its main components are MgAl₂O₄ and MgFe₂O₄, implying that this phase may be one of the $A^{2+}B_2^{3+}O_4$ orthorhombic phases, so-called post-spinel (PS) phases, which have an octahedral framework and a trigonal prism site (Ishii et al. 2018c). These phases are difficult to identify because they have similar crystal structures but different atomic distributions (Ishii et al. 2020). The XRD peaks not belonging to the LiNbO3-structured phase can be assigned to a PS phase (Fig. 2). However, the XRD patterns do not clearly indicate which PS phase produces the few observed peaks. Nevertheless, these peaks can be assigned to the CaTi₂O₄-type phase, which was recently discovered in various AB2O4 compositions (Funamori et al. 1998; Bindi et al. 2014; Ishii et al. 2014, 2015, 2021). We refer to this phase as a PS phase hereafter. The BSE images also indicate limited amounts (~1.5-3 vol%) of an Al-rich phase, which was identified as corundum because this phase can be regarded as an Al₂O₃-MgSiO₃-Fe₂O₃ solid solution. However, XRD patterns indicated no corundum peaks, probably due to the limited intensities. The detailed compositions of these phases are discussed below.

Compositions of the perovskite phase

The component fractions in the $ABO_{3\pm\delta}$ perovskite phase were estimated using EPMA and Mössbauer data based on the following assumptions: (1) Al and Fe³⁺ produce the most charge-coupled component of FeAIO₃. The remaining trivalent cations are referred to as *T*. (2) When the cation-oxygen ratio is smaller than 2:3, the *A*-site cation-vacancy component $T_{2/3}SIO_3$ is considered. When greater, the oxygen vacancy component MgTO_{2.5} is considered. (3) The remaining *T* produces the charge-coupled component *TTO*₃. (4) The remaining Mg²⁺ and Si⁴⁺ produce the MgSiO₃ component.

Figure 4 shows the changes in components of the perovskite phase with temperature obtained by the above procedure. Fe³⁺ and Al3+ ions dominate, resulting in the dominant component FeAlO₃. This component slightly decreases with increasing temperature from 69 to 65 mol%. The second major component is MgSiO₃, which increases with increasing temperature from 28 to 32 mol%. Thus, the perovskite phase in the present system can be approximated by a MgSiO₃-FeAlO₃ solid solution. Liu et al. (2020) reported that the perovskite phase synthesized at 27 GPa and 2000 K in the MgSiO₃-FeSiO₃-Fe₂O₃-Al₂O₃ system without excess MgO has 63–65 mol% of the FeAlO₃ component. These values are slightly smaller than the present study (67 mol% at 2000 K), probably because Fe³⁺ in their perovskite phase (11–15%) was slightly reduced to Fe²⁺ to form some Fe²⁺SiO₃ components. We observed $1 \sim 2 \mod \%$ of the A-site vacancy component of $Fe_{2/3}^{3+}SiO_3$ at lower temperatures of 1700 and 2000 K, whereas 1 mol% of



FIGURE 4. Solubility of MgSiO₃, FeAlO₃, Fe₂O₃, Fe₂O₃, and MgFeO_{2.5} components in the perovskite-structured phase at 27 GPa as a function of temperature. (Color online.)

the oxygen vacancy component MgFeO_{2.5} was found at 2300 K. Although this change is within the analytical errors, the dominant vacancy component might change with temperature. In addition, we observed small amounts, only 1 mol%, of the charge-coupled component Fe_2O_3 in all perovskite phases, which showed no temperature dependence.

Compositions of the associated phases

As mentioned above, we found two phases associated with the LiNbO₃-structured phase, i.e., the PS phase and corundum. The primary composition of the PS phase can be expressed as MgAl₂O₄-MgFe₂O₄. However, there are extra ferric irons. Such extra Fe³⁺ should produce an *A*-site vacancy component Fe_{2/3}Fe₂O₄ because the total cation number is <3 for four oxygen atoms. This component is the third most abundant, representing 5–13 mol% of the phase. This phase also has a minor component of Mg₂SiO₄ (2–5 mol%) because of the small amounts of SiO₂ (0.8–1.6 wt%). The limited Si contents are typical in PS-related oxides, supporting the phase identification as a PS phase (Ishii et al. 2017b, 2018d; Akaogi et al. 2018; Uenver-Thiele et al. 2018). Thus, the compositions of the PS phase can be expressed as (Mg,Fe³⁺, \Box)(Al,Fe)₂O₄ (\Box = vacancy), and is almost independent of the temperature.

