

## The structure of a strained intermediate microcline in cryptoperthitic association with twinned plagioclase

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### Abstract

The crystal structure of a strained intermediate microcline ( $a = 8.643$ ,  $b = 12.929$ ,  $c = 7.190\text{ \AA}$ ;  $\alpha = 90.1^\circ$ ,  $\beta = 116.2^\circ$ ,  $\gamma = 89.6^\circ$ ;  $V = 720.6\text{ \AA}^3$ ;  $C\bar{1}$ ), intergrown as untwinned lamellae in a cryptoperthitic ternary feldspar of bulk composition  $\text{Or}_{33}\text{Ab}_{58}\text{An}_8\text{Cn}_1$ , has been refined to  $R = 0.049$  using 893 reflections. The cryptoperthite is specimen K-235 from the Kungnåt syenites of SW Greenland. Unit-cell volume gives the best estimate of the composition of the microcline phase,  $\text{Or}_9\text{Ab}_6\text{Cn}_3$ , which constitutes  $\sim 36$  percent of the bulk feldspar. The plagioclase composition, determined by mass balance, is approximately  $\text{Ab}_{77}\text{An}_{13}$ .

The plagioclase is twinned at a scale of 100–500 $\text{\AA}$  on both albite- and pericline-twin laws, and special caution was required to exclude from the refinement diffracted peaks from the microcline lattice which overlapped with diffracted peaks from these four plagioclase lattices. In spite of the non-continuous, lamellar nature of the microcline phase in the cryptoperthite, the mosaic texture resulted in only  $0.4^\circ 2\theta$  diffraction peak widths.

Due to its intergrowth with twinned plagioclase, the microcline is strained ( $\Delta a = 0.30\text{ \AA}$ ) in the manner described by Stewart and Wright (1974). This apparently does not prohibit the use of  $b-c$  and  $\alpha^*-\gamma^*$  plots to estimate Al/Si distribution in the tetrahedral sites ( $t_{1o} \sim 0.51$ ,  $t_{1m} \sim 0.35$ ,  $t_{2o} = t_{2m} \sim 0.07$  Al); mean T-O distances ( $T_{1O} = 1.671$ ,  $T_{1m} = 1.651$ ,  $T_{2O} = 1.622$ ,  $T_{2m} = 1.627\text{ \AA}$ ) give similar values (0.47, 0.32, and 0.10 Al, respectively). Without a meaningful basis of comparison, the effects of strain on individual bond lengths and angles could not be evaluated quantitatively.

### Introduction

In the past decade it has been shown that alkali feldspars,  $(\text{K},\text{Na})\text{AlSi}_3\text{O}_8$ , can be characterized most satisfactorily by their lattice parameters. Wright and Stewart (1968) proposed a plot of the  $b$  and  $c$  cell edges (see Fig. 1) "because on such a graph points for samples of different composition but equivalent Al-Si order fall into more or less linear arrays regardless of the symmetry of the starting material" (Stewart, 1975). Samples of the same composition but different Al-Si order (e.g., the maximum microcline-high sanidine series) are arrayed on subparallel lines running between the limiting arrays for the completely ordered maximum microcline-low albite series and the disordered high sanidine-analbite (or high albite) series. Using data from crystal structure analyses, Stewart and Ribbe (1969) determined that relative position on the  $b-c$  plot very closely approximates the

total aluminum content of the  $T_1$  tetrahedral sites, which are designated  $T_{1O}$  and  $T_{1m}$  in triclinic alkali feldspars. Adopting the convention introduced by Kroll (1971), in which  $t_{1o}$  represents the probability of finding aluminum in  $T_{1O}$ , they contoured the  $b-c$  quadrilateral with lines of equal Al content in the  $T_1$  sites: thus  $t_{1o} + t_{1m} = 1.00$  for the ordered series in which all the Al in the formula unit is concentrated in the  $T_{1O}$  site and Si occupies the other three sites (i.e.,  $t_{1o} = 1.00$ ;  $t_{1m} = t_{2o} = t_{2m} = 0.00$ ), and  $t_{1o} + t_{1m} = 0.50$  for the disordered series in which Al is randomly distributed over the four tetrahedral sites (i.e.,  $t_{1o} = t_{1m} = t_{2o} = t_{2m} = 0.25$ ).

