2	Dislocation microstructures in simple-shear-deformed wadsleyite at transition-zone
3	conditions: Weak-beam dark-field TEM characterization of dislocations on the (010) plane.
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11	ABSTRACT
12	Dislocation microstructures of an (010)[001]-textured wadsleyite have been investigated in
13	weak-beam dark-field imaging in a transmission electron microscope. 1/2<101> partial
14	dislocations on the (010) plane are characterized with [100] dislocations on the (001) plane and
15	$1/2 < 111$ > dislocations forming {011} slip bands. The partial dislocations are extended on the
16	(010) stacking fault as a glide configuration (i.e., Shockley-type stacking faults with 1/2<101>
17	displacement vector). The [001] slip on the (010) plane occurs by glide of the dissociated
18	dislocations, which can play an important role in the generation of the crystallographic preferred-
19	orientation patterns reported in water-poor deformation conditions. The glide mechanism on the
20	(010) plane leave the oxygen sub-lattice unaffected, but changes the cation distribution, forming
21	a defective stacking sequence of the magnesium cations in the process of dislocation gliding. The
22	mechanism might be related to transformation plasticity and related effects, such as
23	transformation-enhanced weakening and deep-focus earthquakes in the mantle transition zone.

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25 Keywords: wadsleyite, slip systems, slip plane, Burgers vector, Shockley-type extended
26 dislocation, Frank's rule, Chalmers-Martius criterion

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INTRODUCTION

Enigmatic [001] glide on the (010) plane; i.e., the [001](010) slip system, in deformed 29 wadsleyite has been recently deduced from crystallographic preferred orientation (CPO) patterns 30 obtained by deformation experiments (Demouchy et al. 2011; Kawazoe et al. 2013; Ohuchi et al. 31 2014). In their studies, wadsleyite aggregate was deformed at pressure-temperature conditions 32 characteristic of the mantle transition zone, and a [001](010)-textured CPO pattern was found 33 34 from electron backscatter diffraction (EBSD) measurement on recovered samples. The CPO pattern is primarily controlled by the easiest slip system. In the case of olivine, a polymorph of 35 wadsleyite, deformation fabrics are well correlated with the dominant slip systems (Karato et al. 36 37 2008). Therefore, activation of the [001](010) slip system is simply expected in deformed wadsleyite. Identification of the easiest slip system in wadsleyite is important in understanding 38 39 the physical mechanisms of its plastic deformation (Tommasi et al. 2004) and, in turn, for interpretation of seismic anisotropy observed in the mantle transition zone (Foley and Long 40 2011; Yuan and Beghein 2013). 41

However, real activation of the [001](010) slip system has not yet been confirmed clearly by dislocation microstructures in conventional bright-field and dark-field transmission electron microscopy (TEM) (Cordier 2002). TEM observations in the early 1980s were made on wadsleyite that had been naturally deformed in shocked meteorites (Price et al. 1982; Madon and Poirier 1983; Price 1983). The (010) stacking faults were found in the deformed wadsleyite, and

a topotaxial transformation from ringwoodite to wadsleyite was suggested to occur by a 47 martensitic shear mechanism. In addition, wadsleyite was experimentally deformed in a Kawai-48 49 type multianvil apparatus (Sharp et al. 1994; Thurel and Cordier 2003a; Thurel et al. 2003b). Subsequent TEM characterization of recovered samples revealed activation of the following slip 50 systems: [100](010), [100](001), $[100]\{011\}$, $[100]\{021\}$, $1/2 < 111 > \{101\}$, [010](001), 51 $[010]{101}$ and <101>(010). Wadslevite was also deformed at 14-20 GPa and 1690-2100 K 52 using a rotational Drickamer apparatus (Hustoft et al. 2013; Kawazoe et al. 2010a; Farla et al. 53 2015). However, the [001](010) slip system could not be determined by TEM because the 54 dislocation density was too high to apply the invisibility criterion using conventional bright and 55 dark field TEM imaging. 56