The composition of corundum is expressed as Al_2O_3 -MgSiO₃-Fe₂O₃, as mentioned above. There appears to be almost no temperature dependence, although composition at 1700 K is unknown due to the exceedingly small grain sizes ($\leq 1 \mu$ m) for EPMA analysis. The Al₂O₃, MgSiO₃, and Fe₂O₃ contents are 80, 10, and 10 mol%, respectively.

Reaction controlling the chemistry of the perovskite phase

The present system essentially has four chemical components: MgO, Fe₂O₃, Al₂O₃, and SiO₂. On the other hand, the number of phases is three: perovskite phase, an $A^{2+}B_2^{3+}O_4$ PS phase, and corundum. Therefore, the present system has one degree of freedom at a given pressure and temperature, which would be the partitioning of the FeAlO₃ charge-coupled component because Al₂O₃ and Fe₂O₃ are strongly coupled in the perovskite phase in the present system.

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The resulting equilibrium reaction may be:

$$FeAlO_3 (perovskite phase) + Mg_2SiO_4 (PS) = MgFeAlO_4 (PS) + MgSiO_3 (perovskite phase)$$
(1)

The coincident decrease and increase in FeAlO₃ and MgSiO₃ components, respectively, with temperature (Fig. 4) suggest that the entropy change with this reaction is slightly positive.

IMPLICATIONS

The oxygen-vacancy components MgAlO_{2.5} and MgFeO_{2.5} have been proposed to exist in bridgmanite in the systems MgO-SiO₂-Al₂O₃ and MgO-SiO₂-Fe₂O₃, respectively (Liu et al. 2017a; Fei et al. 2020). The oxygen vacancy components should increase compressibility. Also, they possibly reduce the creep strength of bridgmanite, suggesting a viscosity contrast compared with the mantle containing stoichiometric bridgmanite (Liu et al. 2017a; Reali et al. 2019). Our study demonstrates that the vacancy component changes from *A*-site cation vacancy to oxygen vacancy with increasing temperature. Thus, the oxygen vacancy components are expected to be present in high-temperature regions such as plumes (White and McKenzie 1995). On the other hand, our results also suggest that the *A*-site cation vacancy should be more stable in relatively low-temperature regions such as subducted slabs.

These vacancy components should dominate in shallower regions of the lower mantle, namely the mid-mantle, due to their low density (Liu et al. 2017a). Although the proportions of vacancy components are small, percent-order vacancies should be enough to soften mineral strength (Reali et al. 2019). Therefore, the vacancy components would soften the mid-mantle to enhance mantle dynamics and geochemical circulation. Slab penetration and stagnation in the mid-mantle (Fukao and Obayashi 2013) and plumes becoming invisible by seismic tomography (French and Romanowicz 2015) may reflect the lower viscosity of the mid-mantle compared to deeper regions.

Vacancy in bridgmanite may also play an important role in incorporating water as OH groups in its crystal structure, which has significant importance for the geochemical evolution of the mantle. The oxygen vacancy component of MgAlO_{2.5} may accommodate water based on the following reaction: MgAlO_{2.5} + $\frac{1}{2}H_2O \rightarrow MgAlHO_3$ (e.g., Navrotsky 1999). The oxygen vacancy component of MgFe³⁺O_{2.5} would allow the incorporation of water in the same manner. The *A*-site vacancy component of Fe³⁺_{2/3}SiO₃ might also have the capability to include water based on the following reaction: Fe³⁺_{2/3}SiO₃ + $\frac{1}{3}H_2O \rightarrow Fe^{3+}_{2/3}(OH)_{1/3}SiO_3H_{1/3}$. Thus, both vacancy components may be potential hosts for water in the lower mantle.

However, the pressure dependence of the vacancy components has not been investigated. Such a study requires a wide pressure range, which is impossible using conventional multianvil technology. On the other hand, no percent-order vacancy components can be detected by diamond anvil experiments due to relatively large chemical heterogeneity. Therefore, future experiments will focus on exploring the pressure dependence of vacancy concentrations to provide better constraints on their influence on lower mantle dynamics. Our ultrahigh-pressure multi-anvil technology (Ishii et al. 2016, 2017c, 2019b, 2022b)

provides the best possibility to investigate pressure dependence, and we will tackle this task in the next study.

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