Using data from homogeneous alkali feldspars, Stewart and Wright (1974) contoured the  $b-c$  plot for the  $a$  cell dimension, estimating a standard error for the contours of  $\pm 0.02\text{ \AA}$ . They discussed in considerable detail a phenomenon which is especially common in cryptoperthitic intergrowths of two feldspar

Table 5. Ribbe (1978). Structure factors for K-235 microcline

H	K	L	Y(OBS)	Y(CALC)	SIG(0)					
-10	0	5	34.737	32.47	3.43	-7	5	22.9124	22.41	3.15
-10	2	3	5.2145	7.08	10.31	-7	5	14.5090	15.53	3.62
-10	2	5	19.1200	16.67	3.54	-7	4	23.7506	23.63	2.81
-10	0	3	35.2464	32.86	3.01	-7	3	80.8015	80.84	4.29
-10	0	2	32.9997	32.87	3.08	-7	1	41.6632	39.56	2.88
-9	1	6	3.4582	1.15	15.11	-7	0	13.2000	12.17	4.00
-9	1	5	6.4433	5.41	7.12	-7	-2	29.2136	26.97	2.77
-9	1	4	48.6269	49.54	3.23	-7	5	13.9925	17.52	4.45
-9	1	3	10.8601	13.66	5.01	-7	4	16.5554	16.10	3.79
-9	1	2	3.4757	10.61	15.22	-7	3	23.4613	26.96	3.89
-9	1	1	13.0558	10.83	4.56	-7	7	14.1049	15.09	4.18
-9	1	0	23.2670	23.83	3.85	-7	7	29.3027	25.35	4.63
-9	3	6	5.4755	1.38	10.27	-7	9	6.8392	16.02	9.32
-9	3	5	2.2084	0.25	21.65	-7	9	59.3149	58.81	3.59
-9	3	4	20.2570	18.61	3.10	-7	9	29.3790	29.70	2.88
-9	3	3	39.5326	40.69	3.08	-7	2	7.0500	2.96	6.34
-9	3	2	10.7546	10.90	4.83	-7	1	3.1495	9.25	16.73
-9	3	1	53.9540	51.93	3.45	-7	0	20.3627	22.43	3.91
-9	5	5	19.2452	20.63	5.07	-7	1	49.4606	47.85	3.34
-9	5	4	40.5434	40.65	3.30	-7	1	9.0886	13.64	6.96
-9	5	3	11.8973	6.89	4.32	-6	2	8.3577	5.55	6.46
-9	5	2	21.0954	18.59	3.00	-6	1	34.5563	31.73	3.05
-9	5	1	20.9898	20.76	3.13	-6	0	10.9215	8.58	5.10
-9	7	4	38.3313	36.13	3.10	-6	1	23.4061	22.33	3.03
-9	7	3	19.8194	19.71	3.42	-6	0	6.4543	6.88	7.72
-8	8	5	2.7271	3.40	18.91	-6	1	15.1823	12.76	3.69
-8	8	4	30.9108	28.75	2.95	-6	0	28.0560	29.09	3.14
-8	8	3	37.4211	35.64	3.00	-6	1	44.4905	45.37	3.09
-8	8	2	24.0487	21.74	3.05	-6	0	6.9997	4.47	6.74
-8	6	6	12.7091	10.79	4.36	-6	1	55.5626	55.70	3.36
-8	6	5	37.4123	35.88	2.92	-6	0	22.9070	20.93	2.75