57 The (010) stacking fault is a characteristic microstructure in deformed wadsleyite having the (010)[001]-textured CPO (Demouchy et al. 2011; Ohuchi et al. 2014). Previous studies have 58 discussed that Shockley-type (010) stacking faults can be formed through the glide of 1/2<101> 59 60 partial dislocations on the (010) plane (e.g., Price 1983; Sharp et al. 1994). Based on their theoretical study on crystal chemistry and anisotropic linear elasticity of wadsleyite, Thurel et al. 61 (2003c) reported a possible dissociation along [001] = 1/2[-101] + 1/2[101]. They recommended 62 further detailed investigation on the precise core structure of the dislocations in wadsleyite to 63 better understand and model the plastic behavior of wadsleyite. In this context, Metsue et al. 64 (2010) concluded that, from their calculation of the generalized stacking faults energies on the 65 (010) plane, [001] shear is only possible in (010) where the dislocations dissociate into two non-66 collinear partial dislocations of b = 1/2 < 101 >, i.e., 1/2[-101] and 1/2[101]. Also, as mentioned in 67 68 Demouchy et al. (2011), viscoplastic self-consistent (VPSC) modeling of CPO evolution using the previously reported glide systems for wadsleyite, i.e., $[100]{0kl}$ and $1/2 < 111 > \{101\}$, cannot 69

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reproduce the measured CPO pattern, unless the [001](010) system is also activated. However,
they could not confirm such dislocations by TEM. Therefore, we have re-examined a deformed
wadsleyite with the [001](010) fabric by using weak-beam dark-field (WBDF) TEM imaging.

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EXPERIMENTAL METHOD

75 **Deformation experiment**

76 The simple-shear deformation experiment on a wadsleyite aggregate was performed to a strain γ of 0.4 at a strain rate of 3 \times 10⁻⁵ s⁻¹ at 18 GPa and 1800 K with a deformation-DIA 77 apparatus (run M0180 in Kawazoe et al. 2013). Tungsten carbide anvils with a 3-mm truncation 78 were adopted to reach the target pressure (Kawazoe et al., 2010b). The starting material was a 79 80 single crystal of San Carlos olivine that had been transformed to polycrystalline wadsleyite at 18 81 GPa and high temperature. Grain size and water content of a recovered sample were evaluated as 2.8 µm and 134 wt ppm H₂O, respectively. Further experimental details of the experiment were 82 described in Kawazoe et al. (2013). For comparison, an undeformed wadsleyite (run M0187) in 83 84 the same series experiment was also observed.

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TEM sample and the procedure of the sample preparation

The recovered wadsleyite sample from the deformation experiment was Ar-ion milled to electron transparency at an accelerating voltage of 6 kV and then finally thinned at 2–4 kV with an incident angle of 4-5 degree using an ion slicer (JEOL EM-09100IS) and coated with amorphous carbon for transmission electron microscopy. WBDF-TEM imaging was performed in a field emission transmission electron microscope, Philips CM20FEG, operated at 200 kV. The WBDF-

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TEM images are recorded by using slow-scan CCD camera (Gatan 698) and KODAK SO-160TEM negative films.

94 The Burgers vectors of the dislocations were characterized based on the conventional invisibility criterion method: $\mathbf{g}.\mathbf{b} = 0$ and $\mathbf{g}.(\mathbf{b} \times \mathbf{u}) = 0$, where \mathbf{g}, \mathbf{b} and \mathbf{u} are the diffraction 95 96 vector, the Burgers vector, and the unit vector along the dislocation line, respectively. In addition, 97 the thickness contour fringe method (Ishida et al. 1980; Miyajima and Walte 2009) was used for confirmation of a particular Burgers vector, e.g. 1/2<101>, from possible candidates by 98 constraining the magnitude of the Burgers vector. The number *n* of terminating thickness contour 99 fringes at the extremity of a free dislocation was counted in the WBDF images and applied to the 100 relation $\mathbf{g} \cdot \mathbf{b} = n$. 101