-8	6	4	21.7051	20.61	3.28	-6	1	22.8450	23.83	3.01
-8	4	5	39.5918	39.68	2.98	-6	0	23.5324	20.77	2.97
-8	4	4	19.9246	22.96	3.29	-6	1	81.5124	77.52	4.41
-8	4	3	23.2713	20.21	3.36	-6	0	37.2213	36.62	3.03
-8	4	2	17.5197	19.45	3.54	-6	1	67.4395	68.96	3.77
-8	4	1	59.4878	55.01	3.56	-6	1	Y(OBS)	Y(CALC)	SIG(0)
-8	2	7	21.3823	18.29	2.97	-6	1	33.3224	35.54	3.13
-8	2	6	21.0114	18.47	2.95	-6	0	37.3046	37.07	3.24
-8	2	5	40.7420	39.84	2.92	-6	1	7.7896	8.06	5.37
-8	2	4	11.3321	8.41	3.97	-6	0	46.7337	46.40	3.51
-8	2	3	34.5888	36.37	2.92	-6	1	22.6974	21.43	2.84
-8	2	2	31.9927	32.96	2.82	-6	0	12.1103	12.32	4.69
-8	2	1	9.1948	8.21	5.17	-6	1	16.3038	16.26	3.34
-8	2	0	17.4411	19.27	3.70	-6	0	25.6456	23.85	2.66
-8	0	7	9.4990	5.86	5.10	-6	1	32.2687	31.90	2.63
-8	0	6	43.1918	40.58	2.99	-6	0	17.2727	18.29	2.99
-8	0	5	49.4072	49.71	3.18	-6	1	26.2175	28.48	2.68
-8	0	4	31.9254	32.00	2.79	-6	0	70.9557	72.92	3.86
-8	0	3	34.0937	35.22	3.51	-6	1	56.9975	58.45	3.38
-7	1	8	25.4376	21.94	3.02	-6	1	23.8358	21.92	2.77
-7	1	7	Y(OBS)	Y(CALC)	SIG(0)	-6	1	16.4582	16.85	3.66
-7	1	6	23.0434	24.17	3.23	-6	2	21.4491	19.51	3.36
-7	1	5	34.1457	31.27	2.69	-6	2	33.5606	33.38	2.90
-7	1	4	10.3071	10.11	4.65	-6	2	30.1822	30.62	2.80
-7	1	3	38.3408	38.85	2.80	-6	2	27.2924	27.60	2.62
-7	1	2	19.9794	20.44	2.83	-6	2	39.0420	38.64	2.63
-7	1	1	27.2826	28.55	2.60	-6	1	57.3211	60.42	3.37
-7	1	0	65.3549	64.95	3.68	-6	2	28.3583	29.64	2.67
-7	1	-1	8.4209	7.70	5.37	-6	2	42.2276	45.83	3.29
-7	1	-2	19.3069	16.32	3.02	-6	2	26.1963	27.26	3.07
-7	1	-3	10.5514	5.61	4.69	-6	2	21.1651	22.13	3.11
-7	3	7	49.2615	46.86	3.17	-6	2	57.4363	60.79	3.35
-7	3	5	28.5916	25.48	2.64	-6	2	91.0144	93.59	4.65
-7	3	4	32.4914	32.56	2.65	-6	2	38.2843	33.53	3.61
-7	3	3	56.5229	57.21	3.31	-6	2	131.3284	133.79	6.45
-7	3	2	47.1508	46.38	2.96	-6	2	50.0013	51.07	3.02
-7	3	1	29.4341	30.34	2.75	-6	2	36.9254	37.85	2.74
-7	3	0	47.4235	47.36	3.09	-6	2	19.2753	20.34	3.02
-7	3	-2	30.7020	30.69	2.98	-5	2	8.6751	8.61	5.43
-7	5	7	19.3988	16.84	3.36	-5	1	58.4824	60.03	3.40

Table 5. Ribbe (1978). Structure factors for K-235 microcline

			H	K	L	Y(OBS)	Y(CALC)	SIG(0)
-5	1	5	55.7452	58.30	3.23	-4	90.7910	91.8900
-5	1	4	61.1363	63.12	3.39	-4	36.1702	35.9341
-5	1	1	39.7299	38.77	2.58	-4	50.2393	50.2749
-5	1	1	43.2303	45.56	2.69	-4	41.1007	41.8997
-5	1	1	18.5420	18.65	2.49	-4	18.8771	20.6568
-5	1	1	8.9803	8.68	4.04	-4	15.7790	16.7784
-5	1	1	19.7395	20.97	2.89	-4	9.6506	12.1632
-5	1	1	44.9299	43.83	3.09	-4	21.4984	21.7246
-5	1	1	7.9855	1.83	6.21	-4	13.9547	15.0316
-5	1	1	9.1975	2.69	4.64	-4	53.7676	52.3555
-5	1	1	58.6410	72.40	3.75	-4	7.9325	7.6768
-5	1	1	12.2029	10.64	3.36	-4	99.4450	98.2437
-5	1	1	90.2368	92.25	4.59	-4	51.1327	50.4789
-5	1	1	4.1012	3.82	7.83	-4	28.1074	29.3642
-5	1	1	23.3882	23.69	2.64	-4	37.5708	38.0166
-5	1	1	65.3087	67.25	3.62	-4	18.0252	18.2299
-5	1	1	58.7501	61.58	3.34	-4	25.0461	23.3723
-5	1	1	33.9765	34.03	2.61	-4	2.2661	0.0676
-5	1	1	42.5675	43.06	2.90	-4	29.8872	28.5163
-5	1	1	29.9815	31.62	2.91	-4	20.8251	25.7801
-5	1	1	13.4013	12.02	4.34	-4	58.4580	62.1699
-5	1	1	Y(OBS)	Y(CALC)	SIG(0)	-4	4.9835	4.4504
-5	1	1				-4	43.4927	42.0681
-5	1	1				-4	69.9230	72.2728
-5	1	1				-1	33.7840	33.9100
-5	1	1				-3	81.9482	82.1885
-5	1	1				-5	43.4819	41.1540
-5	1	1				8	10.5766	9.7019
-5	1	1				7	26.9367	25.8405
-5	1	1				5	12.8498	12.5495
-5	1	1				4	52.4375	54.2263
-5	1	1				3	74.3254	77.3920
-5	1	1				2	36.2008	36.2612
-5	1	1				1	36.8446	93.0827
-5	1	1				0	14.4903	13.6146
-5	1	1				-1	21.7660	22.3001
-5	1	1				-2	12.8746	14.1337
-5	1	1				-3	31.7642	33.5029
-5	1	1				-4	35.1419	34.5163
-5	1	1				7	59.4224	60.4777
-5	1	1				5	77.6785	81.3626
-5	1	1				4	86.7413	85.7372
-5	1	1				3	61.6663	63.6047
-5	1	1				2	37.5813	40.3157
-5	1	1				1	11.0306	8.8418
-5	1	1				0	22.7292	21.2319
-5	1	1				-1	6.3331	4.5197
-5	1	1				-3	67.8050	69.3412
-5	1	1				-5	27.8147	29.6305
-5	1	1				8	14.6590	14.0644
-5	1	1				7	14.3800	14.2055
-5	1	1				6	81.0528	86.3285
-5	1	1				5	24.5036	24.1386
-5	1	1				4	61.7065	62.4153
-5	1	1				3	39.5632	39.5216
-5	1	1				2	Y(OBS)	Y(CALC)
-5	1	1				1		SIG(0)
-5	1	1				0		
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-3	5	2	15.4248	14.46	2.52						