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TEM OBSERVATION AND THE RESULTS

The typical dislocation structures are displayed in Figure 1. The long screw segment of [100] 104 105 dislocations are visible in a WBDF TEM image along the [001] zone axis direction, which is likely to indicate a strong lattice friction (see detail in the discussion) along the [100] zone axis 106 107 and less mobility of the screw segment than the edge one (Thurel and Cordier 2003). A few orthogonal dislocation lines belong to 1/2 < 111 > type dislocations (Fig. 1a). In the other grain 108 109 observed along the [100] zone axis, the dislocation arrays, i.e. slip bands, are parallel to the projection of the (0-11) plane and consist of 1/2 < 111 > perfect dislocations that have dissociated 110 into some partial dislocations at the tens of nanometer scale (Fig. 1b). The configuration of the 111 dislocation bands is consistent with the $1/2 < 111 > \{101\}$ slip system. 112

113 One of the most important characters to explain the (010)[001] fabric is that a high 114 density of dislocations parallel to both the [101] and [-101] directions are visible in WBDF

images with $\mathbf{g} = 400$ and $\mathbf{g} = 004$, while one of those two dislocations is invisible systematically 115 with $\mathbf{g} = 404$ and -404, respectively observed along the [010] zone axis (Fig. 2 and S1). The 116 117 dislocation lines are also most likely to be on the (010) plane, not on the {101} planes, because of their long projection lengths on the plane and because no oscillation contrast exists along the 118 lines which indicate that the dislocation lines are not strongly inclined in the [010]-oriented TEM 119 foil (about 200 nm thickness on the middle of the image) but almost parallel to the foil. Also, two 120 121 thickness contour fringes are terminated at the extremity of the dislocation in the WBDF images with $\mathbf{g} = 004$ (indicated by white arrowheads in Fig. 3). From the number (*n*) of terminating 122 thickness fringes at the extremity of a dislocation from a wedge-shaped thin-foil specimen 123 124 (Ishida et al. 1980; Miyajima and Walte 2009), we can determine that its vector product of \mathbf{g}_{004} 125 and the Burgers vector, **b** of the dislocations is two, consistent with $\mathbf{b} = 1/2 [uv1]$. Moreover, WBDF-TEM images with diffraction vectors, $\mathbf{g} = -211$ and $\mathbf{g} = 013$, i.e. two 126

independent diffraction vectors to the (010) plane, display Shockley-type extended dislocations with $\mathbf{b} = 1/2 <101>$ on the end of their associated stacking faults with fringe contrast on the (010) plane along the [101] direction (Fig. 4 and S2). The stacking fault energy of the (010) stacking fault is likely to be low because of the wide distance between partial dislocations.

From all the results obtained from the WBDF images, we conclude that [001] dislocations in the deformed wadsleyite are dissociated to a pair of screw-character 1/2 < 101> dislocations on the

133 (010) plane; i.e.
$$\mathbf{b} = 1/2[101]$$
 and $\mathbf{b} = 1/2[-101]$

134 The partial dislocations glide in the (010) plane.

135 For comparison, typical microstructures of the (010) stacking fault in an undeformed

- sample (M0187 in Kawazoe eta l. 2013) are also shown in the WBDF images with g = -2-1-1
- and 0-80 (Fig. 5). Stacking faults with partial dislocations at the ends are not well aligned along a

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potential macroscopic strain direction, and a number of ledges exist on the stacking faults (Fig.
S4, Supplementary Material). The microstructures are in contrast to a glide configuration in
Figure 4b. The density of stacking faults in individual grains is also much less than that of
deformed sample, M0180 (Figs. 4b and S3) and most grains do not contain stacking faults and
dislocations (e.g., Fig. 4d in Kawazoe et al. 2013).