-3	5	1	53.4723	50.54	2.96						
-3	5	0	57.1299	51.60	3.10						
-3	5	-1	85.9285	85.97	4.38						
-3	5	-2	32.6455	32.86	2.51						
-3	5	-3	54.2781	56.51	3.20	-2	4	1	120.2482	119.77	5.86
-3	5	-4	37.3709	40.23	3.29	-2	4	-1	74.3709	72.55	3.82
-3	5	-5	6.8266	1.02	6.70	-2	4	-2	55.9954	55.80	3.12
-3	7	7	23.2959	24.33	3.24	-2	4	-3	102.1176	107.49	5.13
-3	7	6	47.1304	45.85	3.10	-2	H	L	Y(OBS)	Y(CALC)	SIG(0)
-3	7	5	25.2983	26.90	2.85		K				
-3	7	3	13.2051	14.04	3.49			-4	18.0602	18.55	2.83
-3	7	2	22.9211	23.43	2.45	-2	4	-5	28.5098	29.79	2.70
-3	7	1	20.5678	20.54	2.40	-2	4	-6	12.4618	11.61	4.16
-3	7	0	21.9064	21.24	2.36	-2	4	8	16.8817	17.48	4.38
-3	7	-1	21.3389	20.17	2.50	-2	7		13.2064	8.80	4.05
-3	7	-2	35.3540	32.96	2.65	-2	3		20.9312	22.05	2.15
-3	7	-3	30.3773	30.23	2.70	-2	2		44.3540	46.20	2.63
-3	7	-4	29.8820	29.17	2.78	-2	1		42.3704	40.87	2.38
-3	7	-5	20.9539	22.01	3.51	-2		-1	32.1099	31.17	2.23
-3	9	6	48.5711	50.19	3.87	-2		-2	85.8577	87.02	4.38
-3	9	5	52.5903	54.44	3.27	-2		-3	40.7243	41.60	2.62
-3	9	4	10.6752	5.36	4.21	-1		-5	19.1557	18.47	3.04
-3	9	3	28.2401	28.52	4.14	-2		7	12.0995	12.22	4.24
-3	9	2	60.9324	61.19	3.48	-2		6	56.5807	55.68	3.31
-3	9	-1	4.9299	7.34	8.55	-2		5	37.2671	37.68	2.61
-3	9	-2	22.0160	23.23	2.99	-2		4	176.4303	182.11	8.50
-3	9	-3	18.9766	20.49	3.64	-2		3	6.9311	11.54	4.13
-3	9	-4	44.9811	47.32	3.13	-2			40.6890	42.27	2.28
11	11	5	37.5732	38.42	3.04	-2		-1	13.6684	12.78	2.27
-3	11	4	6.8594	5.01	7.31	-2		-2	54.2919	56.53	3.00
-3	11	3	41.2370	42.34	3.00	-2		-3	37.1032	35.87	2.48
-3	11	2	48.2406	47.77	3.09	-2		-4	82.5485	84.59	4.32
-3	11	1	16.4995	17.43	3.51	-2		-5	33.7272	33.62	2.78
H	K	L	Y(OBS)	Y(CALC)	SIG(0)			-6	51.3922	49.40	3.25
-3	11	0	49.8457	52.78	4.07	-1		7	32.6831	31.84	2.91
-3	11	-1	27.1599	28.55	3.00	-1		6	38.7385	39.53	2.80
-3	11	-2	31.7802	34.67	2.88	-1		5	47.6783	45.06	2.92
-3	11	-3	34.3690	35.98	3.11	-1		4	28.6246	28.07	2.27
-3	13	4	20.0571	21.69	3.67	-1		3	57.2100	53.13	3.08
-3	13	3	19.6843	19.18	3.47	-1		2	99.1184	96.98	4.85
-3	13	2	42.7023	47.07	3.16	-1		1	26.7288	27.02	1.72
-3	13	1	14.1667	15.72	4.32	-1		0	13.6498	15.43	2.14
-3	13	0	24.5088	23.66	3.18	-1		-1	54.1332	52.13	2.81
-3	13	-1	36.8110	36.47	2.96	-1		-3	68.0401	69.43	3.58
-3	13	-2	21.8045	20.10	3.10	-1		-4	67.3727	69.43	3.63
-2	14	3	43.5822	44.16	3.48	-1		-5	29.6604	29.80	2.61
-2	14	2	37.6867	39.10	3.14	-1		-6	4.9573	5.53	9.22
-2	14	1	40.4655	38.06	3.07	-1		-7	7.4336	6.61	6.61
-2	14	0	26.4368	28.58	3.49	-1		7	30.6264	29.77	3.68
-2	12	3	9.0240	12.95	7.02	-1		6	14.8739	15.87	3.68
-2	12	2	2.3481	0.58	21.60	-1		5	92.5119	92.90	4.74
-2	12	1	38.9185	36.18	2.88	-1		4	34.0312	31.16	2.37
-2	12	0	11.3077	11.41	4.72	-1		3	20.4988	21.50	2.32
-2	12	-1	27.6589	28.99	3.15	-1		2	87.0103	78.95	4.34
-2	10	5	28.4497	27.42	2.94	-1		1	55.7197	52.12	2.91
-2	10	4	59.6083	59.02	3.49	-1		-1	132.1071	127.86	6.39
-2	10	3	44.6718	45.87	3.00	-1		-2	14.7237	12.28	2.32
-2	10	2	23.8960	23.53	2.81	-1		-3	42.7955	42.79	2.64
-2	10	1	29.8627	32.40	2.73	-1		-4	43.0305	44.00	2.81
-2	10	-4	24.7538	30.07	3.97	-1		-5	3.1142	1.61	12.90
-2	8	7	38.2019	38.98	3.16	-1		-6	11.4810	13.41	4.94
-2	8	6	12.3763	10.92	4.34	-1		-7	5.0055	4.69	10.33
-2	8	5	32.9532	33.42	2.80	-1		7	19.9476	20.91	3.48
-2	8	4	22.3144	22.52	2.87	-1		5	37.5895	34.98	2.71
-2	8	3	26.9374	26.95	2.61	-1	H	4	32.3882	32.39	2.55
-2	8	2	38.2435	38.31	2.65	-1		L	Y(OBS)	Y(CALC)	SIG(0)
-2	8	1	32.9205	34.06	2.51	-1			7.4925	0.79	4.53
-2	8	0	172.6884	165.89	8.35	-1			56.0314	56.35	3.06
-2	-1	11.4391	8.95	3.29	-1			43.3103	45.41	2.58	
-2	-2	137.5939	142.78	6.76	-1			36.0044	34.64	2.41	
-2	-3	16.6319	16.10	2.98	-1			31.3764	30.24	2.40	
-2	-4	15.2058	15.02	3.43	-1			9.2634	8.17	4.27	
-2	6	7	39.8018	38.33	3.14	-1		-4	82.8529	84.26	4.38
-2	6	6	14.7844	19.43	4.42	-1		-5	20.4516	23.74	3.54
-2	6	5	49.0281	48.81	3.06	-1		6	8.4987	4.60	5.64
-2	6	4	12.6587	13.17	3.27	-1		5	8.8602	8.86	4.99
-2	6	3	24.9058	25.70	2.23	-1		4	56.2005	56.33	3.23
-2	6	2	35.7545	38.38	2.67	-1		3	55.0017	53.39	3.12
-2	6	-3	34.4097	35.63	2.80	-1		2	16.0488	10.18	2.77
-2	4	7	41.6832	41.27	3.03	-1		1	22.0310	22.59	2.55
-2	4	6	6.1153	6.49	7.31	-1		-1	14.0842	13.65	3.00
-2	4	5	45.8723	45.79	2.86	-1		-2	26.6655	26.46	2.57
-2	4	4	29.7953	25.40	2.32	-1		-3	37.7156	39.33	2.79
-2	4	3	5.2665	3.05	5.84	-1		-4	15.0044	11.85	3.50
-2	4	2	7.0567	3.39	4.21	-1		-5			