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DISCUSSION

A [001] slip on the (010) plane has previously been predicted from the enigmatic CPO 145 pattern in deformed wadsleyite. In this study, we have intensively studied wadsleyite grains 146 along the [010] and [100] zone axes, from which we could directly investigate the $\langle u0w \rangle$ and 147 148 <0vw> type dislocations on the (010) plane and the (100) plane, respectively. In the WBDF-TEM images, a high density of 1/2 < 101 partial screw dislocations and screw-dominant [100] 149 dislocations are co-activated on the (010) plane (Figs. 2, 3 and S1). Herein we confirmed that a 150 151 pair of partial dislocations with Shockley-type stacking fault on the (010) plane are a glide configuration, which can contribute bulk strain in the simple-shear deformation and result in the 152 153 development of the (010)[001]-textured CPO pattern in wadsleyite. The configurations of the 154 straight dislocation lines of both dislocations with $\mathbf{b} = 1/2 < 101 >$ and [100] also indicate a high Peierls stress, lying in potential valleys on the slip planes (Poirier 2000). Note that co-activation 155 of the (010)[100] slip system cannot be neglected, wadsleyite CPO was affected and thus its 156 pattern had slightly deviated from the ideal (010)[001]-textured CPO, with a small maximum of 157 the [100] axis in the CPO pattern of the M0180 sample (Fig. 6a of Kawazoe et al. 2013). 158

The (010) stacking faults have been frequently observed in synthetic and natural wadsleyite from high pressure experiments and shocked meteorites (Madon and Poirier 1983;

Price 1983; Price et al. 1982), respectively. As well, some of wadslevite grains in a non-161 deformed sample, M0187 in Kawazoe et al. (2013) display the stacking faults which are not a 162 glide configuration. However, few previous studies on the wadsleyite have insisted on the 163 potential of [001] slip by the glide of dissociated dislocations producing Shockley-type stacking 164 faults on the basis of theoretical viewpoints of the Frank Criterion (e.g., Sharp et al. 1994) and 165 of a dislocation core model based on the *Peierls-Nabarro-Galerkin* model (Metsue et al. 2010, 166 also see Supplementary Material). As Demouchy et al. (2011) reported based on their VPSC 167 approach, unless the [001](010) system is activated, contributions from only the previously 168 reported $[100]{0kl}$ and $1/2 < 111 > \{101\}$ system cannot reproduce the unique CPO in which the 169 [100] and [001] axes are preferentially sub-parallel to the shear direction and the [010] axes 170 171 concentrate in the direction of the shear-plane normal (e.g., Fig. 10B in Demouchy et al. 2011). Therefore, the glide of 1/2 < 101 partial dislocations on the (010) plane, which were 172 characterized in this study, is a major requisite for the deformation mechanisms in the 173 174 (010)[001]-textured wadsleyite. The dissociation of a [001] perfect dislocation into two noncollinear partial dislocations of 1/2[-101] and 1/2[101] is consistent with their theoretical model 175 by Metsue et al. 2010. The [001] slip on the (010) plane occurs by glide of the dissociated 176 dislocations, which can reasonably explain the reported CPO pattern (Demouchy et al. 2011; 177 Kawazoe et al. 2013; Ohuchi et al. 2014). 178

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IMPLICATIONS

We clearly bridge a gap between the bulk fabric and dislocation microstructures in the deformed wadsleyite displaying the enigmatic (010)[001] fabric. The slip in the [001] direction on the (010) plane by the activation of 1/2<101> partial dislocations is likely to play an important role