Table 5. Ribbe (1978). Structure factors for K-235 microcline.

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3	18.8380	18.57	3.04						
32	36.7274	36.60	2.70						
6	26.9400	25.59	2.55						
6	53.0303	51.58	3.08						
6	98.3003	96.99	4.95						
6	57.9909	57.29	3.27						
6	9.6572	8.61	4.57						
6	26.6607	27.55	2.62						
6	9.6734	5.52	4.46						
6	11.5145	16.30	5.22						
6	39.3525	37.39	3.03						
6	82.3749	81.75	4.34						
6	41.3785	43.77	2.91						
2	40.7297	41.54	2.68						
2	13.5223	12.41	2.62						
2	86.3079	88.01	4.38						
2	39.1961	37.67	2.49						
2	76.9637	77.81	4.00						
2	60.5226	62.15	3.38	H	K	L	Y(OBS)	Y(CALC)	SIG(0)
2	7.9905	11.15	5.30						
0	121.2924	120.64	5.97						
-3	93.4137	85.73	4.63						
-7	9.1912	7.69	3.98						
-3	41.3285	39.85	2.89						
-3	100.4601	95.56	5.00						
-1	46.7261	46.04	2.96						
-1	60.2397	59.98	3.36						
-1	57.1756	56.93	3.22						
-1	23.9476	23.67	2.73						
-4	45.5526	45.40	2.93						
-2	16.9662	17.23	2.81						
-4	34.9227	35.19	2.66						
-5	29.5827	29.20	2.72						
-5	36.3673	36.40	2.92						
-5	8.9088	8.48	5.75						
0	67.8785	67.86	3.80						
-1	7.5327	12.14	6.35						
-2	60.3120	62.58	3.47						
-3	14.7449	13.15	3.30						
-4	16.0712	15.95	3.63						
-6	51.5480	51.70	3.35						
11	28.1807	27.17	3.22						
H	Y(OBS)	Y(CALC)	SIG(0)						
11	20.7655	20.21	3.37						
11	13.6682	12.27	4.56						
11	36.4055	36.15	2.85						
11	13.6737	13.26	4.07						
11	18.1346	17.29	3.53						
13	6.5757	8.52	8.68						
13	51.0448	51.68	3.35						
6	37.2653	33.70	2.91						
6	5.2388	8.53	10.36						
6	17.0778	15.90	3.56						
6	22.9565	24.55	3.14						
6	16.9114	19.51	4.01						
6	14.9998	11.17	3.75						
8	56.7606	57.78	3.40						
8	12.6579	11.76	3.85						
8	25.9313	23.62	2.91						
8	53.6003	55.05	3.46						
6	11.8460	11.44	7.24						
6	16.9920	22.69	4.49						
6	14.5195	15.73	3.69						
6	41.2657	42.91	3.51						
6	5.7908	5.98	7.12						
6	38.4349	47.84	3.81						
6	30.8845	31.04	3.40						
6	35.5571	35.57	2.89						
6	21.1581	20.70	2.96						
6	71.2978	72.79	3.83						
6	27.9496	28.32	2.55						
6	16.3659	15.51	2.93						
6	41.6354	42.01	3.15						
6	30.9063	31.83	2.66						
6	60.1861	64.23	3.49						
6	37.7116	37.48	2.62						
6	29.8751	29.29	2.65						
6	28.2453	28.63	2.85						
6	30.8728	34.04	2.97						
6	17.9145	17.12	3.62						
6	14.9597	12.13	3.81						
6	18.6679	20.34	3.11						
6	38.3916	37.85	2.71						
6	74.1252	81.78	4.76						
6	48.8542	51.07	3.02						
6	131.0964	133.79	6.44						