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184	in the previous studies of deformed wadsleyite. The deformation mechanisms on the (010) plane
185	of wadsleyite might be an alternative explanation of transformation-enhanced weakening (Price
186	1983) and deep-focus earthquake in the mantle transition zone (Rubie and Brearley 1994). Just
187	because, At the atomic scale, the stacking faults on the (010) plane is not due to a rearrangement
188	on the closest packing plane of oxygens, i.e. {101} and {021} planes (Smyth et al. 2012), but
189	due to a defective stacking sequence of the magnesium cations in the process of dislocation
190	gliding (see Supplementary Material) and also during the olivine-wadsleyite transformation
191	under a deviatric stress (Fujino and Irifune, 1992).
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194	We thank P. Cordier for constructive discussion on dislocation microstructures and providing a
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	was drawn with software VESTA in the Supplementary Material.
197	
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279	
280	FIGURE CAPTIONS
281	Figure 1. Typical dislocation microstructures of the simple-shear deformed wadsleyite (run
282	M0180 in Kawazoe et al. 2013). (a) Straight, long screw segments of [100] dislocations (black
283	arrowhead) and a few of 1/2[111] dislocations (Lower left, white arrowhead) are visible. (b)
284	Array of 1/2[111] dislocations that have dissociated into several partial dislocations (black
285	arrowheads) are in dislocation bands parallel to the (0-11) plane. The residual contrast of
286	stacking faults on the (010) plane is weakly visible (white arrowheads). The stacking faults on
287	the (010) plane are also indicated by remarkable streak lines along the [010]* direction on the
288	selected area electron diffraction (SAED) pattern of the nearest zone axis (c). The two-sided
289	arrows on the upper left and upper right in (a) and (b), respectively indicate approximately the
290	bulk shear direction in the deformation experiment.
291	

Figure 2. Typical WBDF images of 1/2 <101> dislocations co-activated with [100] dislocations. (a) A whole grain with $\mathbf{g} = 004$, the inset is the nearest principal zone axis. The right half of the grain with (b) $\mathbf{g} = 400$ (c) $\mathbf{g} = 004$, (d) $\mathbf{g} = 404$ and (e) $\mathbf{g} = -404$. Dislocations with $\mathbf{b} =$ [100] are visible in (b), (d) and (e), but they are invisible in (c). Dislocations with $\mathbf{b} = 1/2$ <101> are visible in (b) and (c but one of pairs, 1/2[-101] screw dislocations along the [-404] direction or 1/2[101] screw dislocations along the [404] direction is invisible in (d) and (e), respectively. The two-sided arrow on the upper right in (a) indicates approximately the bulk

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shear direction in the deformation experiment. The inset in the (a) is the nearest principal zone
axis, while the inset of (d) and (e) is the diffraction condition of the WBDF image.

Figure 3. Close-ups of an area in the Fig. 2(c) and the Fig. 2(d), respectively, indicating that (a) two thickness contour fringes are terminated at the extremity of the dislocation and its debris in the WBDF images with $\mathbf{g} = 004$ by two white arrowheads and (b) no oscillation contrasts in horizontally elongated dislocation lines of dislocations with $\mathbf{b} = [100]$ (grey arrowhead), and 1/2[101] (white arrowhead) and 1/2[-101] (residual contrast by $\mathbf{g}.\mathbf{b} = 0$, black arrowhead). Note: The grey arrowhead in the (a) indicates a different type of dislocation that would be a product of reactions among [100] and 1/2 < 101 > dislocations.

Figure. 4. WBDF-TEM images of the Shockley-type extended dislocation with $\mathbf{b} = 1/2 < 101 >$.

309 (a) $\mathbf{g} = -211$ and (b) $\mathbf{g} = 013$. (a) Fringe contrasts of its associated stacking faults on the (010)

plane in the [101] direction are visible in the images (white arrowheads). (b) The 1/2[101] dislocations are terminated on the edge of the (010) stacking faults, indicating the partial dislocations (the white arrowhead) was gliding in the (010) plane. The images correspond to the grains of Fig. 2 and Fig. 1(b), respectively. The two-sided arrow on the upper left in (b) indicates approximately the bulk shear direction in the deformation experiment.

Figure 5. Typical dark field TEM images of non-deformed wadsleyite (run M0187 in Kawazoe et al. 2013). (a) $\mathbf{g} = -2-1-1$, stacking faults are visible, (b) $\mathbf{g} = 0-80$, invisible. Some planar areas in the grain display fringe contrast of stacking faults (indicating white arrowheads) with partial dislocations at the ends, but they are not a glide configuration in contrast to Figure 4b where the (010) stacking fault planes are sub-parallel to a shear direction. The inset in the (b) is the nearest zone axis. The two-sided arrow on the upper right in (a) indicates a potential bulk shear direction.









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Figure 1. Typical dislocation microstructures of the simple-shear deformed wadsleyite (run M0180 in Kawazoe et al. 2013). (a) Straight, long screw segments of [100] dislocations (black arrowhead) and a few of 1/2[111] dislocations (Lower left, white arrowhead) are visible. (b) Array of 1/2[111] dislocations that have dissociated into several partial dislocations (black arrowheads) are in dislocation bands parallel to the (0-11) plane. The residual contrast of stacking faults on the (010) plane is weakly visible (white arrowheads). The stacking faults on the (010) plane are also indicated by remarkable streak lines along the [010]* direction on the selected

area electron diffraction (SAED) pattern of the nearest zone axis (c). The two-sided arrows on
the upper left and upper right in (a) and (b), respectively indicate approximately the bulk shear
direction in the deformation experiment.







Figure 2. Typical WBDF images of 1/2 <101> dislocations co-activated with [100] dislocations. (a) A whole grain with g = 004, the inset is the nearest principal zone axis. The right half of the grain with (b) g = 400 (c) g = 004, (d) g = 404 and (e) g = -404. Dislocations with b = [100] are visible in (b), (d) and (e), but they are invisible in (c). Dislocations with b = 1/2<101> are visible in (b) and (c), but one of pairs, 1/2[-101] screw dislocations along the [-404] direction or

1/2[101] screw dislocations along the [404] direction is invisible in (d) and (e), respectively. The
two-sided arrow on the upper right in (a) indicates approximately the bulk shear direction in the
deformation experiment. The inset in the (a) is the nearest principal zone axis, while the inset of
(d) and (e) is the diffraction condition of the WBDF image.



Figure 3. Close-ups of an area in the Fig. 2(c) and the Fig. 2(d), respectively, indicating that (a) two thickness contour fringes are terminated at the extremity of the dislocation and its debris in the WBDF images with $\mathbf{g} = 004$ by two white arrowheads and (b) no oscillation contrasts in horizontally elongated dislocation lines of dislocations with $\mathbf{b} = [100]$ (grey arrowhead), and 1/2[101] (white arrowhead) and 1/2[-101] (residual contrast by $\mathbf{g}.\mathbf{b} = 0$, black arrowhead). Note: The grey arrowhead in the (a) indicates a different type of dislocation that would be a product of reactions among [100] and 1/2<101> dislocations.

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Figure. 4. WBDF-TEM images of the Shockley-type extended dislocation with $\mathbf{b} = 1/2 < 101 >$. (a) $\mathbf{g} = -211$ and (b) $\mathbf{g} = 013$. (a) Fringe contrasts of its associated stacking faults on the (010) plane in the [101] direction are visible in the images (white arrowheads). (b) The 1/2[101] dislocations are terminated on the edge of the (010) staking faults, indicating the partial dislocations (the white arrowhead) was gliding in the (010) plane. The both of images correspond to the grains of Fig. 2 and Fig. 1(b), respectively. The two-sided arrow on the upper left in (b) indicates approximately the bulk shear direction in the deformation experiment.

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Figure 5. Typical dark field TEM images of non-deformed wadsleyite (run M0187 in Kawazoe et al. 2013). (a) $\mathbf{g} = -2-1-1$, stacking faults are visible, (b) $\mathbf{g} = 0-80$, invisible. Some planar areas in the grain display fringe contrast of stacking faults (indicating white arrowheads) with partial dislocations at the ends, but they are not a glide configuration in contrast to Figure 4b where the (010) stacking fault planes are sub-parallel to a shear direction. The inset in the (b) is the nearest zone axis. The two-sided arrow on the upper right in (a) indicates a potential bulk shear direction.